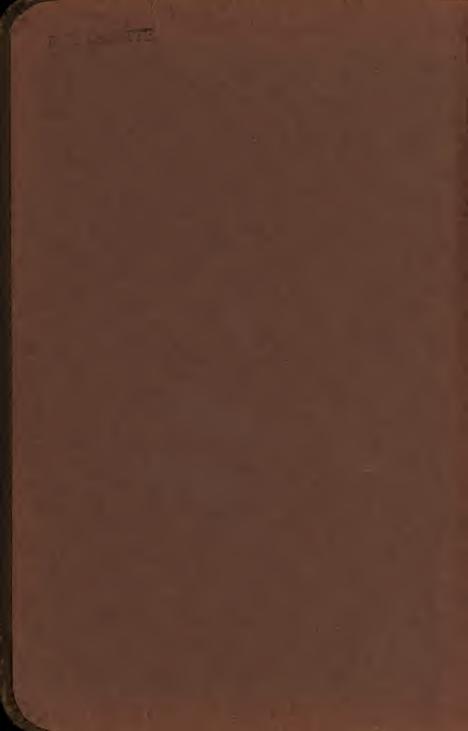
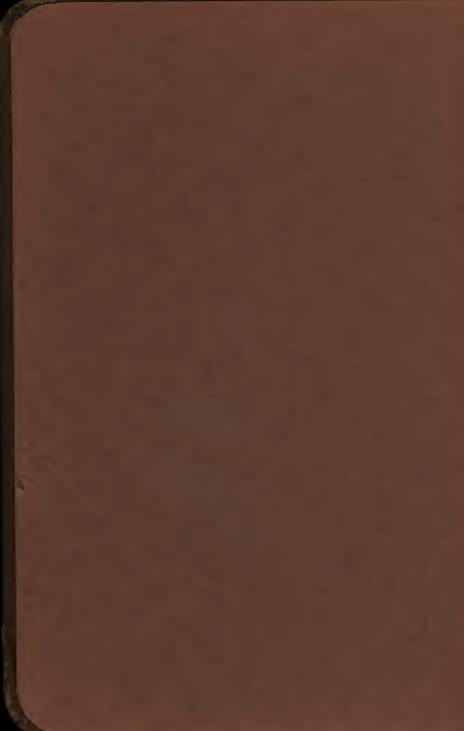
CARNEGIE STEEL COMPANY PITTSBURGH, PA.







NOTE

Attention is called to additions and modifications that have been found of advantage to users of Carnegie Beam Sections.

These are as follows:

Additional weights of CB 301, 165 and 151 pounds. Old weights of 135 and 125 pounds have been discontinued and are replaced by new weights of 138 and 126 pounds.

Additional weights of CB 271, 137 and 124 pounds.

Additional heavier weights of CB 146, 14" column section, advancing by 20 pounds increments from 325 to 425 pounds.

Additional lighter weights of CB 146, 106, 96 and 86 pounds.

A new 12" x 12" constant depth column group in weights of 102, 95, 88 and 82 pounds, to be called CB 124 C. CB 124 and CB 124 A have been discontinued.

A new 12" x 12" constant depth column group in weights of 76, 70 and 65 pounds, to be called CB 124 B.

CB 123 A is changed to a variable depth section in weights of 66, 60 and 55 pounds and will be called CB 123 B.

A new $10^{\prime\prime}$ x $10^{\prime\prime}$ constant depth column group in weights of 64, 59, 54 and 49 pounds, to be called CB 103 A. CB 103 has been discontinued.

New minimum weights of B 40, 20.5 pounds and B 39, 17.5 pounds. Minimum weights as formerly published B 40, 21 pounds and B 39, 18 pounds have been discontinued.

For additional information and data reference should be made to supplementary issue entitled:

CARNEGIE BEAM SECTIONS

Additions to New Series

SECOND EDITION—OCTOBER 1, 1928

PROFILES, PROPERTIES

AND

SAFE LOADS

FOR

NEW SERIES

OF

STRUCTURAL STEEL BEAMS

AND

COLUMN SECTIONS

MANUFACTURED BY
CARNEGIE STEEL COMPANY

SUBSIDIARY OF UNITED STATES STEEL CORPORATION PITTSBURGH, PA.

FIRST EDITION

A. I. A. FILE No. 13

G11618VM1028

Copyright, 1927, by CARNEGIE STEEL COMPANY Pittsburgh, Pa.

First Edition, January 1, 1927.

Printed in U.S.A.

Since the adoption of the present American Standard Beam Sections, in 1896, developments of such magnitude have taken place in the structural steel industry, both at home and abroad, as to demand an improved series of rolled sections suitable for both beam and column purposes.

The series now placed on the market under the name **CARNEGIE BEAM SECTIONS**, provides for this demand by means of a series of shapes combining sound engineering principles with practical improvements. All its sections are produced on a structural mill of the most advanced type.

The series provides a range of rolled steel beam and column sections progressing by regular steps, with contours that will permit sections to be used interchangeably for whichever purpose they are adapted, and in sizes and weights sufficiently varied to meet all ordinary requirements. Their efficiency is high and their component parts are proportioned to permit of ready fabrication.

ADVANTAGES

The advantages characterizing the new series of Carnegie Beam Sections will be explained under the following captions:—

CONTOUR DESIGN
WEB AND FLANGE RATIO
RANGE OF SIZES
PROGRESSIVE BEAM DESIGN
IMPROVED COLUMN DESIGN

CONTOUR DESIGN

A new form of contour has been adopted whose principal characteristic is the elimination of internal flange slope, the flanges being of uniform thickness throughout their width. This feature increases the strength of the section, permits simpler connections and facilitates fabrication.

Carnegie Beam Sections permit the use of maximum unit stresses in shear and compression for resistance to web buckling and flange crippling, respectively, in conformity with usual building specifications. All fillets, which are parabolic in form, combine maximum spread with minimum area.

WEB AND FLANGE RATIO

In the production of most of the Carnegie Beam Sections a method is used whereby an adequate variety of weights in each group, having substantially equal efficiency per pound, is attained by spreading both horizontal and vertical rolls a proportionate amount. This practice causes the depth of sections to vary somewhat from the nominal, but this variation is kept within limits that will not affect the standardization of details.

A second characteristic, found in the heavier groups of column sections, is an increase in width as compared with depth, combining maximum economy in design of framing and in floor space.

RANGE OF SIZES

Carnegie Beam Sections provide a range of beam and column shapes, from 8 to 30 inches deep and from 5 to 16 inches wide, in weights up to 305 pounds per linear foot, with section moduli about the major axis up to 738 in.³, and with radii of gyration about the minor axis up to 4.14 in.

In general, no sharp line has been drawn between beams, girder beams and columns. The consequent economy in number of sections will insure better deliveries, reduce the number of sizes carried in stock, and allow a greater standardization in shop methods and tools.

Profiles, dimensions and weights are given on pages 8 to 30. Other data pertaining to dimensions and properties are tabulated on pages 32 to 41.

The range of depths in which occurs the greatest normal demand is covered by the adoption of sections 14 and 16 inches deep, affording the designer a better and more economical selection of sections to be used as beams.

PROGRESSIVE BEAM DESIGN

The introduction of the 14 and 16 inch Carnegie Beam Sections gives a progressive series in which each depth is approximately 15 per cent. greater than the preceding depth, as shown graphically on range charts on pages 32 and 33. In addition, successive weights in each group are so arranged that their strengths progress by steps having close and approximately regular ratios of increase.

Intermediate groups of heavier sections, of the same depth but with wider flanges and greater strength, are provided for use as beams in structures where it is important to limit the depth of section. These sections are also suitable for columns.

The selectivity of the series for use as beams is indicated graphically in the tables and charts on pages 32 to 35.

Minimum weights of 10-, 12-, 14- and 16-inch sections are offered with a uniform width of 6 inches, which permits a corresponding uniformity in fireproofing and finish.

Very complete groups of sections 24, 27 and 30 inches deep, are provided with flanges 14 inches wide. These will be found convenient for use in structures that cannot be braced laterally and may also be used to advantage where limited clearance is an important factor in design.

Efficient sections, notably 12 inches and deeper, are provided with webs 3% inch in thickness, in order to comply with specifications requiring a minimum thickness of metal.

IMPROVED COLUMN DESIGN

Carnegie Beam Sections include two groups: a Variable-Depth Type and a Constant-Depth Type. The sections of the latter group are intended primarily for columns, though sections of either type may also be used as beams or girders. In the Variable-Depth Type both depth and width increase proportionately as weights increase from the minimum. In the Constant-Depth Type the depth does not change, the increase in weights being obtained by thickening the web and widening the flanges. With the heavier groups of both types, high properties about the minor axis are secured by the proportions adopted.

The Variable-Depth Type contains notably sections of the following depth, flange width and weights:—

CB 83 $8'' \times 8''$ 31 to 90 lbs. CB 145 $14'' \times 12''$ 85 to 105 lbs. CB 146 $14'' \times 15''$ 115 to 305 lbs.

These sections will be used principally as columns.

In addition, sections 8, 9, 10, 12 and 14 inches deep, are provided having intermediate flange widths which may be used either as beams in shallow floors or as light columns.

The Constant-Depth Type is offered in two depths only, 10 and 12 inches, with the following flange widths and weights:—

CB 102 10" x 8" 31 to 42 lbs. CB 124 12" x 10" 75 to 100 lbs. CB 103 10" x 9" 49 to 63 lbs. CB 125 12" x 12" 110 to 140 lbs. CB 104 10" x 10" 70 to 92 lbs. CB 126 12" x 14" 150 to 180 lbs. CB 105 10" x 12" 100 to 140 lbs. CB 127 12" x 14" 190 to 230 lbs.

The 10-inch series will take care of an ordinary 12-story building, while the 12-inch series, in conjunction with the 10-inch series, will take care of an ordinary 18-story building. If desired, the scope of any group can be extended by reinforcement with flange plates.

The Constant-Depth Type presents an innovation in rolled steel column sections in that the over-all depth for all sizes of a nominal depth does not vary. The advantages of this feature are reflected in the symmetry of beam and spandrel framework connecting to the columns at a number of successive floors in a steel building, thus effecting a substantial saving in the drafting room, fabricating shop and in the field. The avoidance of fillers under splices on the columns themselves is also advantageous. To the architect and the general contractor constant depth is valuable in that it permits a greater uniformity in fireproofing and finish.

MISCELLANEOUS DATA

All weights per linear foot of Carnegie Beam Sections are expressed in whole pounds. Fillets are included in weights, areas and other properties.

The dimensions to which the rolls for Carnegie Beam Sections are turned extend to three decimal places of an inch, as shown on diagrams on pages 8 to 29, but it will be more convenient for the designer to use the fractions to which they have been rounded in the tables of dimensions of sections on pages 33 to 41.

Carnegie Beam Sections will be furnished to the specifications of the Association of American Steel Manufacturers, American Society of Testing Materials or to such other acceptable standard specifications as may be required.

PROFILES AND DIMENSIONS

CARNEGIE BEAM SECTIONS 14.00" CB 302 0.530" CB 301

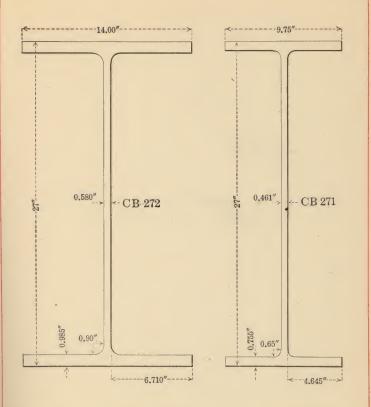
Section	Depth of Section,		Weight	Two	Flange Width,		Flange Thickness,		ickness,
Index	Inches		per Foot,		Inches		Inches		hes
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 302	30.781	30 ² 552	240	14.218	14752	1.597	11932	0.888	5364
	30.522	30 ³ 364	220	14.146	14964	1.4675	11532	0.816	1316
	30.263	30 ¹ 764	200	14.073	14564	1.338	11332	0.743	34
	30.000	30	180	14.000	14	1.2065	11364	0.670	4364
CB 301	30.298	30 ¹ 964	135	10.591	10 ¹ 952	1.031	1 ½ 2	0.621	58
	30.148	30964	125	10.546	10 ³ 564	0.956	6 ½ 4	0.576	3764
	30.000	30	115	10.500	10 ¹ 5	0.882	78	0.530	1752

6.665"----

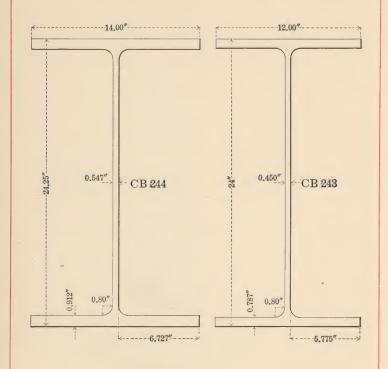
0.70"

----4:985"--

1.00"



Section	Depth of Incl	Section, hes	Weight per Foot.	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
	27.598	271932	190	14.176	1411/64	1.284	19%2	0.756	34
CB 272	27.400	271342	175	14.118	141/8	1.185	1316	0.698	4564
022.2	27.200	271364	160	14.059	141/16	1.085	1564	0.639	41/64
7	27.000	27	145	14.000	14	0.985	6364	0.580	3764
	27.340	2711/82	112	9.855	955/64	0.925	5964	0.566	916
CB 271	27.166	271164	101	9.799	951/64	0.838	27/32	0.510	3364
	27.000	27	91	9.750	934	0.755	34	0.461	15/82

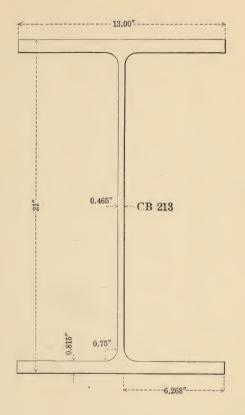


Section Index	Depth of Inc	Section, hes	per Foot,	Flange Width, Inches		Flange T Inc		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 244	24.664 24.526 24.388 24.250	$\begin{array}{c} 24^{2} \frac{1}{3} \\ 24^{1} \frac{1}{3} \\ 24^{2} \frac{1}{3} \\ 24^{2} \\ 4 \end{array}$	160 150 140 130	14.123 14.082 14.041 14.000	14½ 14½ 14¾ 14¾ 14	1.119 1.050 0.981 0.912	1 1/8 1 3/64 6 3/64 2 9/3 2	0.670 0.629 0.588 0.547	4364 56 1932 3564
CB 243	24.310 24.156 24.000	245/16 245/32 24	120 110 100	12.089 12.044 12.000	12352 12364 12	0.942 0.865 0.787	15/16 55/64 25/32	0.539 0.494 0.450	1732 12 2964

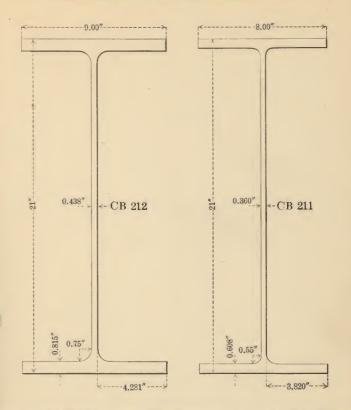




	Section	Depth of Inc	Section, hes	per Foot,		Flange Width, Inches		Flange Thickness, Inches		ickness, nes
	Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
С	B 242	24.308 24.154 24.000	24516 24532 24	94 85 76	9.844 9.797 9.750	9 ² 7⁄3 ² 9 ⁵ 1⁄6 ⁴ 9 ³ ⁄4	0.817 0.740 0.663	13/16 47/64 21/32	0.499 0.452 0.405	1/2 29/64 13/32
C	B 241	24.000	24	70	8.500	81/2	0.663	21/82	0.400	1342

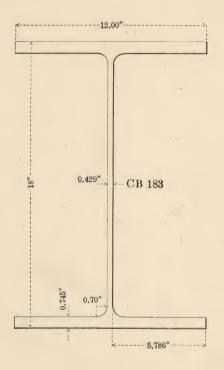


Section Index		Pepth of Section, Inches		Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 213	21.248 21.126 21.000	21¾ 21¾ 21¾ 21	120 112 104	13.070 13.034 13.000	13½6 13½2 13	0.939 0.878 0.815	15/16 78 13/16	0.535 0.499 0.465	1752 151 1552

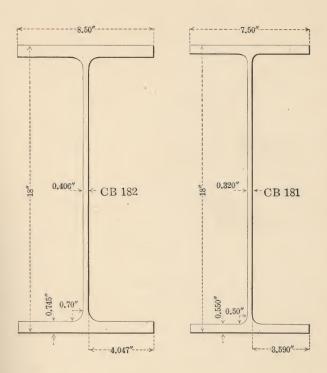


Section	Depth of	Section,	Weight	Flange Width,		Flange Thickness,		Web Thickness,	
	Inc	hes	per Foot.	Inches		Inches		Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 212	21.240	211564	92	9.064	9346	0.935	1516	0.502	1½
	21.120	2116	86	9.032	9342	0.875	76	0.470	15½2
	21.000	21	80	9.000	9	0.815	1316	0.438	716
CB 211	21.248 21.126 21.000 *21.034	2138	70 64 58 60	8.073 8.036 8.000 8.015	8564 8152 8 8164	0.732 0.671 0.608 0.625	4764 4364 3964 58	0.433 0.396 0.360 0.375	716 2564 2364 38

^{*}Special Section Web Thickness 3/8".

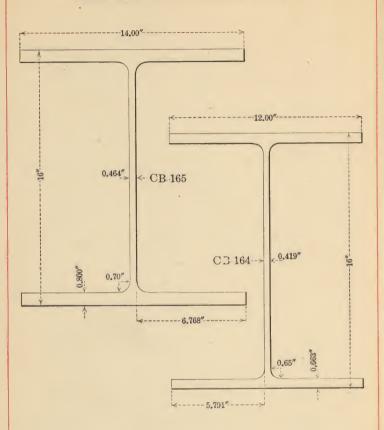


Section	Depth of Inc	Section, hes	per Foot,				Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction	
CB 183	18.238 18.120 18.000	181/8	100 93 86	12.069 12.034 12.000	12½6 12½2 12	0.864 0.805 0.745	5564 1316 34	0.498 0.463 0.429	1/2 15/32 27/64	



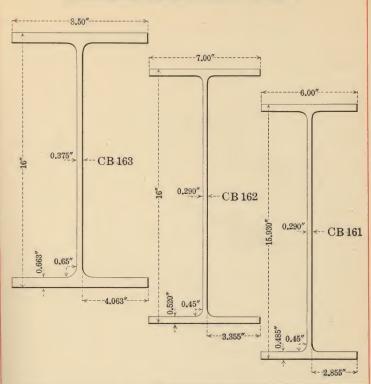
Section Index	Depth of Inc	Section, hes	Weight per Foot,	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 182	18.242 18.110 18.000	18764	78 72 67	8.565 8.530 8.500	8916 81732 812	0.866 0.800 0.745	5564 5164 34	0.471 0.436 0.406	1552 316 1352
CB 181	18.252 18.114 18.000 *18.024	18764 18	58 52 47 51	7.573 7.534 7.500 7.555	73764 71762 716 7916	0.676 0.607 0.550 0.562	4364 3964 3564 916	0.393 0.354 0.320 0.375	2564 2364 516 38

^{*}Special Section Web Thickness 38".



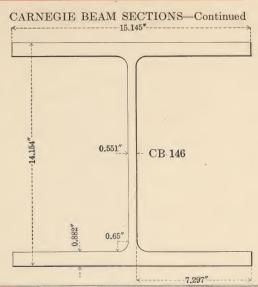
Section			Weight per Foot.	Flange Inc.		Flange T Inc		Web Thickness, Inches	
Index	Decimal		Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 165	16.236 16.110 16.000	16 ¹⁵ 64 16 ⁷ 64 16	115 107 100	14.068 14.032 14.000	14\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	0.918 0.855 0.800	5964 5564 5164	0.532 0.496 0.464	1732 12 1542
CB 164	16.240 16.120 16.000	1	90 83 76	12.076 12.039 12.000	12564 12532 12	0.783 0.723 0.663	2532 2332 2132	0.495 0.458 0.419	75 2964 2764

CARNEGIE BEAM SECTIONS—Continued

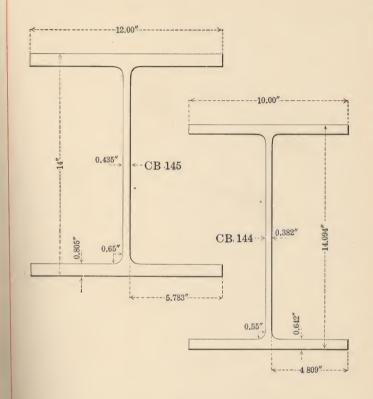


Section	Depth of Inc		Weight per Foot.	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
	16.226	16332	68	8.563	8916	0.776	2532	0.438	716
CB 163	16.114 16.000	16764	63 58	8.531 8.500	81782	0.720 0.663	2352 2352	$0.406 \\ 0.375$	1332 38
	16.254		50	7.072	7564	0.647	4164	0.362	2364
CB 162	16.128 16.000	16	45 40	7.036 7.000	7382	0.584 0.520	3764 3364	0.290	1964
	*15.934		43	7.085	7564	0.487	31/64 17/32	0.375	38 516
CB 161	16.012 15.930		38 35	6.024	61/32	0.326	3164	0.314	1964

*Special Section Web Thickness 36".

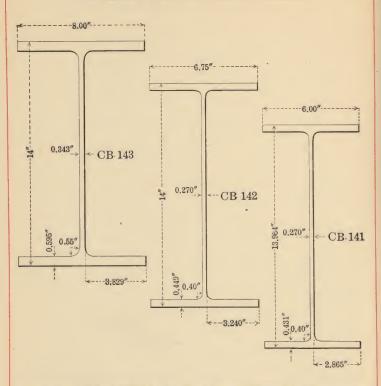


Section	Depth of Inc	Section, hes	Weight per Foot,	Flange Inc		Flange T Inc		Web Th Inc	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
	16.890	165764	305	16.000	16	2.250	21/4	1.406	11342
	16.752	1634	295	15.956	156164	2.181	2316	1.362	12364
	16.614	163964	285	15.912	1529/32	2.112	2764	1.318	15/16
	16.472	161532	275	15.870	1578	2.041	2364	1.276	1932
	16.332	162164	265	15.826	155364	1.971	13/32	1.232	11564
	16.192	16316	255	15.781	152532	1.901	12932	1.187	1316
	16.050	16364	245	15.738	154764	1.830	15364	1.144	1964
	15.908	152932	235	15.693	1511/16	1.759	14964	1.099	1332
	15.764	154964	225	15.650	152332	1.687	111/16	1.056	11/16
OD 140	15.622	15%	215	15.604	153964	1.616	13964	1.010	11/64
CB 146	15.478	153164	205	15.559	15916	1.544	13564	0.965	31/32
	15.334	152164	195	15.513	153864	1.472	11532	0.919	5964
	15.188	15346	185	15.469	151532	1.399	11332	0.875	7/8
	15.042	15364	175	15.424	152764	1.326	12364	0.830	5364
	14.896	145764	165	15.377	1538	1.253	1 1/4	0.783	25/32
	14.750	1434	155	15.330	1521/64	1.180	1316	0.736	4764
	14.602	143964	145	15.284	15%32	1.106	1 764	0.690	13/16
	14.452	142964	135	15.239	151564	1.031	11/32	0.645	41/64
	14.304	141964	125	15.191	15346	0.957	61/64	0.597	1932
	14.154	145/32	115	15.145	15%4	0.882	7,8	0.551	3564
	*14.162	14532	131	15.468	151532	0.886	57/64	0.874	7/8



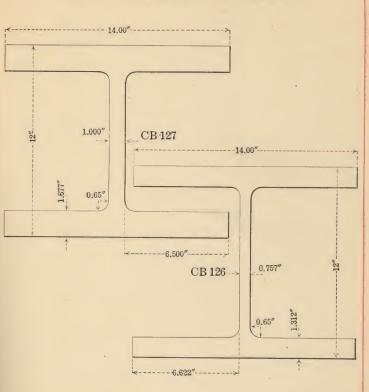
Section		Section, hes	Weight per Foot,	Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal Fraction		Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
	14.370	1438	105	12.101	12332	0.990	6364	0.536	1742
CB 145	14.186	14316	95	12.050	12364	0.898	5764	0.485	31/64
	14.000	14	85	12.000	12	0.805	1346	0.435	716
	14.382	1438	75	10.086	10332	0.786	25/32	0.468	1532
CB 144	14.238	141564	68	10.043	10364	0.714	23/32	0.425	2764
	14.094	14332	61	10.000	10	0.642	41/64	0.382	38

CARNEGIE BEAM SECTIONS—Continued

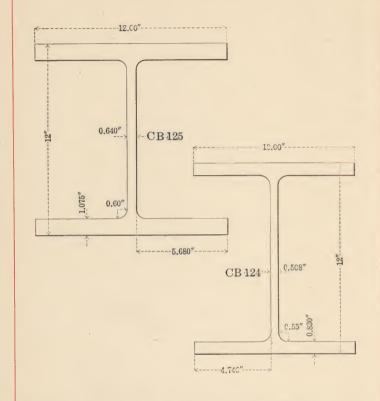


Section	Depth of Section, Inches		Weight per Foot.	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
	14.242	141564	58	8.070	81/16	0.716	2342	0.413	1342
CB 143	14.122	141/8	53	8.035	81/32	0.656	21/32	0.378	38
	14.000	14	48	8.000	8	0.595	1952	0.343	11/32
	14,240	141564	42	6.822	65364	0.569	916	0.342	1142
	14.160	14532	39	6.798	65364	0.529	1732	0.318	516
CB 142	14.080	14564	36	6.774	62532	0.489	31/64	0.294	1964
	14.000	14	33	6.750	634	0.449	2964	0.270	1764
	*14.000	14	38	6.855	65564	0.449	2964	0.375	38
CB 141	13.964	133142	30	6.000	6	0.431	716	0.270	1764

*Special Section Web Thickness 3/8".

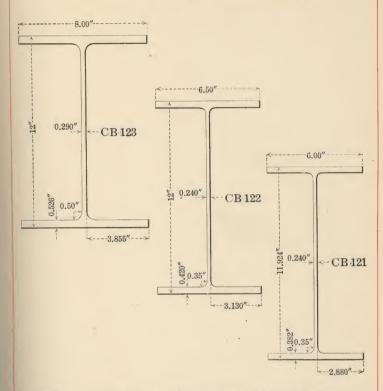


Section Index	Depth of Section, Inches		per Foot,	T	Width,		hickness,	Web Thickness, Inches	
	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 127	CONSTANT	12	230 220 210 200 190	14.980 14.735 14.490 14.245 14.000	14 ⁶ 364 14 ⁴ 764 14 ³ 164 14 ¹ 4 14	1.677	43 64	1.980 1.735 1.490 1.245 1.000	16364 14764 13164 114
CB 126	P 12	12	180 170 160 150	14.735 14.490 14.245 14.000	14 ⁴ 76 ₄ 14 ³ 1/6 ₄ 141/4 14	1.312	16	1.492 1.247 1.002 0.757	13364 134 1 34



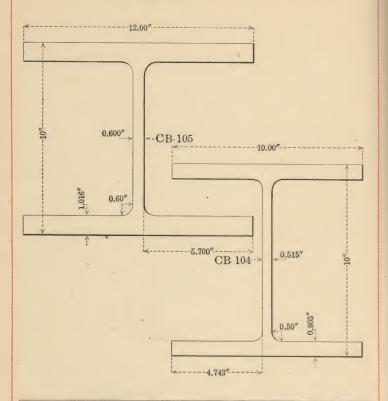
Section	Depth of Section, Inches		Weight per Foot,	Inc	Width, hes	Flange T Inc		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 125	CONSTANT	12	140 130 120 110	12.736 12.491 12.245 12.000	124764 123164 1214 12	1.075	5 64	1.376 1.131 0.885 0.640	136 136 136 5364 4364
CB 124	E 12	12	100 91 83 75	10.613 10.392 10.196 10.000	$ \begin{array}{r} 10^3 \% 4 \\ 10^2 \% 4 \\ 10^1 \% 4 \\ 10 \end{array} $	0.830	<u>53</u> 64	1.121 0.900 0.704 0.508	1 1/8 29/32 45/64 33/64

CARNEGIE BEAM SECTIONS—Continued

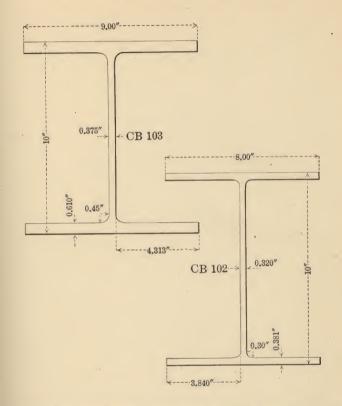


Section Index	Depth of Section, Inches		Weight per Foot,	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
	12.258	121764	50	8.071	8564	0.655	21/32	0.361	23/64
CB 123	12.130	121/8	45	8.036	81/32	0.591	1932	0.326	21/64
	12.000	12	40	8.000	8	0.526	1732	0.290	1964
	12.236	121564	36	6.568	6916	0.538	1742	0.308	916
OD 100	12.118	121/8	32	6.534	61782	0.479	31/64	0.274	932
CB 122	12.000	12	28	6.500	61/2	0.420	2764	0.240	1564
	*12.022	12164	34	6.635	641/64	0.431	716	0.375	3/8
CB 121	11.924	115964	25	6.000	6	0.382	38	0.240	1564

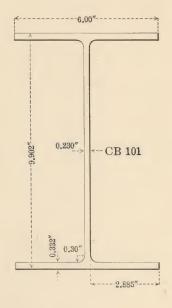
*Special Section Web Thickness 3/8".



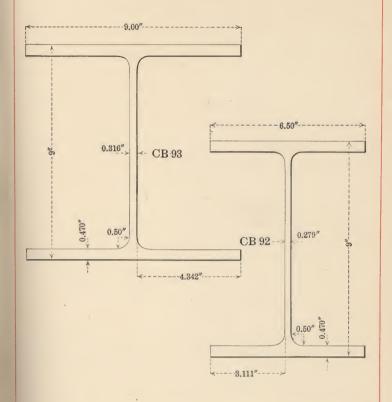
Section Index	Depth of Section, Inches		Weight per Foot,	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 105	C ON STANT	10	140 132 124 116 108 100	13.177 12.941 12.706 12.471 12.236 12.000	$ \begin{array}{r} 13^{1}\%_{4} \\ 12^{1}\%_{6} \\ 12^{4}\%_{6} \\ 12^{1}\%_{2} \\ 12^{1}\%_{6} \\ 12^{1}\%_{6} \\ 12 \\ \end{array} $	1.016	1 64	1.777 1.541 1.306 1.071 0.836 0.600	12532 13564 1516 1564 2732 1932
CB 104	D E P T H	10	92 84 77 70	10.647 10.411 10.206 10.000	10 ⁴ }6 ₄ 10 ¹ }6 ₂ 10 ¹ }6 ₄ 10	0.805	13	1.162 0.926 0.721 0.515	1552 5964 2352 3364



Section	Depth of Section, Inches		Weight per Foot,	Flange Inc		Flange T Inc		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 103	CONSTANT	10	63 56 49	9.412 9.206 9.000	91332 91364 9	0.610	<u>39</u> 64	0.787 0.581 0.375	25 % 2 3 764 3 %
CB 102	D E P T T H	10	42 36 31	8.324 8.147 8.000	82364 8964 8	0.381	3 8	0.644 0.467 0.320	41/64 15/62 5/16

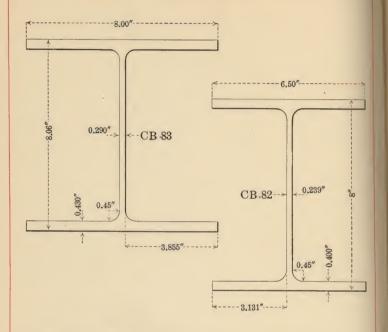


Section Index	Depth of Section, Inches		Weight per Foot,	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 101	10.228 10.098 10.000 9.902	10 ¹⁵ 64 10 ³ 62 10 9 ² 962	30 26 23 21	6.068 6.029 6.000 6.000	61/16 61/12 6	0.495 0.430 0.381 0.332	1/2 3/16 3/8 2/64	0.298 0.259 0.230 0.230	1964 1764 1564



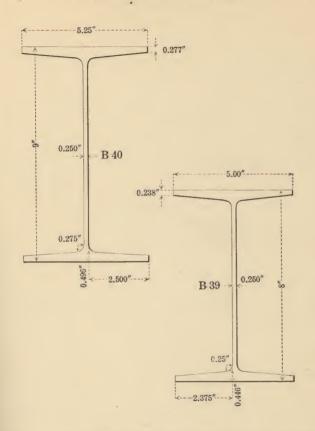
Section Index	Depth of Section, Inches		Weight per Foot,	Flange Width, Inches		Flange Thickness, Inches		Web Thickness, Inches	
	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
CB 93	9.242 9.122 9.000	915/64 91/8 9	48 43 38	9.082 9.041 9.000	9564 9364 9	0.591 0.531 0.470	1932 1732 1532	0.398 0.357 0.316	2564 2364 516
CB 92	9.192 9.096 9.000	9316 9332 9	35 32 29	6.556 6.528 6.500	6%16 617%2 61%	$0.566 \\ 0.518 \\ 0.470$	916 3364 1532	0.335 0.307 0.279	21/64 516 9/32

CARNEGIE BEAM SECTIONS-Concluded

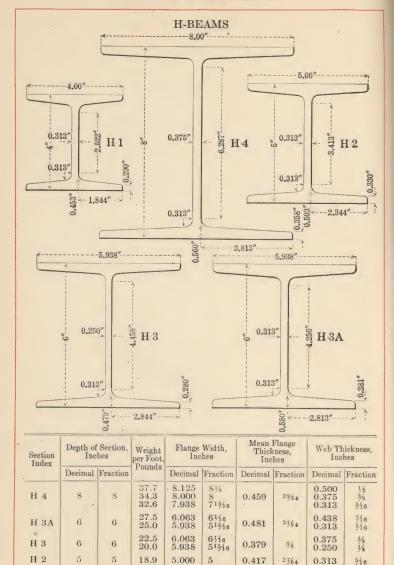


Section Index	Depth of Inc	Section, hes	Weight per Foot,	Tno	Width, hes	Flange T Inc		Web Thickness, Inches	
Index	Decimal	Fraction	Pounds	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction
	9.606	93964	90	8.520	83364	1.203	11364	0.810	1316
	9.456	92964	84	8.469	81532	1.128	11/8	0.759	4964
	9.302	91964	78	8.418	82764	1.051	1364	0.708	4564
	9.150	9532	72	8.366	82364	0.975	31/32	0.656	21/32
	8.994	9	66	8.314	8516	0.897	5784	0.604	3964
CB 83	8.838	827/32	60	8.261	81764	0.819	13/16	0.551	3564
	8.680	811/16	54	8.208	81364	0.740	47/84	0.498	3,5
	8.520	83364	48	8.155	8532	0.660	21/32	0.445	716
	8.360	82364	42	8.100	8332	0.580	3764	0.390	2564
	8.198	81364	36	8.046	8364	0.499	7,6	0.336	11/32
	8.060	81/16	31	8.000	8	0.430	316	0.290	1964
	8.196	81364	30	6.559	6916	0.498	3.6	0.298	1964
CB 82	8.098	8342	27	6.529	617/32	0.449	2964	0.268	1764
	8.000	8	24	6.500	632	0.400	1342	0.239	1564

STANDARD MILL SECTIONS



Section Index			Weight per Foot,	T	Flange Width, Inches		Flange ness, hes	Web Thickness, Inches	
	Decimal	Fraction	Pounds Decimal		Fraction	Decimal	Fraction	Decimal	Fraction
B 40	9	9	25 21	5.380 5.250	538 514	0.3865	<u>25</u> 64	0.380 0.250	38 14
B 39	8	8	21 18	5.110 5.000	5764	0.342	11 32	0.360	²³ 64



4 Full information as to uses of H-Beams is given in pamphlet entitled "Steel Mine Timbers."

4.000

36

0.313

516

0.372

H 1

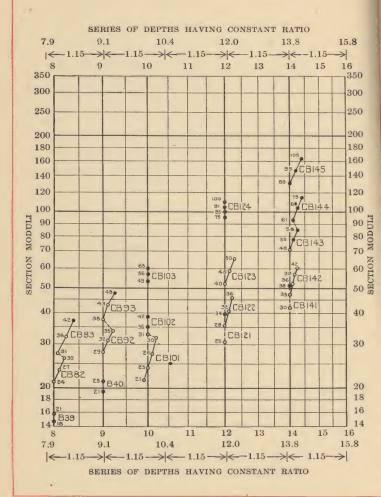
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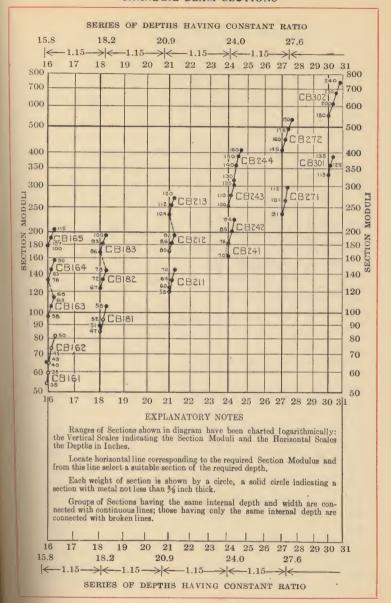
4

13.8

ELEMENTS AND PROPERTIES

RANGE OF SECTIONS SELECTED FOR USE AS BEAMS





CARNEGIE BEAM SECTIONS

BEAM SECTIONS COMPARATIVE TABLE OF SECTION MODULI

																	_		_
Section Modulus	30 I	n.	27 I	n.	24 I	n.	21 I	n.	Section Modulus	24 I	n.	21 I	n.	18 I	n.	16 I	n.	14 I	n.
Sec	Wt.	No.	Wt.	No.	Wt.	No.	Wt.	No.	Sec	Wt.	No.	Wt.	No.	Wt.	No.	Wt.	No.	Wt.	No.
738	240						, ,		236			104							
676	220	CB 3							225	94			СВ						
615	200	0 2					1		205				CB 2 1			115			
553	180	_							203	85			3						
535			190						196		CB 2 4	92		100					
492			175	СВ					191		2					107	CB		
450			160	2 7					184			86	CR		СВ		1 6 5		
411				2	160				182	76			CB 2 1	93	1 8 3		5		
408			145						178		-		2		3	100			
390	135	CB 3		-					171			80							
385		0			150	CB 2			168					86					-
361	125	-				CB 2 4 4			163	70								105	
359				+ 1	140				157						-	90	-		an
334					130				147		СВ							95	CB 1/4
332	115								145		2 4	70	CB 2	78		83	an		5
302	110	-		CR	120				133		1	64	CB 2 1 1	72	CB	76	CB 1		
293			112	2 7					132			01			8 2		1 6 4	85	
277			112	i	110				124			60		67	-				-
272					110	CB 2 4	120	-	120			58		0.					1
265			101			4 3	120		115				-		-		-	75	CB
254		1	101			9	112	CB 2 1	114							68	CB	10	CB 1 4 4
252					100		112	1 3	114		-					00	6 3		4
238			91		100			3									3		
400		1	91					1					1						

CARNEGIE BEAM SECTIONS—Continued

BEAM SECTIONS

COMPARATIVE TABLE OF SECTION MODULI

-						-	-	-		-	11.					1				_	_
Section	18 I	n.	16 I	n.	14 I	n.	12 I	n.	10]	[n.	Section Modulus	14	In.	12	In.	10	In.	9 I	n.	8 1	n.
Sec	Wt.	No.	Wt.	No.	Wt.	No.	Wt.	No.	Wt.	No.	Sec	Wt.	No.	Wt.	No.	Wt.	No.	Wt.	No.	Wt.	No.
110							100				47.8		СВ					48			
105	58		63				91				47.6	33	1 4								
104				an	68	an		an			45.8		2	36							
100				CB 1 6 3		CB 1	83	CB 1 2 4			42.9							43			
97.1		CD	58	3		1 4 4		4			41.8	30	CB 1						CR		
95.1		CB 1					75			1	40.7		4	32					CB 9 3		
94.4	52	8									39.6			34	СВ				0		
93.1					61						38.1				1 2 2	42					
89.9	51										37.9				2			38			
85.6					58						37.4						CB			42	
85.4	47										35.6			28			1 0				
81.9			50	СВ		СВ					35.1					36	2				
78.2				6 2	53	1 4 3					33.8							35			
73.8			45	2		3					32.7					31					
70.9					48						32.0								CB	36	CB 8 3
65.7			43								31.9					30			9 2		3
65.6			40								30.9							32			
65.4							50	CB			30.7			25							
60.6					42			1 2 3			28.0							29			
60.1								J	63		27,6					26	CB 1 0				
59.3			38	CB							27.5						0			31	
58.8				CB 1 6 1			45			CB	26.3				CB					30	
56.6			1	-		CR			56	1 0	24.4				CB 1 2 1	23					
56.3					39	CB 1 4 2				3	23.7				1					27	CB 8 2
54.7			35			2					21.7					21					2
53.2									49		21.2	- 1						25			
52.3							40				21.1								В	24	
51.9					36						19.5							21	4 0		R
51.1			1		38						15.9								0	21	B 3 9
							b .			J	14.7]]		1	18	

CARNEGIE BEAM SECTIONS—Continued

COLUMN SECTIONS

COMPARATIVE TABLE OF RADII OF GYRATION AND AREAS

Area		14 In.			12 In.			10 In.		Area
Ar	Weight	Г 2-2	No.	Weight	r 2-2	No.	Weight	r 2-2	No.	Ar
89.70	305	4.14								89.70
86.76	295	4.13								86.76
83.82	285	4.12								83.82
80.87	275	4.10								80.87
77.93	265	4.09		3						77.93
74.99 72.06	255	4.08								74.99
69.11	245 235	4.05								72.06
67.64	250	4.00		230	3.74					69.11
66.17	225	4.04		230	0.74				-	67.64
64.70	220	4.04		220	3.73					66.17
63.23	215	4.03		220	0.10	CB				64.70 63.23
61.76	210	1.00		210	3.72	1 2				61.76
60.28	205	4.01		210	0,12	2 7				60.28
58.82	200	1.01		200	3.71	1				58.82
57.34	195	4.00		200	0.17					57.34
55.88	200	1,00		190	3.71		·			55.88
54.41	185	3.98			0111					54.41
52.94			CB	180	3.64					52.94
51.47	175	3.97	1 4		0.01					51.47
50.00			6	170	3.65	СВ				50.00
48.52	165	3.96			0.00	1				48.52
47.06				160	3.67	2				47.06
45.58	155	3.94								45.58
44.12				150	3.69					44.12
42.64	145	3.93				_				42.64
41.17				140	3.01		140	3.08		41.17
39.70	135	3.92								39.70
38.81							132	3.09		38.81
38.52	131	3,77								38.52
38.24				130	3.03	СВ				38.24
36.75	125	3.90				1			CB	36.75
36.46						2 5	124	3.09	0	36.46
35.28				120	3.06	9			5	35.28
34.11				1			116	3.11		34.11
33.82	115	3.89								33.82
32.34				110	3.10		400			32.34
31.76	40.5	0.00	CD	1			108	3.13		31.76
30.88	105	3.08	CB 1	100	0.00		100			30.88
29.40	6-	0.00	4	100	2.39	CD	100	3.16		29.40
27.93	95	3.06	5			CB			CIT	27.93
27.06				0.1	0.41	1 2	92	2.50	CB 1	27.06
26.76				91	2.41	4	_		0	26.76
							- 1		4	

CARNEGIE BEAM SECTIONS—Continued

COLUMN SECTIONS

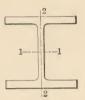
COMPARATIVE TABLE OF RADII OF GYRATION AND AREAS

Area	1	4 In.		1	2 In.		1	0 In.			9 In.		8	3 In.		60
- A	Wt.	r 2-2	No.	Wt.	r 2-2	No.	Wt.	r 2-2	No.	Wt.	r 2-2	No.	Wt.	Г 2-2	No.	Area
26.47 24.99 24.71 24.70		3.05	CB 1 4 5			СВ	84	2.48					90 84	2.17 2.15		26.47 24.99 24.71 24.70
24.41 22.93 22.65 22.05	75	2.47	СВ	83 75	2.45	1 2 4	77	2.51	1 0 4				78	2.14		24.41 22.93 22.65 22.05
21.17 20.59 19.99	68	2.46	1 4 4				70	2.55	-				72	2.12		21.17 20.59
19.40 18.53							63	2.14			į.		66	2.11		19.99 19.40 18.53
17.94 17.63 17.05	58	1.92	-						СВ				60	2.09	8 3	17.94 17.63 17.05
16.47 15.87 15.59 14.69	53	1.91	CB 1 4 3	50	1.98	CB 1 2 3	56	2.20	1 0 3				54	2.07		16.47 15.87 15.59 14.69
14.41 14.12 14.11 14.10	48	1,90				3	49	2.27		48	2.29					14.41 14.12 14.11
13.23 12.65 12.35	42	1.56	-	45	1.97		42	1.73		43	2.28.	CB 9	48	2.06		14.10 13.23 12.65 12.35
12.34 11.76 11.47	39	1.56	CB 1 4	40	1.95		12	1.10				3	42	2.04		12.34 12.76 11.47
11.17 10.59 10.58	36	1.55	2	36	1.55		36	1.80	CB	38	2.26	_	36	2.02		11.17 10.59 10.58
9.71 9.40 9.11	33	1.54	_	32	1.54	CB 1 2 2	31	1.89	0 2	35 32	1.61 1.60	CB 9				10.29 9.71 9.40 9.11
9.10 8.81 8.53										29	1.59	2	31 30	2.01 1.63	СВ	9.10 8.81 8.53
8.22 7.93 7.06				28	1.53							_	27 24	1.62 1.61	8 2	8.22 7.93 7.06

CARNEGIE BEAM SECTIONS—Continued



OF
SECTIONS
DECIMAL

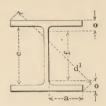


G .1											
Section Index	Weight	Area	Depth	Flange Width	Web Thick-	A	cis 1-1		A	xis 2-2	
and Nominal	Foot	Section		44 IG 011	ness	I	S	r	I	S	r
Depth	Lbs.	In. 2	In.	In.	In.	In.4	In.3	In.	In.4	In.3	In.
CB 302	240 220		$30.781 \\ 30.522$.888 .816	$11356.0 \\ 10320.4$	676.3	12.63	693.9	98.1	3.28
30′′	200 180		30.263 30.000		.743 .670	9305.7 8301.4					3.25 3.23
CB 301 30"	135 125	36.75	30.298 30.148	10.546	.621 .576 .530	5907.3 5441.7 4985.3	361.0	12.17	187.4	35.5	2.27 2.26
	115		30.000								
CB 272	190 175	51.47	27.598 27.400	14.118	.756 .698	7376.9 6746.8	492.5	11.45	556.6	78.9	3.31
27''	160 145		27.200 27.000	14.059 14.000	.639 .580	6121.8 5508.7					3.27 3.25
CB 271	112 101		27.340 27.166			4007.6 3595.7					$\frac{2.12}{2.11}$
27''	91		27.100			3217.0					2.09
OD 044	160 150			$14.123 \\ 14.082$		5065.7 4720.5					3.34
CB 244 24"	140 130	41.16	24.388	14.041 14.000	.588	4380.4 4045.1	359.2	10.32	453.1	64.5	3.32 3.31
CB 243	120			12.089		3669.7					2.81
24"	110 100			12.044 12.000		3343.5 3020.5	276.8 251.7	10.14	252.2 226.9	37.8	2.79 2.78
CB 242	94		24.308 24.154		.499 .452	2734.9 2457.2					2.17 2.16
24"	85 76		24.154 24.000			2184.4					2.14
CB 241 24"	70	20.58	24.000	8.500	.400	1953.8	162.8	9.74	68.0	16.0	1.82
CB 213	120			13.070 13.034		2890.9 2683.7			349.7 324.3		3.15
21''	112 104			13.000		2475.3			298.7		3.13
CB 212	92		21.240			2086.4 1939.3			3 116.3 3 107.7		2.07
21''	86 80		21.120 21.000			1794.4			99.2		2.05
CD 911	70		21.248 21.126			1542.9 1403.3					1.77
CB 211 21"	64 58		21.120			1263.2					1.75
	60	17.64	21.034	8.015	.375	1304.9	124.1	8.60	53.7	13.4	1.75

CARNEGIE BEAM SECTIONS—Continued

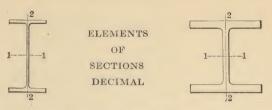


OF
SECTIONS
FRACTIONAL



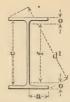
Weight	Depth	Flai	nge	W	eb]	Distance			Section
per Foot	of	Width	Thick- ness	Thick- ness	I Thick- ness +	a	С	f	0	d^1	Index and Nominal
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	Depth
240 220 200 200 180	3034 3012 3014 30	14316 1416 1416 1416	1916 1716 1516 1316	78 1316 34 1116	1/2 7/16 3/8 3/8	611/16	$27\frac{16}{27\frac{16}{16}}$ $27\frac{16}{27\frac{16}{16}}$ $27\frac{16}{16}$	25\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	258 21/2 23/8 21/4	3315/16 335/8 333/8 33/8	CB 302 30"
135 125 115	305/16 301/8 30	1058 10916 10½	1 15/16 78	58 916 12	516 516 516	5 5 5	28346 28346 28346	2634 2634 2634		$32\frac{1}{8}$ $31\frac{15}{16}$ $31\frac{13}{16}$	
190 175 160 145	$27\frac{5}{8}$ $27\frac{3}{8}$ $27\frac{3}{16}$ 27	14316 1436 14316 14316	1 1/4 1 3/16 1 1/16	3/4 1)/16 5/8 9/16	716 38 38 516	634 634 634 634	25 25 25 25 25	23 ¼ 23 ¼ 23 ¼ 23 ¼ 23 ¼	2346 216 2 178	31½6 30¼6 30¾6 30¾6	CB 272
112 101 91	2734 27346 27	978 91316 934	15/16 13/16 3/4	916 32 316	516 516 14	411/16	$25\%6 \\ 25\%6 \\ 25\%6$	241/8 241/8 241/8	158 132 1716	$29\frac{1}{6}$ $28\frac{1}{16}$ $28\frac{1}{16}$	CB 271 27"
160 150 140 130	$241\frac{1}{16}$ $24\frac{1}{2}$ $24\frac{1}{3}$ $24\frac{1}{4}$	14½ 14½6 14½6 14	1 1/8 1 1/16 1 15/16	11/16 5/8 9/16 9/16	38 38 516 516	634 634 634 634	2238 2238 2238 2238 2238	2034 2034 2034 2034	138	287/6 285/6 281/8 28	CB 244 24"
120 110 100	24546 241/8 24	12½6 12½6 12	15/18 78 13/16	1,6	516 14 14	51346	2238 2238 2238	2034 2034 2034	134 1114 158	27346 27 2678	CB 243 24"
94 85 76	24516 2438 24	978 913/16 934	13/16 3/4 11/16	746	1/4 1/4 1/4	411/1	$22\frac{5}{8}$ $22\frac{5}{8}$ $22\frac{5}{8}$ $22\frac{5}{8}$	$21\frac{3}{8}$ $21\frac{3}{8}$ $21\frac{3}{8}$	1346 138 1546	2614 2616 251516	CB 242 24"
70	24	81/2	13/16	3/8	3/4	41/16	2258	2138	1516	251/2	CB 241 24"
120 112 104	21 ½ 21 ½ 21 ½ 21	13½6 13½6 13	15/16 7/8 13/16	1/2	516 14 14	6516 6516 6516		1738 1738 1738	198	2415/16 2413/16 2413/16	
92 86 80	21¼ 21⅓ 21⅓ 21	91/16 91/16 9	1516 78 1316	1,5	1/4 1/4 1/4	4516	19516 19516 19516	1738	111/1 15/8 19/16		CB 212 21"
70 64 58	21¼ 21⅓ 21	8½6 8½6 8	34 111 58	716 38 38	1/4 1/4 3/16	3134	61934 61934 61934	1858 1858 1858	1516 134 1316	$22\frac{5}{8}$ $22\frac{1}{2}$	CB 211 21"
60	21	8	5/8	3/8	316	3134	6 1934	18%	1310	221/2	1

CARNEGIE BEAM SECTIONS—Continued



Section Index	Weight	Area	Depth	Flange Width	Web Thick-	A	xis 1-1		A	xis 2-2	
and Nominal	Foot	Section	Section	** 101011	ness	I	S	r	I	S	r
Depth	Lbs.	In.2	In.	In.	In.	In.4	In.3	In.	In.4	In.3	In.
CB 183	100 93 86	29.40 27.35 25.29		$12.069 \\ 12.034 \\ 12.000$.498 .463 .429	1783.4 1648.4 1514.1	181.9	7.76	253.4 234.0 214.7	38.9	2.94 2.93 2.91
CB 182 18"	78 72 67	21.17	18.242 18.110 18.000	8.530	.471 .436 .406	1318.8 1208.1 1117.1	133.4	7.55	82.9	21.2 19.4 18.0	1.99 1.98 1.97
CB 181 18"	58 52 47	15.30 13.82	18.252 18.114 18.000	7.534 7.500	.393 .354 .320	960.8 855.1 768.6	94.4 85.4	7.48 7.46	43.3 38.7	$13.0 \\ 11.5 \\ 10.3$	1.70 1.68 1.67
	51	15.00	18.024	7.555	.375	810.0	89.9	7.35	40.5	10.7	1.64
CB 165 16"	115 107 100	31.46	16.236 16.110 16.000	14.032	.532 .496 .464	$1665.6 \\ 1537.2 \\ 1426.8$	190.8	6.99	$\frac{426.2}{393.9}$ $\frac{366.0}{366.0}$	56.1	3.55 3.54 3.53
CB 164 16"	90 83 76	24.41	16.240 16.120 16.000	12.039	.495 .458 .419	$1275.5 \\ 1167.7 \\ 1061.3$	144.9	6.92	$230.0 \\ 210.4 \\ 191.1$	35.0	2.95 2.94 2.92
CB 163 16"	68 63 58	18.52	16.226 16.114 16.000	8.531	.406	923.7 849.9 776.6		6.77	74.6	19.0 17.5 16.0	2.02 2.01 2.00
CB 162 16"	50 45 40	13.23 11.75	16.254 16.128 16.000	7.036 7.000	.326	666.0 595.0 524.6	73.8 65.6	$6.73 \\ 6.71 \\ 6.68$	38.2 34.0 29.8		1.61 1.60 1.59
	43	12.65	15.934	7.085	.375	523.8	65.7	6.44	28.9	8.2	1.51
CB 161 16"	38 35	$11.17 \\ 10.29$	16.012 15.930			475.1 435.5	59.3 54.7	$\frac{6.52}{6.50}$	19.2 17.5	6.4 5.8	1.31 1.30

CARNEGIE BEAM SECTIONS—Continued



DIMENSIONS
OF
SECTIONS
FRACTIONAL

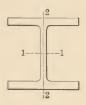


Weight	Depth	Fla	nge	W	eb			Distance	9		Section
per Foot	of	Width	Thick- ness	Thick- ness	½ Thick- ness +	a	С	f	0	d1	Index and Nominal
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	• In.	Depth
100 93 86		12½6 12½6 12½6	76 1316 34	75 716 716	1/4 1/4 1/4	51316 51316 51316	161/2	151/8 151/8 151/8	1916 112 1316	$21\frac{7}{8}$ $21\frac{3}{4}$ $21\frac{5}{8}$	CB 183 18"
78 72 67	18¼ 18⅓ 18	8916 812 812	78 1316 34	1/2 7/16 3/8	14 14 14		16½ 16½ 16½ 16½	151/8 151/8 151/8	11/2	2018 20 191516	CB 182 18"
58 52 47	18¼ 18⅓ 18	7916 7916 712	11/16 5/8 9/16	3/8 3/8 5/16	74 316 316	358 358 358	1638 1638 1638	15 78 15 78 15 78	1½ 1½6	1934 1958 1942	CB 181 18"
51	18	7916	916	3/8	316	358	16 78	1578	13/16	19916	
115 107 100	16¼ 16⅓ 16	141/16 14 14	15/16 7/8 13/16	916 12 716	516 14 14	$\begin{array}{c} 6^{13}16 \\ 6^{13}16 \\ 6^{13}16 \end{array}$	1438	13 13 13	158 1916 132	$21\frac{1}{2}$ $21\frac{3}{8}$ $21\frac{1}{4}$	CB 165 16"
90 83 76	16½ 16½ 16	121/16 121/16 12	13/16 3/4 11/16	3/16 3/16	14 14 14	51346	1458 1458 1458	1338 1338 1338	1716 138 1516	20¼ 20⅓ 20 20	CB 164 16"
68 63 58	1614 1618 16	8916 812 812	34 34 1116	716 38 38 38	1/4 1/4 3/16	41/16 41/16 41/16	1458 1458 1458	13% 13% 13%	1346 138 1546	1838 1834 1838	CB 163 16"
50 45 40	16¼ 16⅓ 16	71/16 71/16 7	5/8 9/16 1/2	38 516 516	316 316 316	338 338 338	141546 141546 141546	14	1 1/8 1 1/16 1	1734 1758 1752	CB 162
43	151516	71/16	1,6	38	316	338	1415/1	14	1	17346	
38 35	16 15 ¹ 516	6 6	1/2 1/2	516 516	316 316	278 278	14 ¹ 510 14 ¹ 510		1 1516	17½8 17½6	CB 161 16"

CARNEGIE BEAM SECTIONS—Continued



OF
SECTIONS
DECIMAL

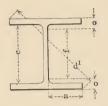


	1	7	1								
Section Index and	Weight	of	Depth	Flange Width	Web Thick-	A	xis 1-1		A	xis 2-2	
Nominal	Foot	Section	Section		ness	I	S	r	1	S	r
Depth	Lbs.	In.2	In.	In.	In.	In.4	In.3	In.	In.4	In.3	In.
	305 295 285 275 265	86.76 83.82 80.87	$16.752 \\ 16.614 \\ 16.472$	$15.956 \\ 15.912 \\ 15.870$	1.362 1.318 1.276	$3948.1 \\ 3778.1 \\ 3607.8$	$471.4 \\ 454.8 \\ 438.1$	6.75 6.71 6.68	1539.1 1479.4 1420.7 1362.0 1304.2	185.4 178.6	4.13
	255 245 235 225 215	74.99 72.06 69.11 66.17 63.23	$\begin{array}{c} 16.192 \\ 16.050 \\ 15.908 \\ 15.764 \\ 15.622 \end{array}$	15.781 15.738 15.693 15.650 15.604	1.187 1.144 1.099 1.056 1.010	3280.0 3119.6 2961.9 2806.2	405.1 388.7 372.4	6.61 6.58 6.55 6.51	$\begin{array}{c} 1247.1 \\ 1190.6 \\ 1134.5 \\ 1079.1 \\ 1024.5 \end{array}$	158.0 151.3 144.6	4.08 4.06 4.05
CB 146 14"	205 195 185 175 165	57.34 54.41 51.47 48.52	15.478 15.334 15.188 15.042 14.896	15.513 15.469 15.424 15.377	.919 .875 .830	2505.0 2358.2 2213.5 2071.7 1932.6	307.6 291.5 275.5	$6.41 \\ 6.38 \\ 6.34$	811.6		4.00 3.98 3.97
-1	155 145 135 125 115	42.64 39.70 36.75 33.82	14.750 14.602 14.452 14.304 14.154	15.284 15.239 15.191 15.145	.690 .645 .597 .551	1796.8 1662.7 1530.4 1402.1 1275.9	227.7 211.8 196.0 180.3	6.24 6.21 6.18 6.14	709.0 658.5 608.4 559.4 510.9	86.2 79.9 73.7	3.93 3.92
	131	38.52	14.162	15.468	.874	1358.4	191.8	5.94	547.3	70.8	3.77
CB 145 14"	105 95 85	27.93	$\begin{array}{c} 14.370 \\ 14.186 \\ 14.000 \end{array}$	12.050	.536 .485 .435	$1169.6\\1044.0\\921.3$	147.2	6.11	292.6 262.0 232.0		3.08 3.06 3.05
CB 144 14"	75 68 61	1,9.99	$\begin{array}{c} 14.382 \\ 14.238 \\ 14.094 \end{array}$	10.043	.468 .425 .382	823.5 738.8 656.2	103.8	6.08	$134.5 \\ 120.6 \\ 107.1$	26.7 24.0 21.4	2.46
CB 143 14''	58 53 48	17.05 15.59 14.12		8.070 8.035 8.000	.413 .378 .343	609.4 552.5 496.0	85.6 78.2 70.9	5.95	62.8 56.8 50.8	15.6 14.1 12.7	
CB 142 14"	33	10.58	14.240 14.160 14.080 14.000	6.822 6.798 6.774 6.750	.342 .318 .294 .270	431.5 398.3 365.6 333.4	$60.6 \\ 56.3 \\ 51.9 \\ 47.6$	5.89 5.88	30.2 27.7 25.4 23.0	8.2 7.5	1.56 1.56 1.55 1.54
	38	11.18	14.000	6.855	.375	357.5	51.1	5.66	24.2	7.1	1.47
CB 141 14"	30	8.82	13.964	6.000	.270	292.0	41.8	5.75	15.5		1.33

CARNEGIE BEAM SECTIONS—Continued



DIMENSIONS
OF
SECTIONS
FRACTIONAL

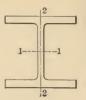


-	Veight	Depth	Fla	nge	We	eb	-]	Distance			Section
	per Foot	of Section	Width	Thick- ness	Thick- ness	½ Thick- ness +	a	c	f	0	d¹	Index and Nominal
-	Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	Depth
	305 295 285 275 265	1678 1634 1658 1642 16516	16 15 ¹⁵ / ₁₆ 15 ¹⁵ / ₁₆ 15 ⁷ / ₈ 15 ¹³ / ₁₆	21/8 21/16	138 138 1516 134 134	34 1116 1116 1116 1116 58	7546 7546 7546 7546 7546	1238 1238 1238 1238 1238 1238	11 11 11 11	278 21316 234		
	255 245 235 225 215	16146	1534 1534 15146 1558 1558	178 11316 134 11116 158	11/8	58 58 916 916 916	75/16 75/16 75/16 75/16 75/16	1238 1238 1238 1238 1238	11 11 11 11 11	2½ 2¾ 2¾ 2516	2258 2212 2238 2214 2218	
	205 195 185 175 165	15½ 15¾6 15¾6 15¼6 14¾8	15%6 15% 15% 15% 15% 15%	1916 112 138 1516 114	15/16 15/16 78 13/16	16 316 316	7516 7516 7516 7516 7516 7516	1238 1238 1238 1238 1238 1238	11 11 11 11 11	21/8 21/16	$\begin{array}{c} 21^{15/16} \\ 21^{13/16} \\ 21^{11/16} \\ 21^{9/16} \\ 21^{7/16} \end{array}$	14''
	155 145 135 125 115	1434 1458 14716 14516 1438	15516 15516 154 15316 1538	1316 138 1 1516 78	34 1116 58 58 916	3/8 3/8 3/8 5/16 5/16	7516 7516 7516 7516 7516	1238 1238 1238 1238 1238 1238	11 11 11 11 11	134	62118	
	131	14316	157/16	7/8	78	716	7516	1238	11	158	21	
	105 95 85	1438 14316 14	1238 12316 12	1 78 1316	916 32 316	516 14 14	5134	1238 6 1238 6 1238	11 11 11	1 1 ½ 1 1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½	6 181316 1858 18716	CB 145 14"
	75 68 61	1438 1434 1438	101/16 101/16 10	134 114 58		14 14 14	4134	$ \begin{array}{c} 6 & 12 \frac{3}{4} \\ 6 & 12 \frac{3}{4} \\ 6 & 12 \frac{3}{4} \end{array} $	1158 1158 1158	138 1546 134	17916 17316 17516	CB 144 14"
	58 53 48	14¼ 14⅓ 14⅓	8316 8316 8	114 58 58	716 38 516	14	378 378 378	1234 1234 1234	1158 1158 1158	1546 134 1346		CB 143 14"
	42 39 36 33	1414 14316 14116			516 516 516 54	316	31/4 31/4 31/4 31/4	1314	8 12¼ 6 12¼ 6 12¼ 6 12¼	1 1 154 78	15 ¹ 34 15 ¹ 44 161558 15946	6 CB 142 14"
	38	14	678	316		316	314	131/1	6 1234	78	1558	CD 141
	30	13154	6 6	316	14	316	278	1314	6 1214	7,8	15316	CB 141 14"

CARNEGIE BEAM SECTIONS-Continued

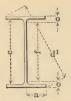


OF
SECTIONS
DECIMAL

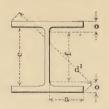


		,									-
Section Index and	Weight	Area of	Depth	Flange Width	Web Thick-	I	Axis 1-1		1	Axis 2-2	
Nominal	Foot	Section	Section		ness	I	S	r	I	S	r
Depth	Lbs.	In.2	In.	In.	In.	In.4	In.3	In.	In.4	In.3	In.
CB 127 12"	230 220 210 200 190	64.70 61.76 58.82	12.000 12.000 12.000 12.000 12.000	14.735 14.490 14.245	1.735 1.490 1.245	1426.6 1391.3 1356.1	237.8 231.9 226.0	$4.70 \\ 4.75 \\ 4.80$		121.9	3.73 3.72 3.71
CB 126 12"	180 170 160 150	50.00	$12.000 \\ 12.000 \\ 12.000 \\ 12.000$	14,490	$1.247 \\ 1.002$	1182.8	197.1 191.3	4.86	702.4 666.9 633.0 600.4	92.1 88.9	3.65 3.67
CB 125 12"	140 130 120 110	38.24 35.28	12,000 12,000 12,000 12,000	$12.491 \\ 12.245$	1.376 1.131 .885 .640	899.5 864.1	155.8 149.9 144.0 138.1	4.85 4.95	372.4 350.5 329.6 309.9	56.1	3.03
CB 124	100 91 83 75	$26.76 \\ 24.41$	$\begin{array}{c} 12.000 \\ 12.000 \\ 12.000 \\ 12.000 \\ 12.000 \end{array}$	10.392 10.196	1.121 .900 .704 .508	659.0 627.2 598.9 570.7		4.84 4.95	167.5 155.9 147.0 138.5		2.41
CB 123 12"	50 45 40	13.23	$\begin{array}{c} 12.258 \\ 12.130 \\ 12.000 \end{array}$	8.071 8.036 8.000	.361 .326 .290	400.5 356.9 313.7	65.4 58.8 52.3	5.19	57.5 51.2 44.9	$14.2 \\ 12.7 \\ 11.2$	1.97
CB 122 12"	36 32 28	9.40 8.22	$\begin{array}{c} 12.236 \\ 12.118 \\ 12.000 \end{array}$	6.568 6.534 6.500	.308 .274 .240	280.1 246.3 213.4	$45.8 \\ 40.7 \\ 35.6$	5.12	25.4 22.3 19.2	6.8	1.55 1.54 1.53
CB 121 12"	34 25		12.022 11.924	6.635	.375	238.1 183.0	39.6		21.0 13.8		1.45 1.37

CARNEGIE BEAM SECTIONS—Continued



DIMENSIONS
OF
SECTIONS
FRACTIONAL



Weight	Depth	Fla	nge	W	eb		I	Distance			Section
per Foot	of Section	Width	Thick- ness	Thick- ness	hick- ness +	a	с	f	0	d¹	Index and Nominal
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	Depth
230 220 210 200 190	12 12 12 12 12	15 1434 1434 1434 1434	1 1 1/16 1 1 1/16 1 1 1/16 1 1 1/16 1 1 1/16	134 132 134	1 38 34 58 12	6 1/2 6 1/2 6 1/2 6 1/2 6 1/2	858 858 858 858 858	7½ 7¼ 7¼ 7¼ 7¼ 7¾	238 238 238 238 238 238	19346 19 181346 1856 18716	CB 127
180 170 160 150	12 12 12 12 12	1434 1412 1414 14	1516 1516 1516 1516	1 ½ · · · · · · · · · · · · · · · · · ·	34 58 916 316	658 658 658 658	938 938 938 938	8 8 8	2 2 2 2	19 $18^{13}16$ $18^{5}8$ $18^{7}16$	CB 126
140 130 120 110	12 12 12 12 12	1234 1234 1234 1234	1316 1316 1316 1316 1316	138 138 138 38 58	34 58 12 38	511/16 511/16 511/16 511/16	91316 91316	858 858	1 1 1 1/1 e	1718	CB 125 12"
100 91 83 75	12 12 12 12	1056 1036 1036 1036	1346 1346 1346	78	916 12 38 516	434 434 434 434	10516 10516 10516 10516	9 1/4 9 1/4 9 1/4 9 1/4	13/8 13/8 13/8 13/8	16 15 78 15 34 15 58	CB 124
50 45 40	12¼ 12⅓ 12⅓	81/16 81/16 8	58 916 12	3/8 5/16 5/16	316 316 316	378 378 378	$\begin{array}{c} 10^{15}16 \\ 10^{15}16 \\ 10^{15}16 \end{array}$	9 7/8	1346 138 136	14 ¹ / ₁₆ 14 ⁹ / ₁₆ 14 ⁷ / ₁₆	CB 123
36 32 28	12¼ 12⅓ 12	6916 6916 632	916 12 316	516 14 14	316 316 18	3316 3316	11½ 11½ 11½	1038 1038 1038	78	1378 131316 131116	CB 122
34 25	111516	65%	316 38	38	316	1	111/8	1038	1	6 1334	CB 121
11_		1				1					

CARNEGIE BEAM SECTIONS—Continued

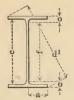


ELEMENTS
OF
SECTIONS
DECIMAL

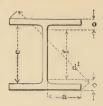


Section Index	Weight	Area of	Depth	Flange	Web Thick-	1	Axis 1-1			Axis 2-2	2
and Nominal	Foot	Section	Section	Width	ness	1	S	r	I	S	r
Depth	Lbs.	In.2	In.	In.	In.	In.4	In.3	In.	In.4	In.3	In.
CB 105 10"	140 132 124 116 108 100	$\begin{array}{c} 41.17 \\ 38.81 \\ 36.46 \\ 34.11 \\ 31.76 \\ 29.40 \end{array}$	$\begin{array}{c} 10.000 \\ 10.000 \\ 10.000 \\ 10.000 \end{array}$	13.177 12.941 12.706 12.471 12.236 12.000	1.541 1.306 1.071 .836	623.2 603.5 583.9 564.3 544.8 525.1	120.7 116.8 112.9 109.0	3.94 4.00 4.07 4.14	391.4 369.6 349.0 329.4 310.7 292.8	57.1 54.9 52.8 50.8	3.08 3.09 3.09 3.11 3.13 3.16
CB 104	92 84 77 70	$\begin{array}{c} 27.06 \\ 24.70 \\ 22.65 \\ 20.59 \end{array}$	$10.000 \\ 10.000$	$\begin{array}{c} 10.647 \\ 10.411 \\ 10.206 \\ 10.000 \end{array}$.926 .721	423.2 403.6 386.5 369.3	$80.7 \\ 77.3$	3.96 4.04 4.13 4.24	163.1 152.0 142.9 134.3	$\frac{29.2}{28.0}$	2.50 2.48 2.51 2.55
CB 103	63 56 49	18.53 16.47 14.41	10.000 10.000 10.000	9.206	.581	$300.4 \\ 283.2 \\ 266.0$	56.6	$4.03 \\ 4.15 \\ 4.30$	79.5	18.1 17.3 16.5	2.14 2.20 2.27
CB 102 10"	42 36 31	$12.35 \\ 10.58 \\ 9.11$	10.000 10.000 10.000		.644 .467 .320	190.4 175.6 163.4	35.1	4.07	36.8 34.4 32.5	8.9 8.5 8.1	1.73 1.80 1.89
CB 101	30 26 23	8.82 7.64 6.76	$\begin{array}{c} 10.228 \\ 10.098 \\ 10.000 \end{array}$	6.029 6.000	.298 .259 .230	$163.2 \\ 139.5 \\ 122.2$	27.6	$4.30 \\ 4.27 \\ 4.25$	18.5 15.7 13.7	$6.1 \\ 5.2 \\ 4.6$	$1.45 \\ 1.43 \\ 1.43$
CB _{9''} 93	21 48 43 38	6.17 14.11 12.65 11.17	9.902 9.242 9.122 9.000	9.082 9.041	.398	107.6 221.1 195.5 170.4			73.8 65.4 57.1		1.39 2.29 2.28 2.26
CB _{9''} 92	35 32 29	10.29 9.40 8.53	9.192 9.096 9.000	6.528	.307	155.4 140.5 126.0	33.8 30.9 28.0	3.87	$26.6 \\ 24.0 \\ 21.5$	8.1 7.4 6.6	1.61 1.60 1.59

CARNEGIE BEAM SECTIONS—Continued



DIMENSIONS OF SECTIONS FRACTIONAL

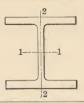


Weight	Depth	Fla	inge	W	eb		Ι	Distance			Section
per Foot	of Section	Width	Thick- ness	Thick- ness	h Thick- ness +	a	с	f	0	d¹	Index and Nominal
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	Depth
140 132 124 116 108 100	10 10 10 10 10 10	$13\frac{4}{6}$ $12\frac{15}{16}$ $12\frac{1}{16}$ $12\frac{1}{4}$ $12\frac{1}{4}$ 12	1 · 1 · 1 · 1 · 1 · 1 · 1 · 1 · 1	134 1916 1516 1116 1316	15/16 13/16 11/16 9/16 3/16 5/16	534 534 534 534 534 534	715/16 715/16 715/16 715/16 715/16 715/16	634 634 634 634	158 158 158 158 158 158	16946 1638 16346 16 151346 1558	CB 105
92 84 77 70	10 10 10 10	1058 10346 10346 10	13/16 13/16 13/16 13/16	1316 1516 34 15	58 12 38 516	434 434 434 434	836 836 836 836	738 738 738 738	15/16 15/16 15/16 15/16	$14\frac{5}{8}$ $14\frac{7}{16}$ $14\frac{5}{16}$ $14\frac{3}{16}$	CB 104 10"
63 56 49	10 10 10	9716 9316 9	58 58 58	1316 916 38	716 516 316	4516 4516 4516	834 834 834	738 738 738	11/16	1334 1356 1312	CB 103 10"
42 36 31	10 10 10	8516 818 8	38 38 38	58 716 516	36 14 316	376 376 378	9316 9316 9316	856 858 858	11/16	$13\frac{1}{1}6$ $12\frac{1}{5}$ $12\frac{1}{5}$ $12\frac{1}{5}$	CB 102 10"
30 26 23	10¼ 10⅓ 10	6 14 6 6 6	1/2 7/16 3/8	516 14 14	316 316 18	$2^{15/16}$ $2^{15/16}$ $2^{15/16}$	9316 9316 9316	858 858 858	34	$11^{15/6}$ $11^{13/6}$ $11^{1/6}$	OD 101
21	938	6	516	1/4	38	215/16	9316	858	5/8	115%	
48 43 38	91/4 91/8 9	91/16 91/16 9	916 12 12	3/8 3/8 5/16	1/4 3/16 3/16	438 438 438	8 8 8	7 7 7	1 1/8 1 1/16 1	13 1278 1234	CB 93
35 32 29	9316 938 9	6946 612 612	916 12 12	516 518 14	316 316 316	31/8 31/8 31/8	8 8 8	7 7 7	1 1/8 1 1/1 6 1	115/16 113/16 113/8	CB _{9"} 92

CARNEGIE BEAM SECTIONS—Continued



OF
SECTIONS
DECIMAL



Section Index	Weight	Area of	Depth	of Width		A	xis 1-1		Axis 2-2			
and Nominal	Foot	Section	Section	1110011	ness	I	S	r	I	S	r	
Depth	Lbs.	In.2	In.	In.	In.	In.4	In.3	In.	In.4	In.3	In.	
	90 84 78 72 66	26.47 24.71 22.93 21.17 19.40	9.606 9.456 9.302 9.150 8.994	8.520 8.469 8.418 8.366 8.314	.759	391.2 358.6 326.5 295.9 265.9	75.8 70.2 64.7	3.81	124.4 114.5 104.7 95.3 86.1	27.0 24.9 22.8	2.17 2.15 2.14 2.12 2.11	
CB 83 8"	60 54 48 42 36 31	17.63 15.87 14.10 12.34 10.58 9.10	8.838 8.680 8.520 8.360 8.198 8.060	8.261 8.208 8.155 8.100 8.046 8.000	.551 .498 .445 .390 .336	237.1 209.2 182.2 156.2 131.3 110.9	48.2 42.8 37.4 32.0	3.67 3.63 3.59 3.56 3.52 3.49	68.3 59.7 51.4	18.7 16.6 14.6 12.7 10.8 9.2	2.09 2.07 2.06 2.04 2.02 2.01	
CB 82	30 27 24	8.81 7.93 7.06	8.196 8.098 8.000	6.559 6.529 6.500	.298 .268 .239		$26.3 \\ 23.7 \\ 21.1$	3.50 3.48 3.46		6.4	1.63 1.62 1.61	

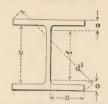
STANDARD MILL SECTIONS

Section Index	Weight	Area	Depth	Flange Width	Web Thick-	1	xis 1-1		Axis 2-2			
and Nominal	Foot	Section	Section	** 161 011	ness	I	S	r	I	S	r	
Depth	Lbs.	In.2	In.	In.	In.	In.4	In.3	In.	In.4	In.3	In.	
B 40 9"	$\frac{25}{21}$	7.34 6.17	9.000	5.380 5.250	.380 .250		$\frac{21.2}{19.5}$	$\frac{3.61}{3.77}$	8.8 8.1	3.3 3.1	1.09 1.14	
B 39 8''	21 18	6.17 5.29	8.000 8.000	$5.110 \\ 5.000$.360 ,250		$15.9 \\ 14.7$	3.21 3.33	6.6 6.1	$\frac{2.6}{2.4}$	1.03 1.07	
H 4 8"	37.7 34.3 32.6	11.00 10.00 9.50	8.000 8.000 8.000	$8.125 \\ 8.000 \\ 7.938$.500 .375 .313	$120.8 \\ 115.5 \\ 112.8$	28.9	$3.31 \\ 3.40 \\ 3.45$	$36.9 \\ 35.1 \\ 34.2$	9.1 8.8 8.6	1.83 1.87 1.90	
H 3A 6"	27.5 25.0	8.08 7.33	6.000 6.000	6.063 5.938	.438 .313		$16.4 \\ 15.7$	$\frac{2.47}{2.53}$	16.0 14.9	5.3 5.0	1.41 1.43	
H 3	22.5 20.0	6.61 5.86	6.000	6.063 5.938	.375 .250		$13.7 \\ 12.9$	$\frac{2.49}{2.57}$	12.2 11.4	$\frac{4.0}{3.8}$	1.36 1.39	
H 2 5"	18.9	5.47	5.000	5.000	.313	23.8	9.5	2.08	7.8	3.1	1.20	
H 1	13.8	3.99	4.000	4.000	.313	10.7	5.3	1.64	3.6	1.8	0.95	

CARNEGIE BEAM SECTIONS-Concluded



DIMENSIONS
OF
SECTIONS
FRACTIONAL

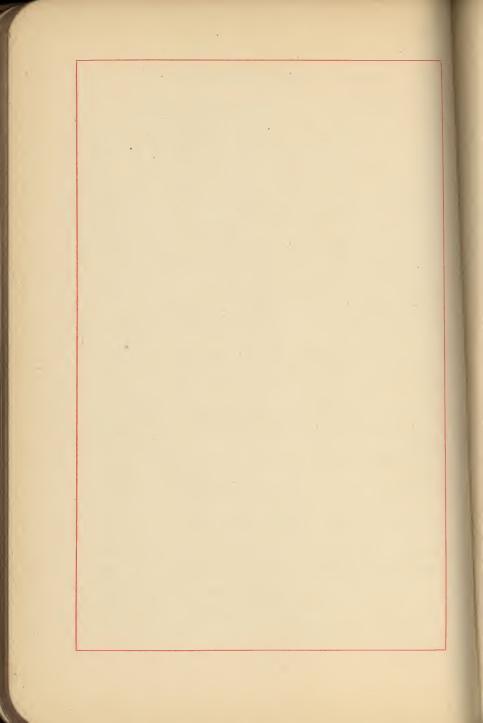


Weight	Depth	Fla	nge	W	eb			Distance	e		Section
per Foot	of Section	Width	Thick- ness	Thick- ness	½ Thick- ness+	a	С	f	0	d1	Index and Nominal
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	Depth
90 84 78 72 66 60 54 48 42 36 31	958 9716 9516 9516 918 9 81316 81116 812 838 8316		1316 138 1316 136 1316 34 1316 34 1316 316 136 34 1316 34 34 34 34 34 34 34 34 34 34 34 34 34	1,6	716 716 36 36 38 516 516 14 14 14 316	376 376 376 376 376 376 376 376 376 376	7316 7316 7316 7316 7316 7316 7316 7316	614 614 614 614 614 614 614 614 614 614	1946 1746 138 1546 144 148 146	1278 1234 12946 12746 1234 1238 11346 11346 11346 11346 11346	
30 27 24	8316 838 8.	6916 612 612	746 348	516 14 14	316 316 38	3316 3316 3316	7316 7316 7316	6 1/4 6 1/4 6 1/4	15/16	10½ 10¾6 10¾6	CB 82 8"

STANDARD MILL SECTIONS

Weight	Depth	Fla	nge	W	eb			Distanc	е		Section
per Foot	of Section	Width	Thick- ness	Thick- ness	½ Thick- ness+	a	С	f	0	d¹	Index and Nominal
Lbs.	In.	In.	In.	In.	In.	In.	In.	In.	In.	In.	Depth
$\frac{25}{21}$	9	538 514	38 38	38 1/4	14 18	2½ 2½ 2½		7½ 7½ 7½	3/4 3/4	10½ 10¾6	B 40 9"
21 18	8 8	51/8 5	516 516	3/8 1/4	316 38	238 238		658 658	11/16 11/16	9½ 9¾6	B 39 8"
37.7 34.3 32.6	8 8 8	838 8 71516	716 716 716	75 36 516	1/4 3/16 3/16	313/16 313/16 313/16		6 1/4 6 1/4 6 1/4	78 78 78 78	11716 11516 1114	H 4 8"
$27.5 \\ 25.0$	6	61/16 515/16	1/2 1/2	716 516	34 316	$\frac{21316}{21316}$		4¼ 4¼	78 78	8916 8½	H 3A 6"
$\frac{22.5}{20.0}$	6	61/16 515/16	38 38	38 14	31 s 38	278 278		4316 4316	34 34	8916 812	H 3 6"
18.9	5	5	716	516	316	238		338	13/16	71/16	H 2 5"
13.8	4	4	3/8	516	316	1 7/8	,	21/2	34	511/16	TT a

Dimensions for Flange Thickness of Standard Mill Sections are the averages between dimensions of toe and root of Flanges.



BEAM AND COLUMN SAFE LOADS

in accordance with Specifications of

AMERICAN INSTITUTE OF STEEL CONSTRUCTION—1923

SAFE LOADS FOR SECTIONS USED AS BEAMS

EXPLANATION OF TABLES

Tables of safe loads for Carnegie Beam Sections used as beams under conditions of static transverse loading, give the uniformly distributed safe loads in thousands of pounds for spans customary in bridge and building construction, based upon an extreme fiber stress of 18,000 pounds per square inch. These tables give the full loads for beams fixed or braced against lateral deflection as well as the reduced loads allowed for beams free or unbraced against side deflection, and also the values for those spans at which the allowed safe load will produce a deflection of ½60 of the span length. The loads in all cases include the weight of the section, which should be deducted in order to arrive at the net load which the section will support.

It is assumed in all cases that the loads are applied normal to the axis 1-1 as shown in the tables of elements of sections, and that the beam deflects vertically in the plane of bending only. If the conditions of loading involve the introduction of forces outside this plane of loading, the allowable safe loads must be determined from the general theory of flexure, in accordance with the mode of application of the load and its character. In cases of eccentric loading, the actual safe loads would be considerably lower than the tabulated safe loads which have been based upon the most favorable conditions of loading.

Vertical Deflection. The vertical deflection of a section under a uniformly distributed load is determined from formula:

Deflection, D=
$$\frac{5}{384} \frac{\text{Wl}^3}{\text{EI}}$$
; Wl=8 f $\frac{\text{I}}{\text{n}}$
" D= $\frac{40}{384} \frac{\text{fl}^2}{\text{En}}$; Span length in feet: l=12L

"
$$D = \frac{15 \text{ fL}^2}{\text{En}} \text{ inches}$$

Steel, E=29,000,000; for fiber stress f=18,000 pounds:

Deflection,
$$D = \frac{0.01862L^2}{2n}$$

n-distance from center line of gravity to extreme fiber:

$$Deflection = \frac{Coefficient}{2n}$$

Deflection Coefficients for Fiber Stress of 18,000 Pounds

Span, Feet	Coefficient 18,000	Span, Feet	Coefficient 18,000	Span, Feet	Coefficient 18,000	Span, Feet	Coefficient 18,000
1	0.019	16	4.767	31	17.894	46	39.401
2	0.074	17	5.381	32	19.068	47	41.133
3	0.168	18	6.033	33	20.278	48	42.902
4	0.298	19	6.722	34	21.526	49	44.708
5	0.466	20	7.448	35	22.810	50	46.552
6	0.670	21	8.212	36	24.132	51	48.432
7	0.912	22	9.012	37	25.492	52	50.350
8	1.192	23	9.850	38	26.888	53	52.306
9	1.508	24	10.726	39	28.322	54	54.298
10	1.862	25	11.638	40	29.793	55	56.328
11	2,253	26	12.588	41	31.301	56	58.395
12	2.681	27	13.574	42	32.847	57	60.499
13	3.147	28	14.599	43	34.430	58	62.640
14	3.650	29	15.660	44	36.050	59	64.819
15	4.190	30	16.759	45	37.707	60	67.035

The deflection, in inches, of sections subjected to transverse stresses due to uniformly distributed loads are obtained as follows:

Symmetrical Sections. To find the deflection in inches of a section symmetrical about the neutral axis, such as I- and H-beams, divide the coefficient in the table corresponding to given span and fiber stress by the depth of the section in inches.

Unsymmetrical Sections. To find the deflection in inches of a section not symmetrical about the neutral axis, such as beams with unbalanced flange plates or with continuous shelf angles, divide the coefficient corresponding to given span and fiber stress by twice the distance of extreme fiber from neutral axis obtained by computation.

Other Fiber Stresses. To find the deflection of any section for other fiber stresses than those given, multiply the coefficient for 18000 pounds fiber stress corresponding to the span given by the ratio of desired fiber stress and 18000.

Limits of Deflection. The deflection of floor beams carrying plastered ceilings should be limited to not more than ½60 of the span length; this limit is indicated in the safe load tables by lower zigzag line, is derived from the following formulas:

Deflection, $D_{\text{max}} = \frac{12L}{360} = \frac{15fL^2}{En}$ Limiting Span, $L_{\text{max}} = \frac{En}{450f}$ for fiber stress of 18,000, Limiting Span, $L_{\text{max}} = 3.580n$

Lateral Deflection of Beams. In computing safe loads it is generally assumed that the compression flanges of the sections are secured against lateral deflection by the use of tie rods or by other means.

In such cases full safe loads may be used up to a span length equal to fifteen times the flange width, but when the unbraced length exceeds this ratio, the full safe loads must be reduced in accordance with the ratios given in the following table in order to insure that the stresses in the compression flanges do not exceed the safe unit stress. The lateral unbraced length of beams and girders should not exceed forty times the width of the compression flanges.

The following table gives values obtained from formula of American Institute of Steel Construction: $f_{C} = \frac{20,000}{1 + \frac{1}{2000} (1/b)^2}$

Reduction of Safe Loads for Ratio of Span Length to Flange Width, 1/b.

Ratio, 1/b	Full Lead, Per Cent.	Ratio, 1/b	Full Load, Per Cent.	Ratio, 1/b	Full Lead, Per Cent.	Ratio, 1/b	Full Load, Per Cent.
		21	91.0	27.5	80.6	34	70.4
15	99.9	21.5	90.3	28	79.8	34.5	69.7
15.5	99.2	22	89.5	28.5	79.0	35	68.9
16	98.5	22.5	88.7	29	78.2	35.5	68.2
16.5	97.8	23	87.9	29.5	77.4	36	67.4
17	97.1	23.5	87.1	30	76.6	36.5	66.7
17.5	96.4	24	86.3	30.5	75.8	37	66.0
18	95.6	24.5	85.5	31	75.1	37.5	65.2
18.5	94.9	25	84.7	31.5	74.3	38	64.5
19	94.1	25.5	83.9	32	73.5	38.5	63.8
19.5	93.4	26	83.0	32.5	72.7	39	63.1
20	92.6	26.5	82.2	33	71.9	39.5	62.4
20.5	91.8	27	81.4	33.5	71.2	40	61.7

In addition to this lateral deflection which is induced within the beam by the action of vertical loading, lateral deflection may be induced by the thrust of floor arches or other loading acting on an axis perpendicular to the line of principal bending stress.

Stresses due to horizontal thrust should either be neutralized by tie rods, or the safe carrying capacity of the beam should be computed in accordance with the general formulas of flexure to provide for the combined stresses due to the action of both vertical and horizontal forces; that is to say, the safe loads should be figured around both the axes 1-1 and 2-2, and the unit stress computed so as not to exceed the allowable fiber stress.

Effect of Impact on Stresses. The formulas upon which the tables of safe loads are based assume all loads to be quiescent or static. The effect of moving loads may be taken care of either by reducing the allowable unit stresses, or else by increasing the theoretical loads.

When a load is suddenly applied, the resultant stresses are twice as great as those due to an equal quiescent load.

When an instantaneously applied load produces impact or percussion, the resultant stresses are dynamic and are measured by the laws governing the energy of bodies in motion. The following formulas give the fiber stress and deflection due to a load falling on center of a beam rigidly supported at both ends when the weight of beam is negligible as compared with that of falling load, and when no account is taken of the local distortion due to impact or percussion at point of application of load; but when the weight of the beam is a real factor, theoretical formulas do not agree with observed results and practical tests give values which are far less than those indicated by theoretical formulas; this is notably true in drop-tests of axles:

W =Weight of falling load, in pounds.

h =Height of fall, in inches.

f =Extreme fiber stress due to static effect of load, W, in pounds per square inch.

fd =Extreme fiber stress due to impact of load, W, in pounds per square inch.

D =Deflection due to static effect of load, W, in inches. Dd=Deflection due to impact of load, W, in inches.

$$f_d = f (1 + \sqrt{\frac{2h}{D} + 1})$$
 $D_d = D (1 + \sqrt{\frac{2h}{D} + 1})$

shearing Stresses. The safe load tables for beams are computed solely with reference to safe unit stresses due to flexure, and the safe loads uniformly distributed on the spans given will not produce excessive shearing stresses in the web.

When, however, beams must support heavy loads which are concentrated near the supports, or when beams of short span are loaded with uniformly distributed loads to their full carrying capacity as regards flexure, the bending moments may be small in comparison with the reactions at the supports, and the beams may fail along the neutral plane as a result of longitudinal shearing stresses, or may buckle as a result of the combined longitudinal and vertical web stresses. On such spans the safe shearing or buckling strength of the web may limit the carrying capacity of the beam, so that the deciding factor will often be the resistance of the web to shearing stresses, rather than the resistance of the flanges to bending stresses.

Longitudinal Shear. At any point in any section of a beam, the horizontal and vertical components of the web stress are equal to each other and proportional to the vertical shear; their intensities are dependent upon the distance of the point from the neutral axis. In order to determine the intensity of the vertical shearing stress at a given point in a vertical section of the beam, therefore, it is sufficient to find the equal intensity of the horizontal shearing stress at the same point in the horizontal plane.

The longitudinal unit shear is zero at the upper and lower flanges of the beam and a maximum at the neutral plane. It is greatest at the supports and zero where there is no vertical shear.

The intensity of the longitudinal shear at any point in any section is the product of the vertical shear, V, for that section and the static moment, Ms, of the section included between the horizontal plane of shear through that point and the extreme fibers on the same side of the neutral plane divided by the product of the moment of inertia of the beam around the proper axis and the thickness at the plane of shear; or

 $Longitudinal\ shear\ per\ square\ inch=\frac{V\ Ms}{t\ I}\cdot$



Example—Required the maximum longitudinal unit shear in Carnegie Beam Section CB-302, 30" x 14", 180 lb. for a maximum vertical shear of 241,200 pounds.

 M_8 of Flange = 14 x 1.2065 x 14.397 = 243.2 M_8 of Web = 13.794 x 0.67 x 6.897 = 63.7

Total Static Moment 306.9 in.3

Moment of Inertia of Beam, $I = 8301.4 \text{ in.}^4$ Longitudinal Shear $= \frac{241200 \times 306.9}{8301.4 \times 0.67}$

= 13,310 pounds per square inch.

Under usual conditions of loading, the longitudinal shear need not be taken into consideration.

Buckling Values of Beam Webs. The vertical shearing stresses or the vertical compressive components of the web stress may, under some conditions, exceed the safe resistance of the beam to buckling, and there remains the possibility that a web which is amply secure as against the safe allowed shear will not be of sufficient strength when considered as a column. In such cases provision must be made for security against buckling either by web stiffeners or by increasing the thickness of the web.

Experiments with beams of various depths and web thicknesses have demonstrated that the length of the web which can be assumed to resist buckling stresses is equal to the end bearing plus one fourth of the depth of the beam; the following formulas have been deduced:

Safe end reaction
$$R = f_b x t (a + \frac{d}{4})$$

Safe interior load $W = 2f_b x t (a^1 + \frac{d}{4})$

In the formulas R is the end reaction, W the concentrated load, t the web thickness, d the depth of the beam, a¹ half the distance over which the concentrated load is applied, a the whole distance over which the end reaction is applied, and fb is the safe unit resistance of the web to buckling.

The first formula is general and applies to any condition of loading. The second formula is for a single load concentrated at the center of a span; it can be extended for a system of concentrated loads, provided the sum of the distances a¹ is not less than a.

For computation of f_b the following formula has been used in the tables, corresponding to an allowable shearing stress of 12,000 pounds, f_b maximum = 15,000 pounds.

$$f{=}\frac{18000}{1{+}\frac{1}{18000}\,(l/r)^2}\,,\;\;l{=}\frac{1}{2}d\;\;{\rm and}\;\;r^2{=}\frac{1}{12}t^2,\;\;f_b{=}\frac{18000}{1{+}\frac{1}{6000}\,(d/t)^2}$$

The tables give for beams with unsupported webs:

1. Allowed web resistance f_b , in pounds per square inch, computed from this compression formula.

2. The distance a, or the distance over which the end reaction must be distributed when the shearing stress, V, in the web is the maximum allowable of 12,000 pounds per square inch.

3. The allowable end reaction (R) when a is taken at $3\frac{1}{2}$ ", which is the usual length of beam actually resting on the 4" angles ordinarily used in building construction for beam seats.

4. The allowable shear V, on the gross area of beam webs at 12,000 pounds per square inch.

Maximum Bending Moments. In addition to data referring to maximum loads on beams as computed from the web resistance, these tables also give the maximum bending moments in foot pounds, which may be used instead of the table of properties, to ascertain the proper size section to be used in any particular instance.

CARNEGIE BEAM SECTIONS

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 18,000 Pounds—Shearing Stress 12,000 Pounds

	1			1	77.3	4 7	1.50		
	Depth	Weight	Web	Maximum			d Reactio		End
Section	of Beam	per Foot	Thick- ness	Bending Moment	. Web Sh	-	Web B		Reaction
Index and Nominal		1000	ness	Woment	End Reaction	Span Limit	Unit Stress	End Bearing	a=3½"
Depth	d		t	M max.	V max.	L min.	fb	a min.	R max.
	Inches	Pounds	Inches	Foot Pounds	Pounds	Feet	Pounds per Sq.In.	Inches	Pounds
CB 302 30'	30.781 30.522 30.263 30.000	240 220 200 180	.888 .816 .743 .670	1106,850 1014,450 922,500 830,100	328,000 298,870 269,820 241,200	13.50 13.58 13.68 13.77	14,997 14,596 14,101 13,492	16.93 17.46 18.19 19.18	149,090 132,570 115,940 99,440
CB 301 30"	30.298 30.148 30.000	135 125 115	.621 .576 .530	584,850 541,500 498,600	225,780 208,380 190,800	10.36 10.39 10.45	12,887 12,358 11,734	20.64 21.74 23.18	88,630 78,560 68,410
CB 272 27"	27.598 27.400 27.200 27.000	190 175 160 145	.756 .698 .639 .580	801,900 738,750 675,150 612,150	$\begin{array}{c} 250,370 \\ 229,500 \\ 208,570 \\ 187,920 \end{array}$	$\begin{array}{c} 12.81 \\ 12.88 \\ 12.95 \\ 13.03 \end{array}$	14,729 14,322 13,825 13,224	15.59 16.11 16.81 17.75	$115,800 \\ 103,470 \\ 90,990 \\ 78,620$
CB 271 27"	27.340 27.166 27.000	112 101 91	.566 .510 .461	439,800 397,050 357,450	185,690 166,260 149,360	9.47 9.55 9.57	12,960 12,221 11,453	18.48 19.88 21.54	75,810 64,140 54,120
CB 244 24"	24.664 24.526 24.388 24.250	160 150 140 130	.670 .629 .588 .547	616,200 577,350 538,800 500,400	198,300 185,120 172,080 159,180	$\begin{array}{c} 12.43 \\ 12.47 \\ 12.52 \\ 12.57 \end{array}$	14,684 14,361 13,989 13,559	13.99 14.36 14.82 15.40	95,100 87,000 78,940 70,920
CB 243 24"	24.310 24.156 24.000	120 110 100	.539 .494 .450	452,850 415,200 377,550	157,240 143,200 129,600	11.52 11.60 11.65	13,443 12,871 12,211	15.62 16.48 17.59	69,400 60,650 52,200
CB 242 24"	24.308 24.154 24.000	94 85 76	.499 .452 .405	337,500 305,250 273,000	145,560 131,010 116,640	9.27 9.32 9.36	12,899 12,196 11,354	16.54 17.73 19.37	61,640 52,580 43,680
CB ·241 24"	24.000	70	.400	244,200	115,200	8.48	11,250	19.60	42,750
CB 213	21.248 21.126 21.000	$\begin{array}{c c} 120 \\ 112 \\ 104 \end{array}$.535 .499 .465	408,150 381,150 353,550	136,410 126,500 117,180	$\begin{array}{c} 11.97 \\ 12.05 \\ 12.07 \end{array}$	14,253 13,860 13,434	12.58 13.01 13.51	67,190 60,730 54,660
CB 212 21"	21.240 21.120 21.000	92 86 80	.502 .470 .438	294,750 275,400 256,350	127,950 119,120 110,380	9.21 9.25 9.29	13,864 13,468 13,014	13.07 13.54 14.11	61,320 55,580 49,880
CB 211 21"	21.248 21.126 21.000	70 64 58	.433 .396 .360	199,350 180,450	110,400 100,390 90,720	7.89 7.94 7.96	12,845 12,209 11,486	14.54 15.48 16.69	49,010 42,460 36,180
1	21.034	60	.375	186,150	94,650	7.87	11,808	16.12	38,780

CARNEGIE BEAM SECTIONS—Continued

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 18,000 Pounds—Shearing Stress 12,000 Pounds

					Value	for End	Reaction	ı, V	
	Depth	Weight	Web Thick-	Maximum Bending	Web Sh	earing	Web Bu	ickling	End Reaction
Section Index and	of Beam	Foot	ness	Moment	End Reaction	Span Limit	Unit Stress	End Bearing	a=3½"
Nominal Depth	d		t	M max.	V max.	L min.	fb	a min.	R max.
	Inches	Pounds	Inches	Foot Pounds	Pounds	Feet	Pounds perSq.In.	Inches	Pounds
CB 183	18.238 18.120 18.000	100 93 86	.498 .463 .429	293,400 272,850 252,300	108,990 100,670 92,660	10.77 10.84 10.89	14,711 14,340 13,917	10.32 10.63 11.02	59,040 53,310 47,760
CB 182	18.242 18.110 18.000	78 72 67	.471 .436 .406	216,900 200,100 186,150	103,100 94,750 87,700	8.41 8.45 8.49	14,400 13,980 13,558	10.64 11.02 11.43	54,670 48,930 44,040
CB 181	18.252 18.114 18.000	58 52 47	.393 .354 .320	157,950 141,600 128,100	86,080 76,950 69,120	7.34 7.36 7.41	13,240 12,531 11,785	11.98 12.82 13.83	41,950 35,610 30,170
10	18.024	51	.375	134,850	81,110	6.65	12,996	12.14	39,020
CB 165 16"	16.236 16.110 16.000	115 107 100	.532 .496 .464	307,800 286,200 267,450	103,650 95,890 89,090	11.88 11.94 12.01	15,000 15,000 15,000	8.93 8.86 8.80	60,320 56,000 52,200
CB 164 16"	16.240 16.120 16.000	90 83 76	.495 .458 .419	235,650 217,350 199,050	96,470 88,600 80,450	9.77 9.81 9.90	15,000 14,920 14,481	8.93 8.94 9.26	56,130 51,450 45,510
CB 163 16"	16.226 16.114 16.000	68 63 58	.438 .406 .375	170,850 158,250 145,650	85,280 78,510 72,000	8.01 8.06 8.09	14,649 14,257 13,810	9.24 9.54 9.90	48,480 43,580 38,840
CB 162	16.254 16.128 16.000 15.934	45 40	.362 .326 .290 .375	122,850 110,700 98,400 98,550	55,680	7.02 7.07	13,473 12,785 11,942 13,836	11.11 12.08	36,890 31,390 25,970 38,830
CB 161 16"	16.012 15.930		.314	88,950 82,050			12,558 11,977		
CB 145	14.370 14.186 14.000	95	.536 .485 .435	244,200 220,800 197,400	82,560	10.70		7.80	
CB 144	14.382 14.238 14.094	68	.468 .425 .382	171,750 155,700 139,650	72,610	8.58		7.83	
CB 143	14.242 14.122 14.000	53	.413 .378 .343	128,400 117,300 106,350	64,060	7.32	14,603	8.07	38,810

CARNEGIE BEAM SECTIONS—Continued

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 18,000 Pounds—Shearing Stress 12,000 Pounds

						s for En	d Reaction	n, V	
Section	Depth	Weight	Web Thick-	Maximum Bending	Web Sh	earing	Web B	uckling	End Reaction
Index and Nominal	Beam	Foot	ness	Moment	End Reaction	Span Limit	Unit Stress	End Bearing	a=3½
Depth	d		t	M max.	V max.	L min.	fb	a min.	Rmax
	Inches	Pounds	Inches	Foot Pounds	Pounds	Feet	Pounds perSq.In.	Inches	Pound
CB 142 14"	14,240 14,160 14,080 14,000	42 39 36 33	.342 .318 .294 .270	90,900 84,450 77,850 71,400	58,440 54,030 49,670 45,360	6.22 6.25 6.27 6.30	13,965 13,529 13,022 12,430	8.68 9.02 9.46 10.02	33,72 30,29 26,88 23,49
	14.000	38	.375	76,650	63,000	4.87	14,607	8,00	38,34
CB 141 14"	13.964	30	.270	62,700	45,240	5.54	12,450	9.97	23,50
CB 124	12.000 12.000 12.000 12.000	100 91 83 75	1.121 .900 .704 .508	164,700 156,750 149,700 142,650	161,420 129,600 101,380 73,150	4.08 4.84 5.91 7.80	15,000 15,000 15,000 15,000	6.60 6.60 6.60 6.60	109,36 87,78 68,64 49,58
CB 123 12"	12.258 12.130 12.000	50 45 40	.361 .326 .290	98,100 88,200 78,450	53,100 47,450 41,760	7.39 7.43 7.51	15,000 14,625 14,004	6.74 6.92 7.28	35,58 31,14 26,40
CB 122	12.236 12.118 12.000	36 32 28	.308 .274 .240	68,700 61,050 53,400	45,220 39,840 34,560	6.08 6.13 6.18	14,251 13,575 12,706	7.24 7.68 8.33	28,79 24,29 19,89
	12.022	34	.375	59,400	54,100	4.39	15,000	6.61	36,59
CB 121 12"	11.924	25	.240	46,050	34,340	5.36	12,753	8.24	19,8
CB 103	10.000 10.000 10.000	63 56 49	.787 .581 .375	90,150 84,900 79,800	94,440 69,720 45,000	$\frac{3.82}{4.87}$ $\frac{3.82}{7.09}$	15,000 15,000 15,000	5.50 5.50 5.50	70,83 52,29 33,75
CB 102 10"	10.000 10.000 10.000	42 36 31	.644 .467 .320	57,150 52,650 49,050	77,280 56,040 38,400	$2.96 \\ 3.76 \\ 5.11$	15,000 15,000 15,000	5.50 5.50 5.50	57,90 42,03 28,80
CB-101 10"	10.228 10.098 10.000	30 26 23	.298 .259 .230	47,850 41,400 36,600	36,570 31,380 27,600	5.23 5.28 5.30	15,000 14,362 13,688	5.63 5.91 6.27	27,0° 22,4° 18,89
	9.902	21	.230	32,550	27,330	4.76	13,752	6.17	18,90

CARNEGIE BEAM SECTIONS—Concluded

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 18,000 Pounds—Shearing Stress 12,000 Pounds

						s for En	d Reactio	n, V	
Section	Depth	Weight	Web Thick-	Maximum Bending	Web Sh	earing	Web B	uckling	End Reaction
Index and	Beam	Foot	ness	Moment	End Reaction	Span Limit	Unit Stress	End Bearing	a=3½"
Nominal Depth	d		t	M max.	V max.	L min.	fb	a min.	Rmax.
	Inches	Pounds	Inches	Foot Founds	Pounds	Feet	Pounds per Sq.In.	Inches	Pounds
CB 93	9.242 9.122 9.000	48 43 38	.398 .357 .316	71,700 64,350 56,850	44,140 39,080 34,130	6.50 6.59 6.66	15,000 15,000 15,000	5.08 5.02 4.95	34,690 30,950 27,250
CB 92 9"	9.192 9.096 9.000	35 32 29	.335 .307 .279	50,700 46,350 42,000	36,950 33,510 30,130	5.49 5.53 5.58	15,000 15,000 15,000	5.06 5.00 4.95	29,130 26,590 24,060
CB 83	8.360 8.198 8.060	42 36 31	.390 .336 .290	56,100 48,000 41,250	39,120 33,050 28,050	5.74 5.81 5.88	15,000 15,000 15,000	4.60 4.51 4.43	32,700 27,970 23,990
CB 82 8"	8.196 8.098 8.000	30 27 24	.298 .268 .239	39,450 35,550 31,650	29,310 26,040 22,940	5.38 5.46 5.52	15,000 15,000 15,000	4.51 4.45 4.40	24,800 22,210 19,720

STANDARD MILL SECTIONS

B 40 9"	9.000	25 21	.380 .250	31,800 29,250	41,040 27,000	3.10 4.33	15,000 14,803	$\frac{4.95}{5.05}$	32,770 21,280
B 39 8"	8.000 8.000	21 18	.360 .250	23,850 22,050	34,560 24,000	$\frac{2.76}{3.68}$	15,000 15,000	4.40 4.40	29,700 20,620
H ·4 8"	8.000 8.000 8.000	37.7 34.3 32.6	.500 .375 .313	45,300 43,350 42,300	48,000 36,000 30,050	3.78 4.82 5.63	15,000 15,000 15,000	4.40 4.40 4.40	41,250 30,940 25,820
H 3-A	6.000	27.5 25.0	.438 .313	24,600 23,550	31,540 22,540	3.12 4.18	15,000 15,000	3.30 3.30	32,850 23,480
H 3 6"	6.000	22.5 20.0	.375 .250	$20,550 \\ 19,350$	27,000 18,000	3.04 4.30	15,000 15,000	3.30 3.30	28,130 18,750
H 2	5.000	18.9	.313	14,250	18,780	3.04	15,000	2.75	22,300
H 1 4"	4,000	13.8	.313	7,950	15,020	2.12	15,000	2.20	21,130

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

	1		No	minal	Dept	h and	Flang	ge Wie	lth—\	Veigh	t per l	Foot		-	
Span			CB	302	30′′x	14"				СВ	301	30′′x1	01/2"		ent
in Feet	240	lbs.	220	lbs.	200	lbs.	180	lbs.	135	lbs.	125	lbs.	115	lbs.	Coefficient of Deflection
1000	-	1 -	1	1	rally	,						erally			ರೆ ಗೆ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed 452	Free 452	Fixed 417		Fixed 382	Free 382	
11									425	425	394	$\frac{417}{394}$	363	363	2.253
12 13	656	656	598	598	540	540	482	482	390 360	390 360	361 333	361 333	$\frac{332}{307}$	332 307	2.681 3.147
14 15	632 590	$\frac{632}{590}$	$\frac{580}{541}$	$\frac{580}{541}$	$\frac{527}{492}$	$\frac{527}{492}$	474 443	$\frac{474}{443}$	334 312	330 303	309 289	$\frac{305}{280}$	$\frac{285}{266}$	$\frac{281}{257}$	3.650
16	553	553	507	507	461	461	415	415	292	279	271	258	249	237	4.190
17 18	$\frac{521}{492}$	$\frac{521}{490}$	477 451	477	434	434	391 369	391 366	$\frac{275}{260}$	$\frac{258}{239}$	$\frac{255}{241}$	$\frac{239}{221}$	$\frac{235}{222}$	219 203	5.381 6.033
19 20	466 443	459 430	427 406	$\frac{421}{394}$	388 369	381 358	350 332	343	$\frac{246}{234}$	222 207	228 217	206	210	189	6.722
21	422	403	386	371	351	336	316	$\frac{321}{302}$	223	193	206	191 178	199 190	176 164	7.448 8.212
22 23	$\frac{402}{385}$	382 359	369 353	349 329	$\frac{335}{321}$	$\frac{317}{300}$	302 289	$\frac{285}{268}$	$\frac{213}{203}$	180 169	197 188	167 156	$\frac{181}{173}$	153 143	9.012 9.850
24 25	369	$\frac{340}{322}$	338 325	$\frac{312}{294}$	$\frac{307}{295}$	282 268	277 266	$\frac{254}{240}$	195 187	158	181	146	166	134	10.726
26		305	312	279	284	253	255	227	180	149 139	173 167	137 129	160 153	126 118	11.638 12.588
$\frac{27}{28}$	328 316	$\frac{289}{274}$	301 290	$\frac{264}{251}$	$\frac{273}{264}$	$\frac{240}{227}$	$\frac{246}{237}$	$\frac{215}{205}$	173 167	$\frac{131}{123}$	$\frac{160}{155}$	121 114	$\frac{148}{142}$	111 105	13.574 14.599
29 30	305 295	$\frac{261}{249}$	$\frac{280}{271}$	239 227	254 246	$\frac{216}{206}$	$\frac{229}{221}$	195	161	117	149	107	138	98	15.660
31	286	236	262	216	238	196	214	185 176	156 151	$\frac{110}{103}$	144	101	133 129	93 88	16.759 17.894
32 33	$\frac{277}{268}$	$\frac{225}{215}$	$\frac{254}{246}$	$\frac{205}{196}$	$\frac{231}{224}$	187 178	$\frac{208}{201}$	167 160	$\frac{146}{142}$	98 93	135 131	90 86	$\frac{125}{121}$	83 78	19.068 20,278
34 35	$\frac{260}{253}$	$\frac{205}{196}$	239 232	188 179	$\frac{217}{211}$	$\frac{170}{162}$	195 190	152 145	138 134	88	127	81	117	74	21.526
36	246	187	225	171	205	155	184	139	130	83	$\frac{124}{120}$	77	114	70	22.810 24.132
37 38	$\frac{239}{233}$	$\frac{179}{171}$	$\frac{219}{214}$	$\frac{163}{156}$	199 194	148 141	$\frac{179}{175}$	133 127	$\frac{126}{123}$	_	117 114		$\frac{108}{105}$		25.492 26.888
39 40	227 221	$\frac{163}{157}$	$\frac{208}{203}$	150 143	189 184	135 130	170 166	121- 116	$\frac{120}{117}$		111		102	- 0	28.322
41	216	150	198	137	180	124	162	111	114		108 106		100 97		29.793 31.301
42 43	211 206	$\frac{144}{138}$	193 189	131 126	$\frac{176}{172}$	$\frac{119}{114}$	158 154	$\frac{107}{102}$	111		103 101		95 93		32.847 34.430
44 45	$\frac{201}{197}$	$\frac{132}{127}$	184	121 116	168 164	109 105	151 148	98	106		98		91		36.050
46	192	122	176	111	160	101	144	94	$\frac{104}{102}$		96 94		89 87		37.707; 39.401
47 48	188 184	117	$\frac{173}{169}$	107	$\frac{157}{154}$	97	141 138		100 97		92 90		85 83	- 19	41.133 42.902
49 50	181 177		166 162		151 148		136	1	95	·	88		81		44.708
51	174		159		145		133 130		94 92		87 85		80· 78		46.552
52 53	170 167		156 153		142 139		$\frac{128}{125}$		90 88		83 82		77 75		50.350
54	164		150		137		123		-87		80		74		54.298
55 56	161		148		134		121		85		79		73		56.328
57	155		142		129		117		84 82		. 77 76		71 70		58.395 60.499
58	153		140		127		114		\81		75		69		62.640

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

-	Nominal Depth and Flange Width—Weight per Foot														
Span			СВ	272	27"x	14"				CB	271	27"x9	3/4"		Coefficient of Deflection
in Feet	190	lbs.	175		160	lbs.	145	lbs.	112	lbs.	101		91]	bs.	oeffi of oeffec
1000	- 1	-	w. 1	Laterally Free Fixed Free Fixed Free						Laterally Fixed Free Fixed Free Fixed Free					
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed						
10									$\frac{371}{352}$	$\frac{371}{352}$	$\frac{333}{318}$	$\frac{333}{318}$	$\frac{299}{286}$	$\frac{299}{286}$	1.862
11										320	289	289 265		260 238	$\frac{2,253}{2,681}$
12 13	$\frac{501}{493}$	$\frac{501}{493}$	$\frac{459}{455}$	$\frac{459}{455}$	$\frac{417}{416}$	$\frac{417}{416}$	376	376	271	$\frac{293}{268}$	$\frac{265}{244}$	241		217	3.147
14 15	458 428	$\frac{458}{428}$	$\frac{422}{394}$			386 360	$\frac{350}{326}$	$\frac{350}{326}$	$\frac{251}{235}$	$\frac{244}{223}$	$\frac{227}{212}$	$\frac{219}{202}$	204 191	198 181	$\frac{3.650}{4.190}$
16	401		369			338	306	306	220	206	199	185	179	166	4.767
17 18	377 356		348 328		318 300	$\frac{318}{299}$	$\frac{288}{272}$	$\frac{288}{270}$	$\frac{207}{195}$	$\frac{189}{175}$	187 176	$\frac{171}{158}$	$\frac{168}{159}$	153 141	$\frac{5.381}{6.033}$
19	338	333	311	305	$\frac{284}{270}$	279 262	258 245	$\frac{253}{237}$	185 176	162 151	167 159	146 136	151 143	131 122	6.722 7.448
20	321	311 293	295 281	287 270	257	246	233	223	168	140	151	126	136	114	8.212
21 22	$\frac{305}{292}$	277	269	254	246	232	223	210	160	131	144	118	130	106	9.012 9.850
$\frac{23}{24}$	279 267	$\frac{260}{246}$	$\frac{257}{246}$	$\frac{240}{226}$	$\frac{235}{225}$	$\frac{218}{207}$	$\frac{213}{204}$	198 187	$\frac{153}{147}$	122 114	$\frac{138}{132}$	$\frac{110}{102}$	124 119	92	10.726
25	257	233	236	214	216	196	196	177	141	107	127 122	96	114	86	11.638 12.588
26 27	247 238	$\frac{221}{210}$	$\frac{227}{219}$	$\frac{203}{192}$	$\frac{208}{200}$	$\frac{185}{176}$	188 181	$\frac{168}{159}$	135 130	94	118	85	110 106	76	13.574
28 29	229 221	199 189	211 204	183 173	193 186	$\frac{166}{158}$	175 169	151 144	$\frac{126}{121}$	88 83	113 110	79 75	102 99	71 67	14.599 15.660
30	214	179	197	165	180	151	163	136	117	78	106	70	95	63	16.759
31 32	$\frac{207}{200}$	171 163	191 185	$\frac{158}{150}$	174 169	$\frac{143}{137}$	158 153	$\frac{130}{123}$	113 110	74 69	102 99	66 62	92 89	59 56	17.894 19.068
33 34	194 189	155 148	179 174	$\frac{143}{136}$	$\frac{164}{159}$	$\frac{130}{124}$	148 144	$\frac{118}{112}$	107 103		96 93		87 84		20.278 21.526
35	183	141	169	130	154	119	140	107	101		91		82		22.810
36 37	178 173	135 129	164 160	$\frac{124}{119}$	150 146	113 108	$\frac{136}{132}$	103	98 95		88 86	1	79 77	1	$24.132 \\ 25.492$
38 39	169 164	123 118	156 152	114 108	142 139	103	$\frac{129}{126}$	94 89	93		84		75 73		26.888 28.322
40	160	114	148	104	135	95	122	86	88		79		71		29.793
41 42	156 153	108 104	144 141	100	$\frac{132}{129}$	91 87	$\frac{119}{117}$	82 79	86 84		77 76		70 68		$31.301 \\ 32.847$
43	149 146	99	137 134	92	$\frac{126}{123}$	83 80	114 111	76 72	82 80		74 72		67		34.430 36.050
44 45	143	92	131	84	120	77	109	69	78		71		64	:	37.707
46 47	139 136	88 85	128 126	81 78	117 115	74 71	106 104	66	76 75		69 68		62		39.401 41.133
48	134		123	10	113	, ,,	102		73		66		60		42.902 44.708
49 50	131	-	121	-	110 108		100 98		72 70		65 64		58 57		46.552
51	126		116		106		96		69		62		58		48.432 50.350
52	123		114			1			1)	1	1	1	1	1	1 30.330

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 18,000 Pounds per Square Inch

	Nominal Depth and Flange Width—Weight per Foot														
Span			CE	3 244	24''x	14"				CB	243	24''x	12"		Coefficient of Deffection
in Feet	160	lbs.	150	lbs.		lbs.	130	lbs.	120	lbs.		lbs.	100	lbs.	Coefficient of Deflection
1000				_	rally		1				Late				ರಿ ಕ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
12 13 14 15	$\frac{397}{379}$ $\frac{352}{329}$		330	355 330 308	344 332 308 287	$\frac{344}{332}$ $\frac{308}{308}$ $\frac{344}{308}$	$ \begin{array}{r} 318 \\ \hline 308 \\ 286 \\ 267 \end{array} $	$\frac{318}{308}$ $\frac{286}{267}$	$ \begin{array}{r} 314 \\ \hline 302 \\ 279 \\ 259 \\ 242 \end{array} $	$\begin{array}{r} 314 \\ 302 \\ 279 \\ 259 \\ 242 \end{array}$	$ \begin{array}{r} 286 \\ \hline 277 \\ 256 \\ 237 \\ 221 \end{array} $	$\begin{array}{r} 286 \\ \hline 277 \\ 256 \\ 237 \\ 221 \\ \end{array}$	$\begin{array}{r} 259 \\ \hline 252 \\ 232 \\ 216 \\ 201 \\ \end{array}$	$\begin{array}{r} 259 \\ \hline 252 \\ 232 \\ 216 \\ 201 \\ \end{array}$	2.681 3.147 3.650 4.190
16 17 18 19 20	$\frac{290}{274}$ $\frac{259}{259}$	290 273 255	289 272 257 243 231	289 272 255 239 224	269 254 239 227 216	269 254 238 223 209	250 235 222 211 200	250 235 221 207 194	226 213 201 191 181	223 208 193 180 168	208 195 185 175 166	205 190 176 165 154	189 178 168 159 151	186 172 160 150 140	4.767 5.381 6.033 6.722 7.448
21 22 23 24 25	235 224 214 205 197	189	220 210 201 192 185	210 198 188 177 167	205 196 187 180 172	196 185 174 165 156	191 182 174 167 160	182 172 162 153 145	173 165 158 151 145	158 148 139 131 123	158 151 144 138 133	144 135 127 119 112	144 137 131 126 121	131 123 115 109 102	8.212 9.012 9.850 10.726 11.638
26 27 28 29 30	183 176 170	$160 \\ 153 \\ 145$	178 171 165 159 154	158 150 143 135 129	166 160 154 149 144	148 140 133 126 121	154 148 143 138 133	137 130 123 117 111	139 134 129 125 121	116 110 104 98 93	128 123 119 115 111	106 100 95 90 85	116 112 108 104 101	96 91 86 81 77	12.588 13.574 14.599 15.660 16.759
31 32 33 34 35	$154 \\ 149 \\ 145$	125 119 113	149 144 140 136 132	123 117 112 106 102	139 135 131 127 123	114 109 104 99 94	129 125 121 118 114	106 101 96 92 88	117 113 110 107 104	88 84 79 75 72	107 104 101 98 95	80 75 71 68 64	97 94 92 89 86	73 69 66 63 59	17.894 19.068 20.278 21.526 22.810
36 37 38 39 40	137 133 130 126 123	99 95	128 125 122 118 115	97 93 88 85 80	120 117 113 111 108	90 87 82 79 75	111 108 105 103 100	84 80 77 73 70	101 98 95 93 91	68 65 62 59 56	92 90 87 85 83	61 58 55 53	84 82 79 77 76	57 54 51 49 47	24.132 25.492 26.888 28.322 29.793
41 42 43 44 45	$ \begin{array}{c} 120 \\ 117 \\ 115 \\ \underline{112} \\ \hline 110 \end{array} $	83 80 76 73	113 110 107 105 103	78 75 71	105 103 100 98 96	72 69 66	98 95 93 91 89	67 64 62	88 86 84 82 81		81 79 77 75 74		74 72 70 69 67		31.301 32.847 34.430 36.050 37.707
46 47	107 105		100 98		94 92		87 85		79 77		72 71		66 64		39.401 41.133

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

			No	minal	Deptl	n and	Flang	e Wid	th—W	eight	per F	oot			
Span		СВ	242	24''x9	34"		CB 24"2	241		CH	3 213	21′′>	13"		Ccefficient of Deflection
in Feet	94	lbs.	85	lbs.	76	lbs.	70	lbs.	120	Ibs.	112	lbs.	104	lhs.	of Of Hec
			Late	rally			Late	erally			Late	rally			ပိ ဓိ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							230	230							
9	291	291	262	262	233	233	217	217							1.508
10	270	270	244	244	218	218	195	195							1.862
11	245	245		222	199	199	178	176	273	273					2.253
12 13	225 208	$\frac{225}{205}$	203 188	203	182 168	182	163	158		272	253	253	234	234	2.681
14	193	187	174	185 169	156	$\frac{166}{151}$	150 140	143 130	$\frac{251}{233}$	$\frac{251}{233}$	$\frac{235}{218}$	$\frac{235}{218}$	$\frac{218}{202}$	$\frac{218}{202}$	3.147 3.650
15	180	171	163	155	146	138	130	118	218	218			189	189	4.190
16	169	158	153	142	137	127	122	108	204	204	191	191	177	177	4.767
17 18	159 150	$\frac{145}{134}$	144 136	131 121	128 121	117 108	$\frac{115}{109}$	99	192 181	$\frac{191}{177}$	179 169	178	166	164	5.381
19	142	124	129	112	115	100	103	84	$\frac{181}{172}$	166	160	166 155	$\frac{157}{149}$	154 143	$6.033 \\ 6.722$
20	135	115	122	104	109	93	98	78	163	156	152	145	141	134	7.448
21	129		116	97	104	87	93	72	155	146	145	136	135	126	8.212
22 23	$\frac{123}{117}$	100 94	$\frac{111}{106}$	90 84	99 95	81 75	89 85	67 62	$\frac{148}{142}$	137 129	139 133	$\frac{128}{120}$	129	119	9.012
24	113	88	102	79	91	70	81	57	136	$\frac{129}{122}$	127	114	123 118	$\frac{111}{105}$	$9.850 \\ 10.726$
25	108	82	98	74	87	66	78	54	131	115	122		113	99	11.638
26	104	77	94	69	84	62	75	50	126	109	117	101	109	94	12.588
27 28	100 96	72 68	90 87	65 61	81 78	58	72 70	47	121 117	$\frac{103}{97}$	$\frac{113}{109}$	96	$\frac{105}{101}$	89 84	13.574 14.599
29	93	64	84	57	75	51	67	77	113	92	105	86	98	80	15,660
30	90	60	81	54	73	48	65		109	88	102	82	94	76	16.759
31	87	57	79	51	70	45	63		105	83	98	78	91	72	17.894
32 33	84 82	53	76 74	48	68	43	61		102 99	79 75	95 92	74 70	88 86	68 65	$ \begin{array}{c} 19.068 \\ 20.278 \end{array} $
34	79		72		64		59 57		96	72	90	67	83	62	21.526
35	77		70		62		56		93	68	87	64	81	59	22.810
36 37	75 73		68 66		61		54		91	65	85	61	79	56	24.132
38	71		64		59 57		53 51		88 86	62	82	58	76	54	25.492 26.888
39	69		63		56		50		84	00	78		73		28.322
40	68		61		55		49		82		76		71		29.793
41	66		60	1	53		48		80						31.301
42 43	64		58 57		52 51		47 45								32.847 34.430
44	61		55		50		44								36.050
45	60		54		49		43								37.707
46	59		53		47		42								39.401

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

	Nominal Depth and Flange Width—Weight per Foot														
Span		CB	212	21''x	9''				CI	3 211	21''	x8''			ient
in Feet	92	lbs.	86 1	bs.	80 1	bs.	70	lbs.	64	lbs.		lbs.	58	lbs.	Coefficient of Deflection
reet			Late	-						Later		1			2 A
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
7							221	221	201_	201	189	189	181	181	0.912
8 9	256	256	238	238	221	221	$\frac{218}{194}$	$\frac{218}{194}$	$\frac{199}{177}$	199 177		186 165	180 160	180 160	1.192 1.508
10		$\frac{236}{236}$	220		205	205	174					149	144	144	1.862
11	214	214	200	200	186	186		156	145	142	135	132	131	128	2.253
12 13	196 181	$\frac{194}{175}$	$\frac{184}{170}$	181 164	171 158	$\frac{168}{153}$	$\frac{145}{134}$	139	133 123	127 115	124 115	$\frac{119}{107}$	120 111	115 104	2.681 3.147
14	168	160	157	149	146	138	124	114	114	104	106	97	103	.94	3.650
15	157	146	147	136	137	127	116	103	106	94	99	88	96	85	4.190
16 17	147	$\frac{134}{123}$	$\frac{138}{130}$	$\frac{125}{115}$	$\frac{128}{121}$	116 106	109 103	94 86	100 94	86 79	93	80 73	90 85	78 71	4.767 5.381
18	131	114	122	106	114	98	97	79	89	72	83	67	80	65	6.033
19 20	124 118	$\frac{105}{97}$	116 110		$\frac{108}{103}$	91 84	92 87	73 67	84	67	78 74	62 57	76 72	60 55	6.722 7.448
								62	76	57	71	53	69	51	8.212
$\frac{21}{22}$	$\frac{112}{107}$	90	$\frac{105}{100}$	84 78	98	78 73	83 79	57	72	52	68	49	66	47	9.012
23 24	103 98	78 73	96 92	73 67	89 85	67	76 73	53 49	69-	49 45	65 62	45 42	63	44	$9.850 \\ 10.726$
25	94	68	88	63	82	59	70	46	64	42	60	39	58	38	11.638
26	91	63	85	59	79	55	67	43	61	39	57	36	56	35	12.588
27 28	87 84	59 56	82 79	55 52	76 73	51 48	65	1	59		55 53		53		13.574 14.599
29	81	52	76	48	71	45	60		55		51		50		15.660 16.759
30	79	49	73	46	68	42	58		53		50		48		
31 32	76 74		71 69		66		56 54		51 50		48		47		17.894 19.068
33	71		67		62		53		48		45		44	1	20.278
34 35	69		65	1	60 59		51 50		47 46		44 43		42		$21.526 \\ 22.810$
36	65		61		57		48		44		41		40		24.132
37	64		60		55		47		43		40		39		25.492
38 39	62	-	58 57		54 53		46		42	1	39	1	38		26.888 28.322
40	60 59		55		51		44		40		37		36	1	29.793
41	58						1	1							31.301
	W.		1		1	1	3	1		1	1	1	L	1	

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 18,000 Pounds per Square Inch

			Nomin	al Dep	oth and	Flang	e Widtl	ı—We	ight pe	r Foot			
Span		CI	3 183	18''x1	2''			CB	182	8''x8½	2"		sient stion
in Feet	100	lbs.	93		86	lbs.	78	bs.	Tates		67	lbs.	Coefficient of Deflection
	Fixed	Free	Later		Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	O
	rixed	Free	rixed	FFEE	Fixed	Free			-				
9							193	$\frac{206}{193}$	$\frac{190}{178}$	$\frac{190}{178}$	175	$\frac{175}{165}$	1.508
10	218	218_	201	201	185	185	174	174	160	160	149	149	1.862
11	213	213	198	198	184	184	158	156	146	144	135	134	2.253
12 13	196 181	196 181	182 168	$\frac{182}{168}$	168 155	$\frac{168}{155}$	145 133	$\frac{141}{127}$	133 123	$\frac{130}{117}$	$\frac{124}{115}$	120 109	$\frac{2.681}{3.147}$
14 15	168 156	168 156	156 146	156 146	144 135	144 135	124 116	116 105	114 107	106 97	106 99	99	$\frac{3.650}{4.190}$
16	147	144	136	134	126	124	108	96	100	89	93	83	4,767
17	138	134	128	125	119	115	102	88	94	81	88	76	5.381
18 19	130 124	$\frac{125}{116}$	$\frac{121}{115}$	116 108	112 106	107 100	96 91	81 75	89 84	75 69	83 78	69 64	$6.033 \\ 6.722$
20	117	109	109	101	101	93	87	69	80	64	74	59	7.448
$\frac{21}{22}$	112 107	102 96	104 99	95 89	96 92	88 82	83 79	64	76 73	59 55	71 68	55 51	8.212 9.012
23	102	90 85	95	83 78	88	77 73	75 72	55 51	70 67	51 47	65 62	47	$9.850 \\ 10.726$
$\frac{24}{25}$	98 94	80	91 87	74	84 81	68	69	48	64	44	60	41	11.638
26	90	75	84	70	78	64	67	45	62	41	57	38	12.588
27 28	87 84	71 67	81 78	66 62	75 72	61 58	64 62	42 39	59 57	38 36	55 53	36 33	13.574 14.599
29 30	81 78	64	75 73	59 56	70 67	54 52	60 58		55 53		51 50		$15.660 \\ 16.759$
31	76	57	70	53	65	49	56		52		48		17.894
32	73	54	68	50	63	46	54		50		47		19.068
33 34	71 69		66 64		61 59		53 51		49 47		45 44		21.526
35	67		62		58		50		46		43		22.810

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

			No	ninal	Depth	and	Flange	e Wid	th-W	eight	per F	oot			
Span			CB	181	18"x7	1/2"				СВ	165	16''x1	14''		Coefficient of Deflection
in Feet	58	lbs.	52 1		51 1	bs.	47 1	bs.	115	lbs.	107		100	lbs.	cf effec
1000				Latera							Later				Ö A
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33	172 158 140 126 115 105 97 90 84 79 74 70 66 63 60 57 55 53 51 49 47 44 42 41 39 38	172 158 140 125 111 99 89 80 73 67 61 55 51 47 43 40 37 34 32	154 142 126 113 103 94 87 87 67 63 60 57 54 49 47 44 42 40 39 38 37 35	154_ 142_ 126_ 112_ 99_ 80_ 72_ 65_ 59_ 45_ 42_ 38_ 33_ 30_ 28_	135 120 108 98 90 83 77 72 67 63 60 57 54 47 45 43 41 40 39 37 36 35 34 33	162 154 135 120 106 94 85 76 69 62 57 52 47 43 40 37 34 31 29 27	93 85 79 73 68 64 60 57 54 51 49 47 45 38 37 35 34 33 32 31	138 128 114 101 90 80 72 65 59 45 41 38 35 32 30 27 25	176 164 154 145 137 130 123	189 176 164 154 145 136 127 120	192 191 176 164 153 143 135 127 121 114 109 104 100 95 92 88 88 82 79 76	192 191 176 164 153 126 118 111 104 98 93 88 88 87 75	153 143 134 126 119 113	178 165 165 165 1153 143 126 118 111 103 97 92 77 73 69 66	0.912 1.192 1.508 1.862 2.253 2.681 3.147 3.650 4.190 4.767 5.381 6.033 6.722 7.448 8.212 9.012 9.850 10.726 11.638 12.588 13.574 14.599 15.660 16.759 17.894 19.068 20.278
34 35	37 36		33 32		32 31		30 29								21.526 22.810

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 18,000 Pounds per Square Inch

			Nomi	nal De	pth and	l Flange	e Width	-Wei	ght per	Foot			
Span		(CB 164	16''x	12''		1	CF	3 163	16"x8½	2"		Coefficient of Deflection
in Feet	90	lbs.	83		76	lbs.	68	lbs.	63		58	lbs.	of of effec
1000				erally					Late	rally			ပြိ မိ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							170.6	170.6	157.0	157.0	144.0	144.0	
9	192.9	192.9	177.2	177.2	160.9	160.9	151.8	151.8	140.6	140.6	129.4	129.4	1.508
10	188.5	188.5	173.9	173.9	159.2	159.2	136.6	136.6	126.6	126.6	116.5	116.5	1.862
11	171.4	171.4	158.1	158.1	144.7	144.7	124.2	123.2	115.1	114.1	105.9	105.0	2.253
12 13	137.1 145.0	$137.1 \\ 145.0$	133.7	133.7	132.7 122.5	$132.7 \\ 122.5$	105.1	100.9 100.1	97.4	92.4	97.1 89.6		
14	134.6	134.6	124.2	124.2	113.7	113.7	97.6	91.1	90.4	84.1	83.2	77.4	3.650
15	125.7	120.7	115.9	115.9	100.1	100.1	91.1	82.9	84.4	76.8	77.7	70.4	4.190
16 17	$117.8 \\ 110.9$	116.0	108.7	$107.0 \\ 99.3$			85.4 80.4	75.7 69.7	$79.1 \\ 74.5$	$70.1 \\ 64.2$	72.8 68.5		
18	104.7	100.1	96.6	92.4	88.4	84.6	75.9	64.0	70.3				
19 20	99.2 94.2	$93.4 \\ 87.6$			83.8 79.6	$78.9 \\ 73.7$	71.9 68.3	58.8 54.5					
21 22	89.8 85.7	$\frac{82.1}{77.0}$	82.8 79.0		75.8 72.4		$65.1 \\ 62.1$	50.4 46.9					8.212 9.012
23	82.0	72.3	75.6	66.4	69.2	60.8	59.4	43.4	55.0	40.0	50.6	36.8	9.850
24 25	78.5 75.4	$68.1 \\ 64.1$	$72.4 \\ 69.5$	62.5 58.9	66.3 63.7	57.2 53.9	$56.9 \\ 54.7$	$\frac{40.3}{37.7}$	52.7 50.6	$37.3 \\ 34.7$	$\frac{48.5}{46.6}$		10.726 11.638
26 27	$72.5 \\ 69.8$	$60.5 \\ 57.1$	$66.9 \\ 64.4$	$55.5 \\ 52.4$	61.2 59.0	50.8 48.0		$\frac{35.0}{32.8}$		$\frac{32.5}{30.2}$			$12.588 \\ 13.574$
28	67.3	54.0	62.1	49.6		45.4		30.6		28.2			14.599
29	65.0	51.1	60,0		54.0		47.1		43.6	i i	40.2		15.660
30	62.8		58.0		53.1		45.5		42.2		38.8		16.759
31	60 8		56.1		51.4		44.1		40.8		37.6		17.894
32	58 9						42.7						19.068

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 18,000 Pounds per Square Inch

			Nomin	nal Der	oth and	Flang	e Widtl	ı—Wei	ght per	Foot			
Span			CE	3 162	16" x 7	7//			C	B 161	16"x6	"	Coefficient of Deflection
in Feet	50	lbs.	45		43 1	bs.	40 l	bs	38 1		35 1	bs.	oeffi of offer
				Late		_		-	- 1	Late	-	70	0 4
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
					143.4				120,7	120.7		110.9	0.070
6 7	141.2	$\frac{141.2}{140.4}$			$\frac{131.7}{112.9}$		111 4	111.4	$118.4 \\ 101.5$			109.4 93.8	$0.670 \\ 0.912$
8					98.8		98.4					80.8	1.192
9	109.2			97.9					79.0			69.8	1.508
10	98.3	95.4	88.6	86.0	79.0	76.7	78.7	76.1	71.1	65.8	65.7	60.8	1.862
11	89.3	84.4	80.5	76.1	71.8	67.9	71.6	67.6			59.7	53.4	2.253
12	81.9						65.6		59.2			47.2	2.681 3.147
13 14	$75.6 \\ 70.2$			$60.7 \\ 54.6$		54.4 48.9				45.4			3.650
15	65.5					44.2			47.4				4.190
16	61.4								44.4				4.767
17 18	57.8 54.6			$\frac{40.7}{37.1}$	$\frac{46.5}{43.9}$								5.381 6.033
19	51.7	37.8		33.9	41.6	30.4	41.4	30.1	37.4	24.3	34.6	22.3	6.722
20	49.1	34.6	44.3	31.2	39.5	28.0	39.4	27.6	35.5	22,1	32,8	20.3	7.448
21	46.8		42.2								31.3		8.212
22	44.7										$29.8 \\ 28.5$		9.012 9.850
$\frac{23}{24}$	41.0	27.0	36.9		32.9		32.8		29.6		27.4		10.726
$\frac{1}{25}$	39.3		35.4		31.6		31.5		28.4		26.3		11.638
26	37.8		34.1		30.4		30.3		27.3		25.3		12.588
27	36.4		32.8		$\frac{29.3}{28.2}$		$\frac{29.2}{28.1}$		26.3 25.4		$\begin{vmatrix} 24.3 \\ 23.5 \end{vmatrix}$		13.574 14.599
28 29	35.1 33.9		31.6		27.2		27.1		24.5		22.6		15.660
30	32.8		29.5		26.3		26.2		23.7		21.9		16.759
31	31.7		28.6		25.5		25.4		22.9		21.2		17.894
32	30.7								1				19.068

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

			Nemi	nal Dep	oth and	Flange	Width	-Weig	ght per	Foot			
Span			CB 145	14''x	12''			_ C:	B 144	14''x1	0''		Coefficient of Deflection
in	105	lbs.	95]	bs.	85	lbs.	75 1	lbs.	68	lbs.	61	lbs.	of of effect
Feet			Late	rally					Late	rally			S Ă
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
9							$\frac{161.5}{152.7}$	161.5 152.7	145.2 138.4	$\frac{145.2}{138.4}$	$\frac{129.2}{124.2}$	$\frac{129.2}{124.2}$	1.508
10	184.9	184.9	165.1	165.1	146.2	146.2	137.4	137,4	124.5	124.5	111.7	111.7	1.862
11							124.9						2.253
12 13							$114.5 \\ 105.7$			$\frac{103.8}{95.0}$		93.1 85.3	$\frac{2.681}{3.147}$
14	139.5	139.5	126.2	126.2	112.8	112.8	98.2	95.6	89.0	86.7	79.8	77.8	3.650
15	130.2	130.2	117.8	117.8	105.3	105.3	91.6	87.9	83.0	79.4	74.5	71.2	4.190
16	122.1	120.7	110.4	108.7	98.7		85.9		77.8				4.767
17 18			$103.9 \\ 98.1$	$\frac{100.9}{93.8}$	$92.9 \\ 87.7$	$90.2 \\ 83.9$	80.8 76.3	$74.5 \\ 68.9$					5.381 6.033
19		$\frac{104.2}{97.2}$				78.2	72.3						6.722
20	97.7	90.8	88.3	81.8	79.0	73.1	68.7	59.6	62.3	53.7	55.9	48.2	7.448
21	93.0	85.0	84.1	76.6	75.2	68.5	65.4	55.4	59.3	50.2	53.2		
22	88.8	79.8	80.3										
23 24	84.9 81.4												10.726
25	78.1						55.0						11.638
26	75.1		67.0		60.7		52.9		47.9		43 0		12.588
27	72.4		65.4		58.5		50.9		46.1		41.4		13.574
28	69.8		63.1		56.4		49.1		44.5		39.9		14.599

CARNEGIE BEAM SECTIONS—Continued

Allowable Uniform Loads in Thousands of Pounds Maximum Bending Stress, 18,000 Pounds per Square Inch

Cheange		No	minal I	Depth ar	d Flang	e Width	-Weigh	t per Fo	ot		
Span			CB 143	14''x8	"		C	B 142	14''x63/4	"	Coefficient of Defication
in Feet	58	lbs.	53 1	lbs.	48	lbs.	42	lbs.	39	lbs.	oeffe oeffe
			Late	erally				Late	rally		OH
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							116.9	116,9	108.1	108.1	
7	141.2	141.2	128.1	128.1	115.2	115.2	103.9	103.9	96.4	96.4	0.912
8	128.4	128.4	117.4	117.4	106.3	106.3	90.9	90.9	84.4	84.4	1.192
9 10	$\frac{114.1}{102.7}$	$\frac{114.1}{102.7}$	104.3 93.9	104.3	94.5 85.0	94.5 85.0	80.8	79.9 70.1	75.0 67.5	73.9 64.8	1.508 1.862
10	102.7	102,1	89.9	99.9	00.0	00.0	12.1	10,1	07.5	04.0	1.002
11	93.4	91.6	85.4	83.5	77.3	75.6	66.1	62.0	61.4	57.3	2.253
12	85.6	82.1	78.2	74.8	70.9	67.8	60.6	55.2	56.3	51.0	2.681
13 14	$79.0 \\ 73.4$	74.1 67.1	72.2 67.1	67.4	65.4	61.1 55.3	55.9 51.9	49.4	51.9 48.2	45.6 41.0	$\frac{3.147}{3.650}$
15	68.5	61.0	62.6	55.5	56.7	50.3	48.5	39.9	45.0	37.0	4.190
16	64.2	55.6	58.7 55.2	50.6 46.3	53.1	45.8	45.5 42.8	36.1 32.8	42.2	33.5 30.4	$\frac{4.767}{5.381}$
17 18	60.4 57.1	50.9 46.7	52.2	42.5	47.2	38.5	40.4	29.8	37.5	27.7	6.033
19	54.0	42.9	49.4	39.1	44.8	35.4	38.3	27.2	35.5	25.3	6.722
20	51.3	39.5	46.9	36.2	42.5	32.6	36.4	24.9	33.8	23.1	7.448
21	48.9	36.5	44.7	33.4	40.5	30.1	34.6	22.8	32.1	21.2	8.212
$\frac{21}{22}$	46.7	33.8	42.7	30.9	38.7	27.8	33.1	21.0	30.7	19.5	9.012
23	44.6	31.3	40.8	28.6	37.0	25.8	31.6		29.4		9.850
24	42.8	29.0	39.1	26.5	35.4	$23.9 \\ 22.2$	30.3		28.1		10.726 11.638
25	41.1	26.9	37.6	24.6	34.0	44.2	29.1		27.0		11.038
26	39.5		36.1		32.7		28.0		26.0		12.588
27	38.0		34.8		31.5		26.9		25.0		13.574
28	36.7		33.5		30.4		26.0		24.1		14.599

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

		Nomin	nal Depth	and Flang	ge Width—	Weight pe	er Foot		
Span			CB 142	14"x63/4"			CB 141	14"x6"	Coefficient of Deflection
in Feet	38	lbs.		lbs.	33	lbs.	30 1		of of reflect
				rally			Later	-	OA
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
4	126.0	126,0							0.298
5	122.6	122.6					90.5	90.5	0.466
6	102.1	102.1	99.3	99.3	90.7	90.7	83.6	83.6	0.670
6 7	87.5	87.5	89.0	89.0	81.7	81.7	71.7	71.7	0.912
8 9	76.6 68.1	76.6 67.3	77.9 69.2	$77.9 \\ 68.2$	71.5 63.5	71.5 62.6	62.7 55.8	61.8 53.3	1.192 1.508
10	61.3	59.0	62.3	59.8	57.2	54.9	50.2	46.5	1.862
11	55.7	52,2	56.7	52.9	52.0	48.5	45.6	40.8	2,253
12	51.1	46.5	51.9	47.1	47.6	43.2	41.8	36.1	2.681
13 14	47.1 43.8	$\frac{41.6}{37.4}$	47.9 44.5	$\frac{42.1}{37.9}$	44.0	38.6 34.6	38.6 35.8	32.1 28.6	3.147 3.650
15	40.9	33.8	41.6	34.2	38.1	31.2	33.5	25.6	4.190
16	38.3	30.6	39.0	30.9	35.7	28.2	31.4	23.0	4.767
17 18	36.0 34.0	27.8 25.3	36.7 34.6	$\frac{28.1}{25.4}$	33.6 31.8	$25.6 \\ 23.3$	29.5 27.9	20.8 18.8	5.381 6.033
19	32.3	23.1	32.8	23.2	30.1	21.3	26.4	17.0	6.722
20	30.6	21.1	31.2	21.2	28.6	19.5	25.1	15.5	7.448
21	29.2	19.4	29.7	19.5	27.2	17.9	23.9		8.212
22 23	27.9 26.6	17.8	28.3 27.1	17.9	26.0 24.9	16.4	22.8 21.8		9.012 9.850
$\frac{23}{24}$	25.5		26.0		23.8		20.9		10.726
25	24.5		24.9		22.9		20.1		11.638
26	23.6		24.0		22.0		19.3		12.588
27 28	22.7		23.1		21.2		18.6		13.574
20	21.9		22.3		20.4		17.9		14.099

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 18,000 Pounds per Square Inch

			Nomin	al Dep	th and	Flange	Width	-Weig	ht per	Foot			
Span			C	B 124	12''x1	0''			C	B 123	12′′x8	"	Coefficient of Deflection
in Feet	100	lbs.	91	lbs.	83	lbs.	75	lbs.	50	lbs.	45	lbs	Coefficient of Deflection
1.000				Late	rally					Late	rally		ರಿ ದ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
5	$\frac{322.8}{263.6}$					202.8							0.466
													0.400
6	219.7 188.3												0.670
8	164.7								98.0	98.0	94.9	94.9	0.912 1.192
9	146.4								87.1	87.1	78.5	78.5	1.508
10	131.8	131.8	125,4	125.4	119.8	119.8	114.1	114.1	78.4	78.4	70.6	70.6	1.862
$\frac{11}{12}$	119.8									70.0	64.2		2.253
13	$109.8 \\ 101.4$			96.5		99.8 91.7	$\frac{95.1}{87.8}$		$65.4 \\ 60.3$	62.7 56.5	58.8 54.3	56.3 50.7	$2.681 \\ 3.147$
14	$94.1 \\ 87.9$		89.6	87.9	85.6	83.7	81.5	79.4	56.0	51.2	50.4	45.9	3.650
15	81.9	85.3	83.6	80.9	79.9	76.7	76.1	12,8	52.3	46.6	47.1	41.7	4.190
16 17	82.4								49.0	42.5	44.1	38.1	4.767
18	77.5 73.2						$67.1 \\ 63.4$		46.1	$\frac{38.9}{35.7}$	$\frac{41.5}{39.2}$	$\frac{34.8}{31.9}$	5.381 6.033
19	69.4								41.3	32.8	37.2	29.5	6.722
20	65.9	58.4	62.7	55.1	59.9	52.2	57.1	49.2	39.2	30.2	35,3	27,2	7.448
21	62.8	54.4		51.3		48.5		45.8	37.3	27.9	33.6	25.1	8.212
22 23	59.9 57.3		57.0 54.5		54.5 52.1		51.9 49.6		35.6 34.1	7.9	32.1		9.012 9.850
24	54.9		52.3		49.9		47.6		32.7		29.4		10.726
	i i												

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

-	}		Nomi	nal De	pth and	l Flang	ge Wid	th-W	eight p	er Foo	t		
Span	CB 123	12"x8"	1		CI	3 122	12"x6	1/2"			CB 121	12"x6"	sient
Feet		lbs.	36	lbs.	34	lbs.	32	lbs.	28	lbs.		lbs.	Ccefficient of Deflection
	Fixed	,	Fixed	Free	Fixed	,	,	Free	Fixed	Free	Fixed	Free	
5					108:2 95.1	108.2 95.1					68.7	68.7	0.466
6 7	83.5	83.5	90.4	90.4		79.2 67.9	79.7	$\frac{79.7}{69.7}$	69.1	69.1		$61.4 \\ 52.6$	0.670 0.912
8 9	78.4	78.4 69.7	68.7	68.7	59.4	59.4	61.0	61.0	53.4	53.4	46.0	45.4	1.192
10	62.7							46.5	47.4 42.7			39.1 34.1	$\frac{1.508}{1.862}$
	52.3	50.0 45.1 40.8	$\frac{42.3}{39.2}$	$41.1 \\ 36.6 \\ 32.9$	39.6 36.6 34.0	$\frac{35.6}{31.8}$ $\frac{28.6}{28.6}$	40.7	40.9 36.4 32.4 29.1 26.2	$35.6 \\ 32.8 \\ 30.5$	31.7	33.5 30.7 28.3 26.3 24.6	30.0 26.5 23.5 21.0 18.8	2.253 2.681 3.147 3.650 4.190
16 17 18 19 20	36.9 34.9 33.0	30.9	32.3 30.5 28.9	26.7 24.3 22.1 20.1 18.3	$28.0 \\ 26.4 \\ 25.0$	23.2 21.1 19.2 17.5 15.9		21.4 19.5 17.7	$25.1 \\ 23.7 \\ 22.5$	18.6	$\frac{20.5}{19.4}$	16.9 15.3 13.8 12.5 11.4	4.767 5.381 6.033 6.722 7.448
21 22 23 24	29.9 28.5 27.3 26.1	22.2	26.2 25.0 23.9 22.9	16.8	22.6 21.6 20.7 19.8	14.6	$\begin{array}{r} 23.2 \\ \hline 22.2 \\ 21.2 \\ 20.3 \end{array}$	14.8	20.3 19.4 18.6 17.8	12.9	17.5 16.7 16.0 15.3		8.212 9.012 9.850 10.726

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 18,000 Pounds per Square Inch

			Nomi	nal De	pth and	Flang	e Width	ı—Wei	ght per	Foot			
Span		C	B 103	10"x9)''			C	B 102	10"x8	"		ient
in Feet	63	lbs.	-	lbs.	49	lbs.	42	lbs.		lbs.	31	lbs.	Coefficient of Deflection
			Late	rally					Late	erally			ပို့ ရှိ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	144.2 120.1	80.1 72.1 65.5 59.8 54.2 49.4 45.2	135.9 113.3 97.1 85.0 75.5 68.0 61.8 56.6 52.3 48.5 45.3	135.9 113.3 97.1 85.0 75.5 68.0 61.8 56.0 50.8 46.2 42.3 38.8	90.0 79.8 70.9 63.8 58.0 53.2 49.1 45.6 42.6	58.0 52.4 47.5 43.1 39.4	76.1 65.3 57.1 50.8 45.7 41.5 38.1 32.6	114.2 91.4 76.1 65.3 57.1 50.8 45.7 41.1 36.8 33.2 27.5 25.1	105.4 84.3 70.2 60.2 52.7 46.8 42.1 38.3 35.1 32.4 30.1 28.1 26.3	84.3 70.2 60.2 52.7 46.8 42.1 37.6 33.7 30.4 27.6 25.1 22.9		76.8 65.3 56.0 49.0 43.6 39.2 34.9 31.2 28.2 25.5 23.2 21.1 19.3	0.168 0.298 0.466 0.670 0.912 1.192 1.508 1.862 2.253 2.681 3.147 3.650 4.190 4.767 5.381 6.033 6.722 7.448

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

-			No	minal	Dept	h and	Flang	e Wid	th-W	Teight	per F	oot			
Span			Cl	B 101	10"	x6''				C	B 93	9"x9	"		Coefficient of Deflection
in Feet	30 1	lbs.	26	lbs.	23	Ibs.	21	lbs.	48	lbs.	43 1	bs.	38	lbs.	of of flec
reet				Late	rally						Late	rally			D C
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
4							54.7	54.7							0.298
4 5	73.1	73.1	62.8	62.8	55.2	55.2		52.2							0.466
6	63 8	63.8	55 3	55 3	48 0	18 0	13 5	43.5	00 2	00 1	70.0	WO 0	00.0	68.3	0.670
6 7 8 9	54.7	54.7	47.4	47.4	41.9	41 9	37.3	37.3	82 0	82.0	73 5	78.2	64 0		0.070
8								32.1							1.192
9	42.6	40.8	36.8	35.2	32.6	31.2	29.0	27.7	63.8	63.8	57.2	57.2	50.5	50.5	1.508
10	38.3	35.6	33.2	30.7	29.3	27.1	26.1	24.2	57.4	57.4	51.4	51.4	45.4	45.4	1.862
11	24 0	21 2	20.1	07.0	90 7	00.0	00.7	01.0	50.0	FO 0	40.0		11 0	41.0	0.050
12	31.0	28.6	27 6	99 0	20.7	23.8	23.7	$\frac{21.2}{18.8}$	17 9	02.2	40.8	46.8	41.3	41.3	2.253 2.681
13	29.5	24 6	25.5	21 3	22.6	18 7	20.1	16.7	44 2	49 7	20 6	90 9	35.0	33 8	3.147
14	27.4	21.9	23.7	19.0	20.9	16.7	18.6	14.9	41.0	38 0	36.7	34 0	32.5	30.7	3.650
15	25.5	19.7	22.1	17.0	19.5	15.0	17.4	13.3	38.3	35.6	34.3	31.8	30.3	28.1	4.190
			1			1									
16	23.9	17.7	20.7	15.3	18.3	13.5	16.3	12.0	35.9	32.5	32.2	29.1	28.4	25.7	4.767
17						12.1	15.3	10.8	33.8		30.3		26.7		5.381
18		14.5	18.4	12.5	16.3	}	14.5		31.9		28.6		25.2		6.033
19	20.2		17.5		15.4		13.7		30.2		27.1		23.9		6 722
20	19.2		16.6		14.7		13.0								7.448
21	18.2		15.8												8.212

CARNEGIE BEAM SECTIONS-Concluded

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

				Nomi	nal De	pth an	d Flang	e Widt	h-W	eight 1	per Foo	t		
	Span		С	B 92	9"x6]	/2"				CB 83	8"x	8''		Coefficient of Deflection
	in Feet	35	lbs.		lbs.	29	lbs.	42	lbs.		lbs.	31	lbs.	Coefficient of Deflection
	1000				erally						erally			ರೆ ದೆ
_		Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
		73.9	73.9	67.0	67.0	60.3	60.3	78.2	78.2	66.1	66.1	56.1	56.1	
	6 7	$\frac{67.6}{58.0}$		$61.8 \\ 53.0$		$\frac{56.0}{48.0}$	56.0 48.0		$\frac{74.8}{64.1}$	$64.1 \\ 54.9$	$64.1 \\ 54.9$	$\frac{55.0}{47.2}$	$\frac{55.0}{47.2}$	0.670
	8	50.7	50.7	46.4	46.4	42.0	42.0	56.1	56.1	48.0	48 0	41.3	41.3	$0.912 \\ 1.192$
	9	$\frac{45.1}{40.6}$		$\frac{41.2}{37.1}$	40.3	$37.3 \\ 33.6$	36.5	49.8 44.9		$\frac{42.7}{38.4}$	$\frac{42.7}{38.4}$	$\frac{36.7}{33.0}$	36 7 33.0	$\frac{1.508}{1.862}$
	11 12	36.9 33.8	$34.0 \\ 30.3$	33.7 30.9	$\frac{31.1}{27.6}$	$\frac{30.5}{28.0}$	28.2 24.9	40.8 37.4	$\frac{40.0}{36.6}$	34.9	$\frac{34.2}{30.6}$	$\frac{30.0}{27.5}$	29.4 26.3	$\frac{2.253}{2.681}$
	13	31.2	27.1	28.5	24.6	25.8	22.3	34.5	32.3	29.6	27 6	25.4	23.7	3.147
	14 15	$\frac{29.0}{27.1}$			$\frac{22.1}{19.9}$			32.0 29.9	29.3 26.6	27.5	25.0	$\frac{23.6}{22.0}$	21.5	3.650 4.190
								20.0	20.0	20.0		22.0		4.150
	16 17	$\frac{25.4}{23.9}$	19.7	$\frac{23.2}{21.8}$	17.9	21.0	16.3	28.0 26.4		24.0		20.6		4.767
	18	22.5		20,6		18.7		24.9		22.6		19.4		$\frac{5.381}{6.033}$
=	19	21 4		19.5	1	17.7				1				6.722
				Nomi	nal D	epth ar	nd Flang	ge Widt	th—V	eight	per Foo	ot		
	Span			CB 8	2 8	'x6½''				*B	10 9"	x5¼′′		Coefficient of Deflection
	in Feet	30	lbs.		27 lt	8.	24	lbs.		25 Ibs		21 1	bs.	Coefficient of Deflection
	1000				Latera	ally					Later	ally		De Co
_		Fixed	l Fre	e Fi	xed	Free	Fixed	Free	Fi	ked 1	Free	Fixed	Free	
	4				-									
	4 5								82	.1	82.1	,		
		58.6	58.	6 5	2.1	52,1	45.9	45,0	63	.7 6	3.7	54.0	54.0	0.298
			58.			52.1	45.9	45.9	- 63 50	.7 6 .9 5	3.7	46.7	46.7	0.466
		58.6 52.6 45.1	52. 45.	6 47	7.3	47.3 40.6	45.9 42.1 36.1	45.9 42.1 36.1	$-\frac{63}{50}$.7 6 .9 5	3.7 0.9 2.4	46.7 38.9	46.7 38.9	0.466
	6 7 8	52.6 45.1 39.5	52. 45. 39.	6 47 1 40 5 35	7.3 0.6 5.5	47.3 40.6 35.5	42.1 36.1 31.6	42.1 36.1 31.6	63 50 42 36 31	.7 6 .9 5 .4 4 .4 3 .8 3	3.7 0.9 2.4 6.1 0.6	38.9 33.4 29.2	38.9 32.9 27.8	0.466 0.670 0.912 1.192
		52.6 45.1	52. 45. 39. 34.	6 47 1 40 5 35 3 31	7.3 0.6 5.5 6	47.3 40.6	42.1 36.1	42.1 36.1	63 50 42 36	.7 6 .9 5 .4 4 .4 3 .8 3 .3 2	3.7 0.9 2.4 6.1 0.6 6.2	38.9 33.4 29.2 26.0	38.9 32.9 27.8 23.8	0.466 0.670 0.912 1.192 1.508
	6 7 8 9 10	52.6 45.1 39.5 35.1 31.6	52. 45. 39. 34. 30.	6 47 1 40 5 35 3 31 1 28	7.3 0.6 5.5 .6 3.4	47.3 40.6 35.5 30.9 27.0	42.1 36.1 31.6 28.1 25.3	42.1 36.1 31.6 27.5 24.0	63 50 42 36 31 28 25	.7 6 .9 5 .4 4 .4 3 .8 3 .3 2 .5 2	3.7 0.9 2.4 6.1 0.6 6.2 2.7	38.9 33.4 29.2 26.0 23.4	38.9 32.9 27.8 23.8 20.6	0.466 0.670 0.912 1.192 1.508 1.862
	6 7 8 9 10 11 12	52.6 45.1 39.5 35.1 31.6 28.7 26.3	52. 45. 39. 34. 30.	6 47 1 40 5 35 3 31 1 28 5 25 5 23	.3 0.6 5.5 .6 3.4 3.7	47.3 40.6 35.5 30.9 27.0 23.8 21.2	42.1 36.1 31.6 28.1 25.3 23.0 21.1	42.1 36.1 31.6 27.5 24.0 21.2 18.8	63 50 42 36 31 28 25 23 21	.7 6 .9 5 .4 4 .4 3 .8 3 .3 2 .5 2	3.7 0.9 2.4 6.1 0.6 6.2 2.7 9.8 7.4	38.9 33.4 29.2 26.0 23.4 21.2	46.7 38.9 32.9 27.8 23.8 20.6 17.9 15.7	0.466 0.670 0.912 1.192 1.508
	6 7 8 9 10 11 12 13	52.6 45.1 39.5 35.1 31.6 28.7 26.3 24.3	52. 45. 39. 34. 30. 26. 23. 21.	6 47 1 40 5 35 3 31 1 28 5 25 5 23 1 21	.3 .6 .5 .6 .4 .8 .7	47.3 40.6 35.5 30.9 27.0 23.8 21.2 18.9	42.1 36.1 31.6 28.1 25.3 23.0 21.1 19.4	42.1 36.1 31.6 27.5 24.0 21.2 18.8 16.8	63 50 42 36 31 28 25 23 21 19	.7 6 .9 5 .4 4 .4 3 .8 3 .3 2 .5 2 .1 1 .2 1 .6 1	3.7 0.9 2.4 6.1 0.6 6.2 2.7 9.8 7.4 5.3	38.9 33.4 29.2 26.0 23.4 21.2 19.5 18.0	46.7 38.9 32.9 27.8 23.8 20.6 17.9 15.7 13.8	0.466 0.670 0.912 1.192 1.508 1.862 2.253 2.681 3.147
	6 7 8 9 10 11 12	52.6 45.1 39.5 35.1 31.6 28.7 26.3	52. 45. 39. 34. 30. 26. 23. 21.	6 47 1 40 5 35 3 31 1 28 5 25 5 23 1 21 9 20	.3 .6 .5 .6 .4 .8 .7	47.3 40.6 35.5 30.9 27.0 23.8 21.2	42.1 36.1 31.6 28.1 25.3 23.0 21.1	42.1 36.1 31.6 27.5 24.0 21.2 18.8	63 50 42 36 31 28 25 23 21	.7 6 .9 5 .4 4 .4 3 .8 3 .3 2 .5 2 .1 1 .2 1 .6 1 .2 1	3.7 0.9 2.4 6.1 0.6 6.2 2.7 9.8 7.4 5.3 3.6	38.9 33.4 29.2 26.0 23.4 21.2	46.7 38.9 32.9 27.8 23.8 20.6 17.9 15.7	0.466 0.670 0.912 1.192 1.508 1.862 2.253 2.681
	6 7 8 9 10 11 12 13 14 15	52.6 45.1 39.5 35.1 31.6 28.7 26.3 24.3 22.6 21.1	52. 45. 39. 34. 30. 26. 23. 21.	6 47 1 40 5 35 3 31 1 28 5 25 5 23 1 21 9 20	7.3 0.6 5.5 6.8 3.4 6.8 8.7 9 0.3	47.3 40.6 35.5 30.9 27.0 23.8 21.2 18.9	42.1 36.1 31.6 28.1 25.3 23.0 21.1 19.4 18.1	42.1 36.1 31.6 27.5 24.0 21.2 18.8 16.8	63 50 42 36 31 28 25 23 21 19 18 17	.7 6 .9 5 .4 4 .4 3 .8 3 .3 2 .5 2 .1 1 .2 1 .6 1 .0 1	3.7 0.9 2.4 6.1 0.6 6.2 2.7 9.8 7.4 5.3 3.6 2.1	46.7 38.9 33.4 29.2 26.0 23.4 21.2 19.5 18.0 16.7 15.6	38.9 32.9 27.8 23.8 20.6 17.9 15.7 13.8 12.3 10.9	0.466 0.670 0.912 1.192 1.508 1.862 2.253 2.681 3.147 3.650 4.190
	6 7 8 9 10 11 12 13 14 15	52.6 45.1 39.5 35.1 31.6 28.7 26.3 24.3 22.6	52. 45. 39. 34. 30. 26. 23. 21. 18.	6 47 1 40 5 35 3 31 1 28 5 25 5 23 1 21 9 20	3.4 3.4 3.4 3.7 9	47.3 40.6 35.5 30.9 27.0 23.8 21.2 18.9	42.1 36.1 31.6 28.1 25.3 23.0 21.1 19.4 18.1	42.1 36.1 31.6 27.5 24.0 21.2 18.8 16.8	63 50 42 36 31 28 25 23 21 19 18	.7 6 .9 5 .4 4 .8 3 .3 2 .5 2 .1 1 .2 1 .0 1	3.7 0.9 2.4 6.1 0.6 6.2 2.7 9.8 7.4 5.3 3.6 2.1	38.9 33.4 29.2 26.0 23.4 21.2 19.5 18.0 16.7	46.7 38.9 32.9 27.8 23.8 20.6 17.9 15.7 13.8 12.3	0.466 0.670 0.912 1.192 1.508 1.862 2.253 2.681 3.147 3.650
	6 7 8 9 10 11 12 13 14 15	52.6 45.1 39.5 35.1 31.6 28.7 26.3 24.3 22.6 21.1	52. 45. 39. 34. 30. 26. 23. 21. 18.	6 47 1 40 5 35 3 31 1 28 5 25 5 23 1 21 9 20	7.3 0.6 5.5 0.6 3.4 3.4 3.8 3.7 0.3 3.9	47.3 40.6 35.5 30.9 27.0 23.8 21.2 18.9	42.1 36.1 31.6 28.1 25.3 23.0 21.1 19.4 18.1	42.1 36.1 31.6 27.5 24.0 21.2 18.8 16.8	63 50 42 36 31 28 25 23 21 19 18 17	.7 6.9 5 .4 4.4 3.8 3.3 22.5 2 .1 1 1.2 1 1.6 1 1.2 1 1.0 1 1.9 1	3.7 0.9 2.4 6.1 0.6 6.2 2.7 9.8 7.4 5.3 3.6 2.1	46.7 38.9 33.4 29.2 26.0 23.4 21.2 19.5 18.0 16.7 15.6	38.9 32.9 27.8 23.8 20.6 17.9 15.7 13.8 12.3 10.9	0.466 0.670 0.912 1.192 1.508 1.862 2.253 2.681 3.147 3.650 4.190 4.767

STANDARD MILL SECTIONS

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 18,000 Pounds per Square Inch

		1	Vomina	al Der	oth and	l Flange	e Width	ı—Wei	ght per	Foot			
Span		B 39	8"x5	"				H 4	8"x8	"			Coefficient of Deflection
in Feet	21	lbs.		18 lb	8.	37.7	lbs.		1.3 lbs.		32.6	lbs.	of of effec
reet			terally					-	terally				ŭÁ
	Fixed	Free	Fix	ed :	Free	Fixed	Free	Fixe	d Fr	ee F	ixed	Free	
3 4 5	69.1 63.4 47.6 38.1	$ \begin{array}{r} 69.1 \\ \hline 63.4 \\ 47.6 \\ 38.1 \end{array} $	44.	1 4	48.0 14.1 35.2	96.0 90.6 72.5	96.0 90.6 72.5	72.0 69.4			30.1	60.1	0.168 0.298 0.466
6 7 8 9 10	31.7 27.2 23.8 21.1 19.0	31.7 26.6 22.5 19.2 16.6	25. 22. 19.	2 2 2 2 3 3 4 5 6 1	29.4 24.5 20.7 17.7 15.2	60.4 51.8 45.3 40.3 36.2	60.4 51.8 45.3 40.3 36.2	57.3 49.4 43.4 38.3 34.7	5 49 4 43 5 38	.5 4 .4 4 .5 3	6.4 8.3 2.3 7.6 3.8	56.4 48.3 42.3 37.6 33.8	$\begin{array}{c} 0.670 \\ 0.912 \\ 1.192 \\ 1.508 \\ 1.862 \end{array}$
11 12 13 14 15	17.3 15.9 14.6 13.6	.9 12.6 14.7 11. .6 11.1 13.6 10. .6 9.8 12.6 9. .7 11.0				32.9 30.2 27.9 25.9	32.3 29.0 26.1 23.7	31.3 28.9 26.24.3 23.1	$ \begin{array}{c c} 0 & 27 \\ 7 & 24 \\ 8 & 22 \end{array} $.6 2 .9 2 .6 2	0.8 28.2 26.0 24.2 22.6	30.0 26.9 24.2 21.9	2.253 2.681 3.147 3.650 4.190
16 17	11.9 11.2					22.7 21.3		21.7			21.2		4.767 5.381
			Nomin	al De	pth an	d Flang	ge Widt	h—We	eight pe	er Foot	t		
Span]	H 3 A	6"x6"	,	1	Н 3	6"x6"		H 2 5	5''x5''	H 1	4"x4"	ient
in	27.5	Ibs.	25	lbs.	22	.5 lbs.	20	lbs.	18.9			8 lbs.	Coefficient of Deflection
Feet		Late			-		erally		Late			erally	ರೆ ಗ
	Fixed	Free	Fixed	Free	Fixe	l Free	Fixed	Free	Fixed	Free	Fixed	Free	
3 4 5	63.1 49.3 39.4	63.1 49.3 39.4	$\frac{45.1}{37.6}$	45.1 37.6		41.0	36.0 31.0	36.0	$\frac{37.6}{28.5}$ 22.8	$\frac{37.6}{28.5}$ 22.8	$ \begin{array}{r} 30.0 \\ 21.2 \\ 15.9 \\ 12.7 \end{array} $	$\begin{array}{r} 30.0 \\ \hline 21.2 \\ 15.9 \\ 12.7 \end{array}$	0.168 0.298 0.466
6 7	32.9 28.2		$\frac{31.4}{26.9}$			27.4 23.4	$25.9 \\ 22.2$	$\frac{25.9}{22.2}$		19.0 15.9	10.6	10.1	$0.670 \\ 0.912$
8	24.6	24.4	23.5	23.1	20.8	20.3	19.4	19.0	14.3	13.4	9.1	8.3	1.192
9 10	$\frac{21.9}{19.7}$		$\frac{20.9}{18.8}$	$\frac{19.9}{17.3}$	18.2	17.5	$17.2 \\ 15.5$	$16.4 \\ 14.3$	12.7 11.4		7.1		1.508 1.862
11 12 13	17.9 16.4 15.2		17.1 15.7 14.5		14.6 13.5 12.6		14.1 12.9 11.9	110	10.4		0.3		2.253 2.681 3.147

COLUMNS AND STRUTS

A compression member, subjected to longitudinal pressure, is shortened by the compression and also tends to deflect laterally, due to the fact that the load cannot be applied coincident with the longitudinal axis and that the material is not perfectly homogeneous. This flexure occurs generally in the direction of the least resisting moment of the section; the load which will cause a column to fail decreases in the ratio of length to least lateral resistance of the section, the ultimate failure being the result of combined stresses due to compression, transverse shear and flexure.

Column Formulas. Under ideal conditions, when it can be assumed that the load is applied axially and that the material is perfectly homogeneous, the resistance of the column would equal its resistance to compressive forces up to the elastic limit, and there would not be any flexure; if, however, a deflection be imparted to the column by a lateral force, the column would ultimately fail by bending.

Euler's Formula, $P = k \frac{\pi^2 E I}{l^2}$ or $\frac{P}{A} = k \frac{\pi^2 E}{(l/r)^2}$, is based upon the foregoing theory, and gives results close to the ultimate strength found for long and slender struts, when k is a constant varying with the condition of end bearing, (k=4 for columns fixed both ends). For shorter and heavier columns, or for lower ratios of l/r the results do not correspond with actual tests.

Rankine's Formula, $P = \frac{Af}{1+c~(1/r)^2}$ or $\frac{P}{A} = \frac{f}{1+c~(1/r)^2}$, represents the type of formula now in general use and the various formulas for proportioning columns which are based upon this general formula agree with actual tests within certain limits. In this formula a certain compressive unit stress for direct crushing is assumed and reduced in ratio of length of column and least radius of gyration, 1/r; value of c is an empirical factor, varying with the resistance of the material and with conditions of end bearing.

Straight Line Formulas. In practice, compression members of a greater ratio of slenderness, 1/r, than 120 are rarely used, and within this limit the curve can be represented by a straight line, the general formula assuming the simpler form: $\frac{P}{A} = f - c \left(\frac{1}{r}\right)$.

Compression formulas determining the resistance of webs in rolled beams or riveted girders against buckling, or the necessary reduction of safe loads due to lateral deflection of unbraced beams, are likewise based on one or the other type of column formulas.

Ratio of Slenderness. 1/r is ratio of the unsupported length of a compression member to its radius of gyration, generally the least radius, excepting when the unsupported length is rigidly braced to prevent deflection in the direction which corresponds to the least radius of gyration. It is, therefore, necessary to determine the radii of gyration and to use the proper ratio of slenderness in any particular case.

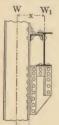
Usual practice limits the maximum ratio of l/r for main members under permanent stress, permitting a higher ratio for secondary members under temporary stress, as in wind bracing.

Compressive Unit Stresses. The tables of allowable loads of column sections have been computed in accordance with the formula for steel columns of American Institute of Steel Construction—1923,

$$f = \frac{18,000}{1 + \frac{1}{18,000} (l/r)^2},$$

Maximum unit stress at l/r=60 : 15,000 lb. per sq. inch. Maximum l/r: Primary members=120; Secondary members=200.

Combined Bending and Compression Stresses. Generally the loads are concentric and equally distributed over the cross section of the column or balanced on opposite sides thereof. In the case of beams carried on brackets or other forms of eccentric loading, bending stresses are produced which should be taken into consideration and the column sections so proportioned that the combined stresses do not exceed the allowable axial compressive stress.



W = Concentric load. W₁ = Eccentric load.

M =Bending moment due to eccentric load=W1x.

I = Moment of inertia in direction of bending.

n =Distance from extreme fiber in direction of bending.

A =Area of column section, in square inches.

f =Allowable axial unit stress; f should be equal to or greater than $\frac{W+W_1}{A} + \frac{Mn}{I}$, the fiber stresses due to compression and bending respectively.

Example:—Required a beam column, 25 feet long, to sustain a balanced load of 220,000 pounds and an eccentric load of 40,000 pounds applied 17 inches from the column center on axis 1-1.

Assume Carnegie Beam Section CB-165, 16"x14", 100 lb.

$$A = 29.41$$
 $I_{1-1} = 1426.8$ $r_{2-2} = 3.53$ $1/r = 25x12 \div 3.53 = 85$

Actual fiber stress = $\frac{220,000+40,000}{29.41} + \frac{40,000x17x8}{1426.8} = 12,653$ pounds.

This stress is within the limits of the allowable fiber stress for ratio of 1/r = 85, 12,844 pounds, obtained from the column formula.

ALLOWABLE UNIT STRESSES IN POUNDS PER SQUARE INCH

by Compression Formula of

American Institute of Steel Construction: $f = \frac{18,000}{1 + \frac{1}{18,000} (l/r)^2}$

The following tables give the unit stresses for ratios of l/r in intervals of 5/10. Intermediate values may be found by interpolation from the figures given for the tenth units of l/r by adding or deducting from the nearest tabulated figure the corresponding multiple.

Example: Unit stress for 1/r=94.7 and 1/r=150.8 1/r= 94.7 11989 +3x8.4 or 12031-2x8.4=12014 1/r=150.8 7941 +2x5.9 or 7971-3x5.9=7953

MAIN MEMBERS-Ratios of 1/r up to 120

			-								
Ratio,	Unit Stress,	Diff. 0.10	Ratio,	Unit Stress,	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10
1/1	Pounds	0.10	1/1	Pounds	0.10		rounds		-/-	rouncs	
60	15000			13714			12414			11163	
.5	14958	8.4		13671	8.7		12371	8.6		11122	8.1
61	14916		76	13627			12328			11082	
.5	14874	8.4	.5	13584	8.7		12286	8.5		11042	8.0
62	14832		77	13540		92	12243			11002	
.5	14790	8.4	.5	13496	8.7	.5	12201	8.5		10962	8.0
63	14748		78	13453		93	12158		108	10922	
.5	14705	8.5	.5	13409	8.7	.5	12116	8.5	.5	10883	7.9
64	14663		79	13366		94	12073		109	10843	
.5	14621	8.5	.5	13322	8.7	.5	12031	8.4	.5	10804	7.9
65	14578		80	13279		95	11989		110	10764	
.5	14535	8.5	.5	13235	8.7	.5	11947	8.4	.5	10725	7.9
66	14493		81	13192		96	11905		111	10686	
.5	14450	8.6	.5	13148	8.7	.5	11863	8.4	.5	10647	7.8
67	14407		82	13105		97	11821		112	10608	
.5	14364	8.6	.5	13061	8.7	.5	11779	8.4	.5	10569	7.8
68	14321		83	13018		98	11737		113	10530	
.5	14278	8.6	.5	12974	8.7	.5	11696	8.3	.5	10491	7.7
69	14235		84	12931		99	11654		114	10453	
.5	14192	8.7	.5	12888	8.7	.5	11613	8.3	.5	10415	7.7
70	14148		85	12844			11571		115	10376	
.5	14105	8.7	.5	12801	8.6	.5	11530	8.2	.5	10338	7.6
71	14062		86	12758		101	11489		116	10300	
.5	14019	8.7	.5	12715	. 8.6		11448	8.2	.5	10262	7.6
72	13975		87	12672		102	11407		117	10224	
.5	13932	8.7	.5	12629	8.6	.5	11366	8.2	.5	10187	7.5
73	13888		88	12585		103	11325		118	10149	
.5	13845	8.7	.5	12542	8.6		11284	8.2	.5	10112	7.5
74	13801	011	89	12500	0.0	104	11244	0.2		10074	
.5	13758	8.7	.5	12457	8.6		11203	8.1		10037	7.4
75	13714	0.1		12414			11163	014	120		
10	TOLLY		11 30	TATIT		1 200	11100		,, 1=0	,_0000	

ALLOWABLE UNIT STRESSES IN POUNDS PER SQUARE INCH by Compression Formula of

American Institute of Steel Construction: $f = \frac{18,000}{1 + \frac{1}{18,000} \, (l/r)^2}$

SECONDARY MEMBERS—Ratios of 1/r up to 200

					v						
Ratio,	Unit	Diff.	Ratio,	Unit	Diff.	D-41-	Unit	D'm	D	Unit	D:00
l/r	Stress,	0.10	l/r	Stress,	0.10	Ratio,	Ducos,	Diff. 0.10	Ratio,	Lucas,	Diff. 0.10
-/-	Pounds	0120	1/1	Pounds	0.10	1/1	Pounds	0.10	1/1	Pounds	0.10
										1	
120	10000		140	8617		160	7431		180	6429	
.5	9963	7.4	.5	8585	6.4	.5	7404	5.4	.5	6406	4.6
121	9926		141	8553		161	7377		181	6383	1.0
.5	9890	7.3	.5	8521	6.3	.5	7350	5.4	.5	6360	4.5
122	9853		142	8490		162	7323		182	6338	1.0
.5	9816	7.3	.5	8458	6.3	.5	7296	5.4	.5	6315	4.5
123	9780		143	8427	0.0	163	7269	011	183	6293	1.0
.5	9744	7.2	.5	8396	6.3	.5	7243	5.3	.5	6270	4.5
124	9708		144	8364	0.0	164	7217	0.0	184	6248	4.0
.5	9672	7.2	.5	8333	6.2	.5	7190	5.3	.5	6226	4.4
125	9636		145	8302	0.2	165	7164	0.0	185	6204	4.4
.5	9600	7.1	.5	8272	6.1	.5	7138	5.2			4.4
126	9564	1.1	146	8241	0.1	166	7112	0.2	186	6182	4.4
.5	9529	7.1	.5	8210	6.1		7086	5.2			4.0
127	9493	4.1	147	8180	0.1	167		5.2	.5	6139	4.3
	9458	7.0			0.1		7061	F 4	187	6117	4.0
128	9423	1.0	.5	8150	6.1	.5	7035	5.1	.5	6095	4.3
		7.0	148	8119	0.0	168	7009		188	6074	
129	9388	7.0	.5	8089	6.0	.5	6984	5.1	.5	6053	4.3
	9353	0.0	149	8060	0.0	169	6959		189	6031	
.5	9318	6.9	.5	8030	6.0	.5	6934	5.0	.5	6010	4.2
130	9284	0.0	150	8000	~ .	170	6908		190	5989	
.5	9249	6.9	.5	7971	5.9	.5	6883	5.0°	.5	5968	4.2
131	9215		151	7941		171	6858		191	5947	
.5	9181	6.8	.5	7912	5.9	.5	6834	4.9	.5	5926	4.2
132	9146	1	152	7882		172	6809		192	5906	
.5	9112	6.8	.5	7853	5.8	.5	6785	4.9	.5	5885	4.1
133	9078		153	7824		173	6760		193	5864	
.5	9045	6.7	.5	7796	5.8	.5	6736	4.9	.5	5844	4.1
134	9011		154	7767		174	6711		194	5824	
.5	8978	6.7	.5	7738	5.7	.5	6687	4.8	.5	5803	4.0
135	8944		155	7710		175	6663		195	5783	
.5	8911	6.6	.5	7681	5.7	.5	6639	4.8	.5	5763	4.0
136	8878		156	7653		176	6615		196	5743	
.5	8845	6.6	.5	7625	5.6	.5	6592	4.7	.5	5723	3.9
137	8812		157	7597		177	6568		197	5703	
.5	8779	6.5	.5	7569	5.6	.5	6545	4.7	.5	5684	3.9
138	8746		158	7541		178	6521		198	5664	
.5	8714	6.5	.5	7514	5.5	.5	6498	4.7	.5	5643	3.9
139	8681		159	7486		179	6475		199	5624	
.5	8649	6.4	.5	7459	5.5	.5	6452	4.6	.5	5606	3.9
140	8617		160	7431		180	6429		200	5586	
										1	

CARNEGIE BEAM SECTIONS

18-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

			Nominal	Depth ar	d Flange	Width-	-Weight 1	per Foot		
Effective Length	CB:	183 18"	x12"	CB 1	82 18"x	81/2"		CB 181	18"x7½	"
in Feet	100	93	86	78	72	67	58	52	51	47
	lbs.	1bs.	1bs.	1bs.	lbs.	lbs.	lbs.	1bs.	lbs.	lbs.
6	441	410	379	344	318	296	256	$ \begin{array}{r} 230 \\ 230 \\ 230 \\ \hline 224 \\ 215 \end{array} $	225	207
7	441	410	379	344	318	296	256		225	207
8	441	410	379	344	318	296	256		225	207
9	441	410	379	344	318	296	251		218	202
10	441	410	379	344	316	294	240		208	193
11	441	410	379	332	306	284	230	205	199	185
12	441	410	379	320	295	273	219	196	189	176
13	441	410	379	308	283	263	209	186	180	168
14	441	410	379	296	272	252	199	177	171	159
15	438	407	375	284	261	242	189	168	162	151
16	428	397	367	272	250	232	180	160	153	143
17	417	388	358	261	240	222	171	151	145	136
18	407	378	349	250	229	212	162	144	137	129
19	396	368	339	239	219	203	154	136	130	122
20	386	358	330	228	210	194	146	129	123	116
21	375	349	321	218	201	186	138	122	117	110
22	365	339	312	209	192	177	131	116	111	104
23	355	329	304	200	183	170	125	110	105	99
24	345	320	295	191	175	162	118	105	100	94
25	335	311	286	182	167	155	112	99	94	89
26 27 28 29 30	$\begin{array}{r} 325 \\ 316 \\ 306 \\ 297 \\ \hline 288 \end{array}$	302 293 284 276 267	278 270 262 254 246	175 167 160 153 147	160 153 147 140 134	148 142 135 130 124	107 102 97	94 90 85	90 85	85 80
31 32 33 34 35	280 271 263 255 248	259 251 244 237 229	239 231 224 218 211	140 135 129	129 123 118	119 114				-
Area, in. 2	29.40	27.35	25.29	22.94	21.17	19.69	17.05	15.30	15.00	13.82
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	1783.4	1648.4	1514.1	1318.8	1208.1	1117.1	960.8	855.1	810.0	768.6
	7.79	7.76	7.74	7.58	7.55	7.53	7.51	7.48	7.35	7.46
	253.4	234.0	214.7	90.9	82.9	76.4	49.0	43.3	40.5	38.7
	2.94	2.93	2.91	1.99	1.98	1.97	1.70	1.68	1.64	1.67
Weight Lbs. per Foot	l .	93	86	78	72	67	58	52	51	47

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to 1201/r and those below lower zig-zag line are for ratios not over 2001/r.

CARNEGIE BEAM SECTIONS—Continued

16-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

				Nom	inal I	epth a	and Fla	ange V	Vidth-	-Weig	ht per	Foot			
Effective Length in Feet		CB 16 16"x14			CB 16 6"x12			CB 16 6"x8½				162 'x7''	-		161 'x6''
m reet	115 lbs.	107 1bs.	100 lbs.	90 lbs.	83 1bs.	76 1bs.	68 lbs	63 1bs.	58 1bs.	50 lbs.	45 lbs.	43 1bs.	40 lbs.	38 1bs.	35 Ibs.
6 7 8 9	507 507 507 507 507	472 472 472 472 472	441 441 441 441	397 397 397 397 397	366 366 366 366 366	335 335 335 335 335	300 300 300 300 300	278 278 278 278 278	256 256 256 256 256	221 221 221 212 202	198 198 198 190 181	190 190 186 177 169	176 176 176 168 161	168 164 155 146 137	154 150 142 134 126
11 12 13 14 15	507 507 507 507 507	472 472 472 472 472	441 441 441 441	397 397 397 397 395	366 366 366 364	335 335 335 335 332	291 281 270 260 250	269 259 250 240 231	247 238 230 221 212	193 183 174 165 156	173 164 156 148 140	160 151 143 135 127	153 145 138 131 124	129 120 112 105 98	118 110 103 96 90
16 17 18 19 20	507 507 505 495 485	472 472 469 460 451	441 441 438 430 421	386 376 367 358 348	355 347 338 329 321	324 316 308 300 292	240 230 220 211 202	221 212 203 194 186	203 195 186 178 171	148 140 132 125 118	132 125 118 112 106	120 113 107 100 95	117 110 104 99 93	92 86 80 75 70	84 78 73 68 64
21 22 23 24 25	476 466 456 446 436	442 433 423 414 405	413 404 395 386 378	339 330 320 311 302	312 303 295 287 278	284 277 269 261 253	193 185 177 169 162	178 170 163 156 149	163 156 149 143 136	112 106 101 95 90	100 95 90 85 81	89 84 80 75 71	88 84 79 75 71	66	60
26 27 28 29 30	426 416 406 397 387	396 386 377 368 360	369 361 352 344 336	294 285 277 269 261	$\begin{array}{c} 270 \\ 262 \\ 255 \\ 247 \\ \hline 240 \\ \end{array}$	246 239 232 225 218	155 148 142 136 130,	143 136 131 125 120	131 125 120 114 110	86	77				
31 32 33 34 35	378 369 360 351 342	351 342 334 326 318	327 319 312 304 296	253 245 238 231 224	233 226 219 212 206	211 205 199 193 187	125 120 115	115 110 106	105 101 97						
Area,in.2	33.82	31.46	29.41	26.46	24.41	22.34	20.00	18.52	17.06	14.70	13.23	12.65	11.75	11.17	10.29
I1-1, in ⁴ r1-1, in. I2-2, in. ⁴ r2-2, in.	7.02	1537.2 6.99 393.9 3.54	6.97	1275.5 6.94 230.0 2.95	6.92	6.89	923.7 6.80 81.3 2.02	849.9 6.77 74.6 2.01	776.6 6.75 68.0 2.00	666.0 6.73 38.2 1.61	595.0 6.71 34.0 1.60	523.8 6.44 28.9 1.51	524.6 6.68 29.8 1.59	475.1 6.52 19.2 1.31	435.5 6.50 17.5 1.30
Weight Lbs. per Foot	115	107	100	90	83	76	68	63	58	50	45	43	40	38	35

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120\ 1/r$ and those below lower zig-zag line are for ratios not over $200\ 1/r$.

CARNEGIE BEAM SECTIONS—Continued

14-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

			Nominal	Donth or	d Florac	Width_	-Woight 1	per Foot		
Effective			Moninga			14"x15"	11018111	per 1 000		
Length	305	295	285	275	265	255	245	235	225	215
in Feet	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	1bs.	lbs.	lbs.
11 12 13 14 15	1346 1346 1346 1346 1346	1301 1301 1301 1301 1301	1257 1257 1257 1257 1257 1257	1213 1213 1213 1213 1213 1213	1169 1169 1169 1169 1169	1125 1125 1125 1125 1125 1125	1081 1081 1081 1081 1081	1037 1037 1037 1037 1037	993 993 993 993 993	949 949 949 949 949
16 17 18 19 20	1346 1346 1346 1346 1346	1301 1301 1301 1301 1301	1257 1257 1257 1257 1257 1257	1213 1213 1213 1213 1213	1169 1169 1169 1169 1169	$\begin{array}{c} 1125 \\ 1125 \\ 1125 \\ 1125 \\ 1125 \\ 1125 \end{array}$	1081 1081 1081 1081 1081	1037 1037 1037 1037 1037	993 993 993 993 993	949 949 949 949 949
21	1339	1294	1249	1203	1158	1114	1069	1024	979	935
22	1317	1273	1229	1183	1139	1095	1051	1006	963	919
23	1295	1251	1208	1163	1120	1076	1033	989	946	902
24	1272	1229	1187	1143	1100	1057	1014	971	929	886
25	1250	1208	1165	1122	1080	1038	996	953	912	870
26	1227	1186	1144	1101	1060	1019	977	936	895	853
27	1205	1164	1123	1081	1040	1000	959	918	878	837
28	1182	1142	1102	1060	1020	980	940	900	860	821
29	1159	1120	1080	1040	1000	961	922	882	843	804
30	1137	1098	1059	1019	981	942	903	864	826	788
31	1115	1077	1038	999	961	923	885	847	810	772
32	1092	1055	1018	979	942	905	867	830	793	756
33	1070	1034	997	959	922	886	849	812	777	740
34	1049	1013	977	939	903	868	832	795	760	725
35	1027	992	957	920	885	850	814	779	744	709
36	1006	971	937	900	866	832	797	762	728	694
37	985	951	917	881	848	814	780	746	713	679
38	965	931	898	863	830	797	763	730	697	664
39	944	911	879	844	812	780	747	714	682	650
40	924	892	860	826	795	763	731	699	668	636
Area, in.2	89.70	86.76	83.82	80.87	77.93	74.99	72.06	69.11	66.17	63.23
I ₁₋₁ , in. ⁴	4121.5	3948.1	3778.1	3607.8	3442.4	3280.0	3119.6	2961.9	2806.2	2654.7
r ₁₋₁ , in.	6.78	6.75	6.71	6.68	-6.65	6.61	6.58	6.55	6.51	6.48
I ₂₋₂ , in. ⁴	1539.1	1479.4	1420.7	1362.0	1304.2	1247.1	1190.6	1134.5	1079.1	1024.5
r ₂₋₂ , in.	4.14	4.13	4.12	4.10	4.09	4.08	4.06	4.05	4.04	4.03
Weight Lbs. per Foot	305	295	285	275	265	255	245	235	225	215

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120\ l/r$ and those below lower zig-zag line are for ratios not over $200\ l/r$.

CARNEGIE BEAM SECTIONS—Continued

14-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

			Nomin	al Deptl	and Fl	ange Wi	dth-W	eight per	r Foot		
Effective Length					CB 1	46 14"	x15"				
in Feet	205	195	185	175	165	155	145	135	131	125	115
	Ibs.	1bs.	lbs.	lbs.	lbs.	1bs.	lbs.	lbs.	lbs.	lbs.	lbs.
11 12 13 14 15	904 904 904 904 904	860 860 860 860 860	816 816 816 816 816	772 772 772 772 772 772	728 728 728 728 728 728	684 684 684 684	640 640 640 640 640	596 596 596 596 596	578 578 578 578 578	551 551 551 551 551	507 507 507 507 507
16 17 18 19 20	904 904 904 904 904	860 860 860 860 860	816 816 816 816 815	772 772 772 772 772 770	728 728 728 728 725	684 684 684 680	640 640 640 640 636	596 596 596 596 591	578 578 578 576 566	551 551 551 551 547	507 507 507 507 502
21	890	846	801	757	713	668	625	581	555	537	494
22	874	831	787	744	700	657	614	570	545	527	485
23	859	816	773	730	688	645	602	560	534	518	476
24	843	801	759	717	675	633	591	549	524	508	467
25	828	786	745	703	662	621	580	539	513	498	458
26	812	771	731	690	649	608	568	528	502	488	448
27	796	756	716	676	637	596	557	518	492	478	439
28	781	741	702	663	624	584	546	507	481	468	430
29	765	727	688	649	611	572	535	497	471	459	421
30	749	712	674	636	599	560	523	486	460	449	413
31	734	697	660	623	586	549	512	476	450	439	404
32	719	683	646	610	574	537	502	466	440	430	395
33	704	668	632	597	561	526	491	456	430	421	386
34	689	654	6 7 9	584	549	514	480	446	420	411	378
35	674	640	606	571	538	503	470	436	410	402	369
36	660	626	593	559	526	492	459	426	401	393	361
37	645	613	580	547	514	481	449	417	392	385	353
38	631	599	567	535	503	470	439	407	382	376	345
39	618	586	554	523	492	460	429	398	374	368	337
40	604	573	542	511	481	450	420	389	365	359	330
Area, in. 2	60.28	57.34	54.41	51.47	48.52	45.58	42.64	39.70	38.52	36.75	33.82
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	2505.0	2358.2	2213.5	2071.7	1932.6	1796.8	1662.7	1530.4	1358.4	1402.1	1275.9
	6.45	6.41	6.38	6.34	6.31	6.28	6.24	6.21	5.94	6.18	6.14
	970.3	916.8	863.9	811.6	759.9	709.0	658.5	608.4	547.3	559.4	510.9
	4.01	4.00	3.98	3.97	3.96	3.94	3.93	3.92	3.77	3.90	3.89
Weight Lbs. per Foot	205	195	185	175	165	155	145	135	131	125	115

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120\,1/r$ and those below lower zig-zag line are for ratios not over $200\,1/r$.

CARNEGIE BEAM SECTIONS—Continued

14-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

				Nomi	nal De	epth a	nd Fla	nge W	idth-	Weigh	it per	Foot			
Effective Length		B 145 4"x12			B 144 4"x10			B 143 4"x8"				CB 142 L''x63/4			CB 141 14"x6"
in Feet	105 lbs.	95 lbs.	85 lbs.	75 lbs.	68 lbs.	61 1bs.	58 1bs.	53 lbs.	48 lbs.	42 lbs.	39 lbs.	38 1bs.	36 lbs.	33 1bs.	30 lbs.
6 7 8 9 10	463 463 463 463 463	419 419 419 419 419	375 375 375 375 375	331 331 331 331 331	300 300 300 300 300 300	269 269 269 269 269	$\begin{array}{c} 256 \\ 256 \\ 256 \\ 256 \\ 256 \\ \hline 252 \end{array}$	234 234 234 234 230	212 212 212 212 212 208	185 185 184 176 167	172 172 171 163 155	168 168 163 155 147	159 159 157 150 143	146 146 144 137 131	132 130 123 116 109
11 12 13 14 15	463 463 463 463	419 419 419 419 419	375 375 375 375 375	331 331 325 316 306	300 300 294 286 277	269 269 263 256 248	243 234 225 215 206	222 213 205 196 188	200 193 185 177 170	159 151 143 135 128	148 140 133 126 119	139 131 124 117	136 129 122 115 109	124 118 111 105 99	103 96 90 84 79
16 17 18 19 20	457 447 437 426 416	413 403 394 384 375	369 360 352 343 335	297 288 279 269 260	269 260 252 244 235	240 233 225 217 210	197 189 180 172 164	180 172 164 157 149	162 155 148 141 135	121 114 108 102 96	112 106 100 94 89	103 97 91 86 81	103 97 92 86 82	94 88 84 79 74	74 69 64 60 57
21 22 23 24 25	405 395 384 374 364	$\frac{346}{337}$	326 318 309 301 293	251 243 234 226 218	$\begin{array}{c} 227 \\ 219 \\ 212 \\ 204 \\ \hline 197 \end{array}$	203 196 189 182 175	157 150 143 136 130	143 136 130 124 118	129 123 117 112 107	91 86 81 77 73	84 80 75 71 68	76 72 68 64	77 73 69 65 62	70 66 63 59 56	53 50
26 27 28 29 30	354 344 335 325 316	310	284 276 269 261 254	210 203 196 189 182	190 183 177 170 164	169 163 157 152 146	124 119 114 109 104	113 108 103 99 94	102 97 93 89 85	69	64				
31 32 33 34 35	307 298 290 281 273	276 268 260 253 246	246 239 232 226 219	176 169 163 158 152	158 153 147 142 137	141 136 131 126 122	99 95	90	81						
Area,in.2	30.88	27.93	24.99	22.05	19.99	17.94	17.05	15.59	14.12	12.35	11.47	11.18	10.58	9.71	8.82
I1-1, in.4 r1-1, in. I2-2, in.4 r2-2, in.	6.15	1044.0 6.11 262.0 3.06	6.07	6.11	738.8 6.08 120.6 2.46	656.2 6.05 107.1 2.44	609.4 5.98 62.8 1.92	552.5 5.95 56.8 1.91	5.93 50.8 1.90	431.5 5.91 30.2 1.56	398.3 5.89 27.7 1.56	357.5 5.66 24.2 1.47	365.6 5.88 25.4 1.55	333.4 5.86 23.0 1.54	292.0 5.75 15.5 1.33
Weight Lbs. per Foot	105	95	85 shows	75	68	61	58	53	48	42	39 over 6	38	36 se bet	33 ween	30 zig-zag

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120 \, 1/r$ and those below lower zig-zag line are for ratios not over $200 \, 1/r$.

CARNEGIE BEAM SECTIONS—Continued

12-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

			N	ominal	Depth	and Fla	ange W	idth—	Weight	per Fo	ot		
Effective Length		CB 12	27 12'	'x14''	1	CH	3 126	12"x14	L''	Cl	B 125	12"x12	2"
in Feet	230	220	210	200	190	180	170	160	150	140	130	120	110
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	1bs.	lbs.	lbs.	lbs.	Ibs.	lbs.	lbs.
11 12 13 14 15	1015 1015 1015 1015 1015	971 971 971 971 971	926 926 926 926 926 926	882 882 882 882 882	838 838 838 838 838	794 794 794 794 794	750 750 750 750 750 750	706 706 706 706 706	662 662 662 662 662	618 618 618 618 618	574 574 574 574 574	529 529 529 529 529	485 485 485 485 485
16	$1015 \\ 1015 \\ 1015 \\ 1009 \\ 991$	971	926	882	838	794	750	706	662	605	563	521	480
17		971	926	882	838	794	750	706	662	591	550	509	469
18		971	926	882	838	794	750	706	662	576	537	497	458
19		964	920	875	831	782	740	698	655	562	524	485	448
20		947	903	859	816	768	726	684	643	548	510	473	437
21	972	929	886	843	801	753	712	671	631	533	497	461	426
22	954	911	869	826	785	737	697	658	618	519	484	449	415
23	935	893	851	810	769	722	683	645	606	505	471	437	404
24	916	875	834	793	754	707	669	631	593	491	458	426	393
25	897	857	817	777	738	692	654	618	581	478	446	414	383
26	878	839	799	760	722	677	640	604	568	464	433	403	373
27	859	821	782	744	706	662	626	591	556	451	421	391	362
28	841	803	765	727	691	647	612	578	544	438	409	380	352
29	822	785	748	711	676	632	598	565	532	425	397	370	342
30	804	767	731	695	660	617	584	552	519	413	386	359	333
31	786	750	715	679	645	603	571	539	508	401	375	349	323
32	768	733	698	664	631	589	557	527	496	389	364	339	314
33	750	716	682	648	616	575	544	514	484	378	353	329	305
34	733	700	666	633	602	561	531	502	473	367	343	319	297
35	716	683	651	618	588	548	519	490	462	356	333	310	288
36 37 38 39 40	699 683 667 651 636	667 652 636 621 607	636 621 606 592 578	590 576 562 549	574 560 547 534 521	535 522 509 497 485	506 494 482 470 459	479 467 456 445 434	451 440 430 419 409	346 336 326 316 307	323 314 305 296 287	301 293 284 276 268	280 272 264 257 250
Ārea, in.2	67.64	64.70	61.76	58.82	55.88	52.94	50.00	47.06	44.12	41.18	38.24	35.28	32.34
I ₁₋₁ , in. ⁴	1461.9	1426.6	1391.3	1356.1	1320.8	1218.1	1182.8	1147.5	1112.2	934.8	899.5	864.1	828.8
r ₁₋₁ , in.	4.65	4.70	4.75	4.80	4.86	4.80	4.86	4.94	5.02	4.76	4.85	.4.95	5.06
I ₂₋₂ , in. ⁴	945.5	898.2	852.9	809.5	767.8	702.4	666.9	633.0	600.4	372.4	350.5	329.6	309.9
r ₂₋₂ , in.	3.74	3.73	3.72	3.71	3.71	3.64	3.65	3.67	3.69	3.01	3.03	3.06	3.10
Weight Lbs. per Foot	230	220	210	200	190	180	170	160	150	140	130	120	110

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to 120 l/r and those below lower zig-zag line are for ratios not over 200 l/r.

CARNEGIE BEAM SECTIONS-Continued

12-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

			Nor	ninal D	epth an	d Flang	e Width	ı—Weig	ht per l	Foot		
Effective Length		CB 124	12"x10)"	СВ	123 12	2"x8"	C	B 122	12"x6}	½"	CB 121 12"x6"
in Feet	100 Ibs.	91 1bs.	83 1bs.	75 1bs.	50 1bs.	45 lbs.	40 Mbs.	36 Ibs.	34 lbs.	32 lbs.	28 lbs.	25 lbs.
6 7 8 9	441 441 441 441	401 401 401 401	366 366 366 366	331 331 331 331	220 220 220 220 220	198 198 198 198	176 176 176 176	159 159 157 150	150 150 145 137	141 141 139 133	123 123 121 116	110 109 104 98
10 11 12 13 14	441 441 428 415	401 401 401 391 379	366 366 359 348	331 331 327 318	212 204 197 189	197 191 184 177 170	175 169 163 156 150	136 129 122 115	130 123 116 109 103	127 120 114 108 102	110 105 99 94 89	93 87 82 77 72
15 16 17 18 19 20	390 377 364 352 339	368 356 345 333 322 311	338 328 317 307 297 287	309 300 290 281 272 263	181 174 166 159 152	156 149 143 137	138 132 125 121 115	109 103 97 92 87 82	97 91 86 81 76 71	96 91 86 81 76 72	79 74 70 66 63	63 59 55 52 49
21 22 23 24 25	327 316 304 293 282	300 289 279 269 259	277 267 258 249 240	254 246 237 229 221	139 133 127 122 116	125 119 114 109 104	110 105 100 96 92	77 73 69 65 62	67 63 60 56	68 64 61 57 54	59 56 53 50 47	46 43
26 27 28 29 30	272 262 252 243 234	249 240 232 223 215	231 223 215 207 200	214 206 199 192 185	111 106 102 97 93	99 95 91 87 83	88 84 80 77 73					
31 32 33 34 35	226 217 210 202 195	207 200 193 186 179	193 186 179 173 167	179 173 167 161 155	89 86 82	80 77	70 67					
Area, in.2	29.41	26.76	24.41	22.05	14.69	13.23	11.76	10.59	9.99	9.40	8.22	7.34
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	659.0 4.73 167.5 2.39	627.2 4.84 155.9 2.41	598.9 4.95 147.0 2.45	570.7 5.09 138.5 2.51	400.5 5.22 57.5 1.98	356.9 5.19 51.2 1.97	313.7 5.17 44.9 1.95	280.1 5.14 25.4 1.55	238.1 4.88 21.0 1.45	246.3 5.12 22.3 1.54	213.4 5.10 19.2 1.53	183.0 4.99 13.8 1.37
Weight Lbs. per Foot	100	91	83	75	50	45	40	36	34	32	28	25

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120\,1/r$ and those below lower zig-zag line are for ratios not over $200\,1/r$.

CARNEGIE BEAM SECTIONS—Continued

10-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

			No	minal l	Depth a	and Fla	nge Wi	dth-V	Veight 1	er Foo	t		
Effective Length		CI	3 105	10"x12	77	1	CF	3 104	10"x10	'	CB 1	03 10	"x9"
in Feet	140 lbs.	132 lbs.	124 lbs.	116 lbs.	108 lbs.	100 lbs.	92 1bs.	84 lbs.	77 1bs.	70 lbs.	63 1bs.	56 lbs.	49 lbs.
10 11 12 13 14 15	618 618 618 618 618	582 582 582 582 582 582	547 547 547 547 547	512 512 512 512 512 512	476 476 476 476 476	441 441 441 441 441	406 406 400 389 378	371 371 364 354 344	340 340 336 326 317	309 309 307 299 290	278 275 267 258 248 239	247 239 232 224 216	216 212 205 199 192
16 17 18 19 20	609 596 582 568 554	575 562 549 536 523	540 528 516 504 492	507 496 484 473 461	473 463 452 442 431	439 430 420 410 401	367 356 344 333 322	334 323 313 303 292	308 298 289 280 270	282 273 265 257 248	230 222 213 205 196	208 201 193 186 178	186 179 173 166 160
21 22 23 24 25	540 526 512 499 485	510 497 484 472 458	479 467 455 443 431	450 438 427 416 405	420 410 399 389 378	391 381 372 362 353	311 301 290 280 271	283 273 263 254 245	261 253 244 235 227	240 232 225 217 210	188 181 173 166 159	171 165 158 152 146	154 148 142 137 132
26 27 28 29 30	472 459 446 434 421	446 434 422 410 398	419 407 396 385 374	394 383 372 362 352	368 358 349 339 330	343 334 325 316 307	261 252 243 235 226	237 228 220 212 205	219 212 204 197 190	202 195 189 182 176	153 147 141 135 130	140 134 129 124 119	127 122 117 112 108
31 32 33 34 35	409 398 386 375 364	387 376 365 355 345	364 353 343 333 324	$ \begin{array}{r} 342 \\ 332 \\ 323 \\ 314 \\ 305 \end{array} $	$ \begin{array}{r} 320 \\ \hline 311 \\ 303 \\ 294 \\ 286 \end{array} $	299 291 283 275 267	218 211 203 196 190	198 191 184 178 171	184 177 171 165 160	170 164 158 153 148	125 120 115 110 106	115 110 106 102 98	104 100 96 93 89
36 37 38 39 40	354 344 334 325 315	335 325 316 307 298	315 306 297 289 280	296 288 280 272 264	278 270 262 255 248	260 252 245 239 232	183 177 171 165 160	166 160 154 149 144	154 149 144 139 134	143 138 133 129 125		94	86 83
Area, in.	41.17	38.81	36.46	34.11	31.76	29.40	27.06	24.70	22.65	20.59	18.53	16.47	14.41
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	623.2 3.89 391.4 3.08	603.5 3.94 369.6 3.09	583.9 4.00 349.0 3.09	564.3 4.07 329.4 3.11	544.8 4.14 310.7 3.13	525.1 4.23 292.8 3.16	423.2 3.96 163.1 2.50	403.6 4.04 152.0 2.48	386.5 4.13 142.9 2.51	369.3 4.24 134.3 2.55	300.4 4.03 85.2 2.14	283.2 4.15 79.5 2.20	266.0 4.30 74.2 2.27
Weight Lbs. per Foot		132	124	116	108	100	92	84	77	70	63	56	49

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120\,1/r$ and those below lower zig-zag line are for ratios not over $200\,1/r$.

CARNEGIE BEAM SECTIONS-Continued

10 AND 9-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

			N	ominal	Depth	and Fl	ange W	idth—	Weight	per Fo	ot		
Effective Length	CB 1	02 10)"x8"	(CB 101	10"x	6"	CB	93 9	'x9''	CB 9	2 9"x	6½"
in Feet	42 1bs.	36 lbs.	31 lbs.	30 Ibs.	26 1bs.	23 1bs.	21 lbs.	48 lbs.	43 lbs.	38 lbs.	35 lbs.	32 Ibs.	29 Its.
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	185 185 185 185 175 168 161 153 146 132 125 119 113 107 97 92 88 83 79 75 72	159 159 159 153 147 140 134 128 122 117 111 106 101 96 83 79 75 71 68 65 62 59	137 137 137 134 129 114 109 104 100 95 91 83 87 77 75 72 68 65 62 60 62 60 57 54	132 132 128 121 115 109 103 97 91 86 80 76 71 69 63 59 55 55 53 50	115 110 104 99 93 88 83 78 73 69 65 61 57 54 50 48 45 42	101 101 97 92 87 83 78 73 69 65 61 57 54 45 42 40	93 92 88 83 79 74 70 65 61 57 45 42 39 37 35	212 212 212 212 212 212 208 202 196 189 170 164 158 152 146 141 135 130 125 120 116 111 107	190 190 190 190 190 190 190 186 181 175 169 163 157 152 146 141 135 120 116 1107 103 99 95	168 168 168 168 168 169 159 154 149 144 138 128 124 119 106 102 95 94 90 87 83	154 154 154 148 142 128 122 115 109 103 98 88 83 74 70 67 63 60	141 141 135 129 123 117 111 105 99 94 89 84 80 75 71 67 64 60 57 54	128 128 128 122 117 111 105 100 95 80 76 80 76 68 64 61 57 54 52 49
31 32 33 34 35			52					103 99 95 92 89	92 88 85 82 79	80 77 74 72 69			
Area, in.2	12.35	10.58	9.11	8.82	7.64	6.76	6.17	14.11	12.65	11.17	10.29	9.40	8.53
I1-1. in.4 r1-1, in. I2-2, in.4 r2-2, in.	190.4 3.93 36.8 1.73	175.6 4.07 34.4 1.80	163.4 4.23 32.5 1.89	163.2 4.30 18.5 1.45	139.5 4.27 15.7 1.43	122.2 4.25 13.7 1.43	107.6 4.18 12.0 1.39	221.1 3.96 73.8 2.29	195.5 3.93 65.4 2.28	170.4 3.91 57.1 2.26	155.4 3.89 26.6 1.61	140.5 3.87 24.0 1.60	126.0 3.84 21.5 1.59
Weight Lbs. per Foot	42	36	31	30	26	23	21	48	43	38	35	32	29

Safe load values above upper zig-zag line are for ratios of l/r not over 60, those between zig-zag lines are for ratios up to 120 l/r and those below lower zig-zag line are for ratios not over 200 l/r.

CARNEGIE BEAM SECTIONS—Concluded

8-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

	Nominal Depth and Flange Width—Weight per Foot													
Effective Length					СВ	83 8	"x8"					CB 8	2 8"2	61/2"
in Feet	90 lbs.	84 lbs.	78 lbs.	72 1bs.	66 lbs.	60 lbs.	54 lbs.	48 lbs.	42 1bs.	36 1bs.	31 Ibs.	30 lbs.	27 lbs.	24 1bs.
6 7 8 9 10	397 397 397 397 397	371 371 371 371 371 371	344 344 344 344 344	318 318 318 318 318 318	291 291 291 291 291 291	264 264 264 264 264	238 238 238 238 238 238	212 212 212 212 212 212	185 185 185 185 185	159 159 159 159 159	137 137 137 137 137 137	132 132 132 127 122	119 119 119 114 109	106 106 106 102 97
11 12 13 14 15	395 383 370 357 345	368 356 344 332 320	341 330 319 307 296	314 303 293 282 272	287 277 268 258 249	260 251 242 234 225	233 225 217 209 201	207 200 192 185 178	180 174 168 161 155	154 149 143 138 132	132 127 123 118 113	116 111 105 100 95	104 99 94 89 85	93 88 84 79 75
16 17 18 19 20	332 320 307 295 284	308 296 285 274 263	285 274 264 253 243	262 252 242 232 223	239 230 221 212 203	216 208 199 191 183	193 186 178 171 164	171 164 158 151 145	149 143 137 131 126	127 122 116 112 107	109 104 100 96 91	90 85 80 76 72	80 76 72 68 64	71 67 64 60 57
21 22 23 24 25	$\begin{array}{r} 272 \\ \hline 261 \\ 251 \\ 241 \\ 231 \\ \end{array}$	$\begin{array}{r} 252 \\ \hline 242 \\ 232 \\ 223 \\ 214 \\ \end{array}$	$\begin{array}{r} 233 \\ \hline 224 \\ 215 \\ 206 \\ 197 \\ \end{array}$	$\begin{array}{c} 213 \\ 205 \\ 196 \\ 188 \\ 180 \\ \end{array}$	195 187 179 172 164	176 168 161 154 148	157 150 144 138 132	139 133 127 122 117	120 115 110 105 101	102 98 93 89 86	87 84 80 77 73	68 65 61 58 55	61 58 55 52 49	54 51 48 46 43
26 27 28 29 30	222 213 204 196 188	205 197 189 181 174	189 182 174 167 160	173 166 159 153 146	158 151 145 139 133	142 136 130 125 120	126 121 116 111 107	$112 \\ 107 \\ 102 \\ 98 \\ 94$	97 93 89 85 81	82 78 75 72 69	70 67 64 61 59	52 50	47 44	41
31 32 33 34 35	181 174 167 161 155	167 160 154 148 143	154 148 142 137 131	141 135 130 125 120	128 123 118 113 109	115 110 106 102	102 98 94 90	90 87 83 80	78 75 72 69	66 63 61	56 54 52			
Area, in.2	26.47	24.71	22.93	21.17	19.40	17.63	15.87	14.10	12.34	10.58	9.10	8.81	7.93	7.06
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	391.2 3.84 124.4 2.17	3.81	3.77	295.9 3.74 95.3 2.12	265.9 3.70 86.1 2.11	237.1 3.67 77.1 2.09	209.2 3.63 68.3 2.07	182.2 3.59 59.7 2.06	156.2 3.56 51.4 2.04	131.3 3.52 43.4 2.02	110.9 3.49 36.7 2.01	107.8 3.50 23.4 1.63	95.9 3.48 20.8 1.62	84.3 3.46 18.3 1.61
Weight Lbs. per Foot	90	84	78	.72	66	60	54	48	42	36	31	30	27	24

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120\ 1/r$ and those below lower zig-zag line are for ratios not over $200\ 1/r$.

STANDARD MILL SECTIONS

MISCELLANEOUS SMALL COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—American Institute of Steel Construction—1923

	Nominal Depth and Flange Width—Weight per Foot												
Effective Length		40 5½″		B 39 8"x5"		4 8"2	8"	H 6":	3 A x6"	H 3 6"x6"		H 2 5"x5"	H 1 4"x4"
in Feet	25 lbs.	21 lbs.	21 lbs.	18 lbs.	37.7 lbs.	34.3 1bs.	32.6 lbs.	27.5 1bs.	25 lbs.	22.5 lbs.	20 lbs.	18.9 Ibs.	13.8 lbs.
3 4 5	110 110 110	93 93 93	93 93 93	79 79 79	165 165 165	150 150 150	143 143 143	121 121 121	110 110 110	99 99 99	88 88 88	82 82 82	60 60 59
6 7 8 9	106 99 92 85 79	91 85 80 74 69	87 81 75 69 63	76 71 66 61 56	165 165 165 165 160	150 150 150 150 146	143 143 143 143 140	121 121 116 110 104	110 110 106 100 95	99 93 88 88 83	88 83 79 75	82 77 73 68 63	54 50 46 42 38
11 12 13 14 15	73 67 - 62 57 53	59 54 50 45	58 53 49 45 41	52 47 44 40 37	154 147 141 135 129	141 135 130 124 119	135 130 124 119 114	98 92 87 81 76	90 84 79 75	78 73 69 64 60	70 66 62 58 55	59 55 51 47 44	35 32 29 26 24
16 17 18 19 20	49 45 42	43 40 37 34	38 35	34 32	123 117 112 106 101	114 108 103 99 94	109 104 100 95	72 67 63 59 56	66 62 58 55 51	56 53 50 46 44	51 48 45 42 40	41 38 35 33 31	
21 22 23 24 25					96 92 87 83 79	90 85 81 78 74	86 83 79 75 72	52 49 46	48 46 43	41 38	37 35 33		
26 27 28 29 30					76 72 69 66 63	71 67 64 62 59	68 65 62 60 57						
Area, in.2	7.34	6.17	6.17	5.29	11.00	10.00	9.50	8.08	7.33	6.61	5.86	5.47	3.99
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	95.5 3.61 8.8 1.09	87.6 3.77 8.1 1.14	63.4 3.21 6.6 1.03	58.7 3.33 6.1 1.07	120.8 3.31 36.9 1.83	115.5 3.40 35.1 1.87	112.8 3.45 34.2 1 90	49.3 2.47 16.0 1.41	47.0 2.53 14.9 1.43	41.0 2.49 12.2 1.36	38.8 2.57 11.4 1.39	23.8 2.08 7.8 1.20	10.7 1.64 3.6 0.95
Weight Lbs. per Foot	25	21	21	18	37.7	34.3	32.6	27.5	25	22.5	20	18.9	13.8

Safe load values above upper zig-zag line are for ratios of 1/r not over 60, those between zig-zag lines are for ratios up to $120\,1/r$ and those below lower zig-zag line are for ratios not over $200\,1/r$.

BEAM AND COLUMN SAFE LOADS

in accordance with Building Codes of

THE CITY OF NEW YORK as amended to January 1, 1926

and

THE CITY OF CHICAGO as amended to July 1, 1924

SAFE LOADS FOR SECTIONS USED AS BEAMS

EXPLANATION OF TABLES

Tables of safe loads for Carnegie Beam Sections used as beams under conditions of static transverse loading, give the uniformly distributed safe loads in thousands of pounds for spans customary in bridge and building construction, based upon an extreme fiber stress of 16,000 pounds per square inch. These tables give the full loads for beams fixed or braced against lateral deflection as well as the reduced loads allowed for beams free or unbraced against side deflection, and also the values for those spans at which the allowed safe load will produce a deflection of ½50 of the span length. The loads in all cases include the weight of the section, which should be deducted in order to arrive at the net load which the section will support.

It is assumed in all cases that the loads are applied normal to the axis 1-1 as shown in the tables of elements of sections, and that the beam deflects vertically in the plane of bending only. If the conditions of loading involve the introduction of forces outside this plane of loading, the allowable safe loads must be determined from the general theory of flexure, in accordance with the mode of application of the load and its character. In cases of eccentric loading, the actual safe loads would be considerably lower than the tabulated safe loads which have been based upon the most favorable conditions of loading.

Vertical Deflection. The vertical deflection of a section under a uniformly distributed load is determined from formula:

Deflection, D=
$$\frac{5}{384} \frac{\text{Wl}^3}{\text{EI}}$$
; Wl=8 f $\frac{\text{I}}{\text{n}}$
" D= $\frac{40}{384} \frac{\text{fl}^2}{\text{En}}$; Span length in feet: l=12L

" D= $\frac{15 \text{ fL}^2}{\text{En}}$ inches

Steel, E=29,000,000; for fiber stress f=16,000 pounds:

Deflection, D=
$$\frac{0.01655L^2}{2n}$$

n=distance from center line of gravity to extreme fiber:

$$Deflection = \frac{Coefficient}{2n}$$

Deflection Coefficients for Fiber Stress of 16,000 Pounds

Span, Feet	Coefficient 16,000	Span, Feet	Coefficient 16,000	Span, Feet	Coefficient 16,000	Span, Feet	Coefficient 16,000
1	0.017	16	4.237	31	15.906	46	35.023
2	0.066	17	4.783	32	16.949	47	36.563
3	0.149	18	5.363	33	18.025	48	38.135
4	0.265	19	5.975	34	19,134	49	39.741
5	0.414	20	6.621	35	20.276	50	41.379
6	0 596	21	7.299	36	21.451	51	43.051
7	0.811	22	8.011	37	22.659	52	44.756
8	1.059	23	8.756	38	23.901	53	46.494
9	1.341	24	9,534	39	25.175	54	48.265
10	1.655	25	10.345	40	26.483	55	50.069
11	2.003	26	11.189	41	27.823	56	51.906
12	2.383	27	12.066	42	29.197	57	53,777
13	2.797	28	12.977	43	30.604	58	55.680
14	3.244	29	13.920	44	32.044	59	57.617
15	3.724	30	14.897	45	33.517	60	59.586

The deflection, in inches, of sections subjected to transverse stresses due to uniformly distributed loads are obtained as follows:

symmetrical Sections. To find the deflection in inches of a section symmetrical about the neutral axis, such as I- and H-beams, divide the coefficient in the table corresponding to given span and fiber stress by the depth of the section in inches.

Unsymmetrical Sections. To find the deflection in inches of a section not symmetrical about the neutral axis, such as beams with unbalanced flange plates or with continuous shelf angles, divide the coefficient corresponding to given span and fiber stress by twice the distance of extreme fiber from neutral axis obtained by computation.

Other Fiber Stresses. To find the deflection of any section for other fiber stresses than those given, multiply the coefficient for 16,000 pounds fiber stress corresponding to the span given by the ratio of desired fiber stress and 16,000.

Limits of Deflection. The deflection of floor beams carrying plastered ceilings should be limited to not more than ½60 of the span length; this limit is indicated in the safe load tables by lower zigzag line, is derived from the following formulas:

Deflection, D_{max}. = $\frac{12L}{360} = \frac{15fL^2}{En}$ Limiting Span, L_{max}. = $\frac{En}{450f}$ for fiber stress of 16,000, Limiting Span, L_{max}. = 4.027n

Lateral Deflection of Beams. In computing safe loads it is generally assumed that the compression flanges of the sections are secured against lateral deflection by the use of tie rods or by other means.

When lateral bracing is not provided and the unbraced span length is excessive, the full safe loads must be reduced in accordance with the ratios given in the following table in order to insure that the stresses in the compression flanges do not exceed the safe unit stress. The lateral unbraced length of beams and girders should not exceed forty times the width of the compression flanges.

The following table gives values obtained from formulas for:

New York Building Code fe=21,000-250 l/b, interpretation of fc=16,000-70 l/r, r= $b/\sqrt{12}$ (approximate value: r=0.28b). Full stress of 16,000 pounds is used up to values of 1/b=20.

CHICAGO BUILDING CODE f_C=20,000-160 l/b.
Full stress of 16,000 pounds is used up to values of l/b=25.

Reduction of Safe Loads for Ratio of Span Length to Flange Width, 1/b.

	Full Lead, Per Cent.				Load, Cent.			Load, Cent.	-	Full Load, Per Cent.	
Ratio, 1/b	New York	Chicago	Ratio, 1/b	New York	Chicago	Ratio, 1/b	New York	Chicago	Ratio, 1/b	New York	Chicago
20 20.5 21 21.5 22 22.5 23 23.5 24 24.5	100 99.2 98.4 97.7 96.9 96.1 95.3 94.5 93.8	100 100 100 100 100 100 100 100 100	25 25.5 26 26.5 27 27.5 28 28.5 29 29.5	92.2 91.4 90.6 89.8 89.1 88.3 87.5 86.7 85.9 85.2	100 99.5 99.0 98.5 98.0 97.5 97.0 96.5 96.0 95.5	30 30.5 31 31.5 32 32.5 33 33.5 34 34.5	84.4 83.6 82.8 82.0 81.3 80.5 79.7 78.9 78.1 77.3	95.0 94.5 94.0 93.5 93.0 92.5 92.0 91.5 91.0 90.5	35 35.5 36 36.5 37 37.5 38 38.5 39 39.5 40	76.6 75.8 75.0 74.2 73.4 72.7 71.9 71.1 70.3 69.5 68.8	90.0 89.5 89.0 88.5 88.0 87.5 87.0 86.5 86.0 85.5 85.0

In addition to this lateral deflection which is induced within the beam by the action of vertical loading, lateral deflection may be induced by the thrust of floor arches or other loading acting on an axis perpendicular to the line of principal bending stress.

Stresses due to horizontal thrust should either be neutralized by tie rods, or the safe carrying capacity of the beam should be computed in accordance with the general formulas of flexure to provide for the combined stresses due to the action of both vertical and horizontal forces; that is to say, the safe loads should be figured around both the axes 1-1 and 2-2, and the unit stress computed so as not to exceed the allowable fiber stress.

Effect of Impact on Stresses. The formulas upon which the tables of safe loads are based assume all loads to be quiescent or static. The effect of moving loads may be taken care of either by reducing the allowable unit stresses, or else by increasing the theoretical loads.

When a load is suddenly applied, the resultant stresses are twice as great as those due to an equal quiescent load.

When an instantaneously applied load produces impact or percussion, the resultant stresses are dynamic and are measured by the laws governing the energy of bodies in motion. The following formulas give the fiber stress and deflection due to a load falling on center of a beam rigidly supported at both ends when the weight of beam is negligible as compared with that of falling load, and when no account is taken of the local distortion due to impact or percussion at point of application of load; but when the weight of the beam is a real factor, theoretical formulas do not agree with observed results and practical tests give values which are far less than those indicated by theoretical formulas; this is notably true in drop-tests of axles:

W = Weight of falling load, in pounds.

h =Height of fall, in inches.

f =Extreme fiber stress due to static effect of load, W,

in pounds per square inch.

fd =Extreme fiber stress due to impact of load, W, in pounds per square inch.

D =Deflection due to static effect of load, W, in inches. Dd=Deflection due to impact of load, W, in inches.

$$f_{d} = f(1 + \sqrt{\frac{2h}{D} + 1})$$
 $D_{d} = D(1 + \sqrt{\frac{2h}{D} + 1})$

Shearing Stresses. The safe load tables for beams are computed solely with reference to safe unit stresses due to flexure, and the safe loads uniformly distributed on the spans given will not produce excessive shearing stresses in the web.

When, however, beams must support heavy loads which are concentrated near the supports, or when beams of short span are loaded with uniformly distributed loads to their full carrying capacity as regards flexure, the bending moments may be small in comparison with the reactions at the supports, and the beams may fail along the neutral plane as a result of longitudinal shearing stresses, or may buckle as a result of the combined longitudinal and vertical web stresses. On such spans the safe shearing or buckling strength of the web may limit the carrying capacity of the beam, so that the deciding factor will often be the resistance of the web to shearing stresses, rather than the resistance of the flanges to bending stresses.

Longitudinal Shear. At any point in any section of a beam, the horizontal and vertical components of the web stress are equal to each other and proportional to the vertical shear; their intensities are dependent upon the distance of the point from the neutral axis. In order to determine the intensity of the vertical shearing stress at a given point in a vertical section of the beam, therefore, it is sufficient to find the equal intensity of the horizontal shearing stress at the same point in the horizontal plane.

The longitudinal unit shear is zero at the upper and lower flanges of the beam and a maximum at the neutral plane. It is greatest at the supports and zero where there is no vertical shear.

The intensity of the longitudinal shear at any point in any section is the product of the vertical shear, V, for that section and the static moment, Ms, of the section included between the horizontal plane of shear through that point and the extreme fibers on the same side of the neutral plane divided by the product of the moment of inertia of the beam around the proper axis and the thickness at the plane of shear; or

Longitudinal shear per square inch= $\frac{V Ms}{t I}$.



Example—Required the maximum longitudinal unit shear in Carnegie Beam Section CB-302, 30" x 14", 180 lb, for a maximum vertical shear of 201,000 pounds.

 M_8 of Flange = 14 x 1.2065 x 14.397 = 243.2 M_8 of Web = 13.794 x 0.67 x 6.897 = 63.7 Total Static Moment 306.9 in.8

Moment of Inertia of Beam, I=8301.4 in.4

Longitudinal Shear= $\frac{201,000 \times 306.9}{8301.4 \times 0.67}$ = 11,090 pounds per square inch,

Under usual conditions of loading, the longitudinal shear need not be taken into consideration.

Buckling Values of Beam Webs. The vertical shearing stresses or the vertical compressive components of the web stress may, under some conditions, exceed the safe resistance of the beam to buckling, and there remains the possibility that a web which is amply secure as against the safe allowed shear will not be of sufficient strength when considered as a column. In such cases provision must be made for security against buckling either by web stiffeners or by increasing the thickness of the web.

Experiments with beams of various depths and web thicknesses have demonstrated that the length of the web which can be assumed to resist buckling stresses is equal to the end bearing plus one fourth of the depth of the beam; the following formulas have been deduced:

Safe end reaction
$$R = f_b x t (a + \frac{d}{4})$$

Safe interior load $W = 2f_b x t (a^1 + \frac{d}{4})$

[a] In the formulas R is the end reaction, W the concentrated load, t the web thickness, d the depth of the beam, a¹ half the distance over which the concentrated load is applied, a the whole distance over which the end reaction is applied, and fb is the safe unit resistance of the web to buckling.

The first formula is general and applies to any condition of loading. The second formula is for a single load concentrated at the center of a span; it can be extended for a system of concentrated loads, provided the sum of the distances a¹ is not less than a.

For computation of f_b the following formula has been used in the tables, corresponding to an allowable shearing stress of 10,000 pounds, f_b maximum = 15,000 pounds.

$$f_c=19,000-100 \, l/r$$
, $l=\frac{1}{2}d$ and $r=t/\sqrt{12}$, $f_b=19,000-173d/t$

This formula is not part of the building codes of New York or of Chicago, and the values based upon same are given in the tables which follow for general information only.

The tables give for beams with unsupported webs:

- 1. Allowed web resistance fb, in pounds per square inch, computed from this compression formula.
- 2. The distance a, or the distance over which the end reaction must be distributed when the shearing stress, V, in the web is the maximum allowable of 10,000 pounds per square inch.
- 3. The allowable end reaction (R) when a is taken at $3\frac{1}{2}$ ", which is the usual length of beam actually resting on the 4" angles ordinarily used in building construction for beam seats.
- 4. The allowable shear V, on the gross area of beam webs at 10,000 pounds per square inch.

Maximum Bending Moments. In addition to data referring to maximum loads on beams as computed from the web resistance, these tables also give the maximum bending moments in foot pounds, which may be used instead of the table of properties, to ascertain the proper size section to be used in any particular instance.

CARNEGIE BEAM SECTIONS

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 16,000 Pounds—Shearing Stress 10,000 Pounds

-	1				***		1.72	**	
	Donth	Weight	Web Thick- ness	Maximum	Valu		End		
Section	Depth of	Weight per Foot		Bending	Web Sh	earing	Web B	Reaction	
Index	Beam			Moment	End Span Reaction Limit		Unit Stress	End Bearing	a=3½"
and Nominal				M			fb	a min.	R max.
Depth	d		t	M max.	V max.	L min.		a mm.	n max.
	Inches	Pounds	Inches	Foot Pounds	Pounds	Feet	Pounds perSq.In.	Inches	Pounds
	00 701	040	000	000.050	072 240	14,40	13.003	15.98	129,270
CB 302	$30.781 \\ 30.522$	$ \begin{array}{c c} 240 \\ 220 \end{array} $.888	983,850 901,750	249.060	14.48	12,529	16.73	113,800
30′′	30.263	200 180	.743	820,000 737,850		14.59 14.68	11,954 $11,254$	17.75 19.16	98,280 82,940
	30.000								
CB 301	30.298 30.148	$\frac{135}{125}$.621	519,850 481,350	188,150 173,650	$\frac{11.05}{11.09}$	10,559	$21.12 \\ 22.78$	72,620 63,220
30′′	30.000	115	.530		159,000	11.15	9,208	25.08	53,680
	27.598	190	.756	712,800	208,640	13.67	12,685	14.86	99,730
CB 272	$27.400 \\ 27.200$	175 160	.698	656,650	191,250 173,810	13.73 13.81	12,209 11,636	15.59 16.58	88.200 76,590
27''	27.000	145	.580		156,600	13.90	10,947	17.92	65,080
~~ ~~	27,340	112	.566	390.950	154,740	10.11	10.643	18.85	62,260
CB 271 27"	$\frac{27.166}{27.000}$	101	.510	352,950	138,550	$10.19 \\ 10.21$	9,785	$20.97 \\ 23.70$	51,360 41,900
	27.000	91	,401	317,790	124,470	10.21	8,868	25.10	41,900
CB 244	$24.664 \\ 24.526$	160 150	.670 .629		165,250 154,270	13.26 13.31	12,632 $12,254$	13.36	81,810
24"	24.388	140	.588	478,950	143,400	13.36	11,825	14.53	74,240 66,730
	24.250	130	.547	444,800	132,650	13.41	11,330	15.34	59,270
CB 243	$24.310 \\ 24.156$	120 110	.539		131,030 119,330	12.29	11,197	15.63	57,800 49,670
24''	24.000	100	.450		108,000	12.37 12.43	10,541 9,773	16.88 18.56	41,780
	24.308	94	.499	300,000	121,300	9.89	10,573	16.91	50,530
CB 242 24"	24.154	85	.452	271,350	109,180	9.94	9,755	18.72	42,060
CB 241	24.000	76	.405	242,650	97,200	9.99	8,748	21.43	33,660
24"	24.000	70	.400	217,050	96,000	9.04	8,620	21.84	32,760
	21.248	120	.535	362.800	113.680	12.77	12.129	12.21	57,180
CB 213 21"	21.126	112	.499	338,800	105,420	12.86	11,676	12.81	51,160
	21.000	104	.465	314,250	97,650	12.87	11,187	13.52	45,520
CB 212	$21.240 \\ 21.120$	92 86	.502 .470	262,000 244.800	106,630 99,260	9.83	11,680 11,226	12.87 13.53	51,660 46,330
21"	21.120	80	.438	244.800 227,350	99,260	9.86 9.91	10,705	13.53	41,030
	21.248	70	.433	193,600	92,000	8.42	10,511	14.90	40.100
CB 211	21,126	64	.396	177,200	83,660	8.47	9,771	16.34	33,980
21"	21.000	58	.360	160,400	75,600	8.49	8,908	18.32	28,060
]21.034	60	.375	165,450	78,880	8.39	9,296	17.37	30,530

CARNEGIE BEAM SECTIONS—Continued

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 16,000 Pounds—Shearing Stress 10,000 Pounds

	1					Valu	es for En	d Reaction	n, V	
	a .:	Depth	Weight	Web Thick-	Maximum Bending	Web Si	nearing	Web B	uckling	End Reaction
	Section Index and	Beam	per Foot	ness	Moment	End Reaction	Span Limit	Unit Stress	End Bearing	a=3½"
	Nominal	d		t	M max.	V max.	L min.	fb	amin.	R max.
		Inches	Pounds	Inches	Foot Pounds	Peunds	Feet	Pounds perSq.In.	Inches	Pounds
	CB 183 18"	18.238 18.120 18.000	100 93 86	.498 .463 .429	260,800 242,550 224,250	90,830 83,900 77,220	11.49 11.56 11.62	12,664 12,229 11,741	9.84 10.29 10.83	50,830 45,470 40,300
	CB 182 18"	18.242 18.110 18.000	78 72 67	.471 .436 .406	192,800 177,850 165,450	85,920 78,960 73,080	8.98 9.01 9.06	12,300 11,814 11,330	10.27 10.80 11.39	46,700 41,350 36,800
	CB 181 18"	18.252 18.114 18.000	58 52 47	.393 .354 .320	140,400 125,850 113,850	71,730 64,120 57,600	7.83 7.85 7.91	10,965 10,148 9,269	12.08 13.32 14.92	34,750 28,840 23,730
		18.024	51	.375	119,850	67,590	7.09	10,685	12.36	32,080
	CB 165 16"	16.236 16.110 16.000	115 107 100	.532 .496 .464	273,600 254,400 237,750	86,380 79,910 74,240	12.67 12.74 12.81	13,720 13,381 13,034	7.77 8.01 8.28	55,170 49,960 45,360
	CB 164 16"	16.240 16.120 16.000	90 83 76	.495 .458 .419	209,450 193,200 176,950	80,390 73,830 67,040	10.42 10.47 10.56	13,324 12,911 12,394	8.13 8.46 8.91	49,860 44,530 38,950
	CB 163 16"	16.226 16.114 16.000	68 63 58	.438 .406 .375	151,850 140,650 129,450	71,070 65,420 60,000	8.55 8.60 8.63	12,591 12,134 11,619	8.83 9.25 9.77	41,670 37,090 32,680
	CB 162 16"	16.254 16.128 16.000 15.934	50 45 40 43	.362 .326 .290 .375	109,200 98,400 87,450 87,600	58,840 52,580 46,400 59,750	7.42 7.49 7.54 5.86	11,232 10,441 9,455 11,649	10.41 11.41 12.92 9.69	30,750 25,640 20,570 32,690
	CB 161 16"	16.012 15.930	38 35	.314 .290	79,050 72,950	50,280 46,200	6.29 6.32	10,178 9,497	11.73 12.79	23,980 20,610
1	CB 145 14"	14.370 14.186 14.000	105 95 85	.536 .485 .435	217,050 196,250 175,450	77,020 68,800 60,900	11.27 11.41 11.53	14,362 13,940 13,432	6.41 6.63 6.92	54,600 47,640 40,900
	CB 144 14"	14,382 14,238 14,094	75 68 61	.468 .425 .382	152,650 138,400 124,150	67,310 60,510 53,840	9.07 9.15 9.22	13,684 13,204 12,617	6.91 7.22 7.65	45,440 39,620 33,850
	CB 143	14.242 14.122 14.000	58 53 48	.413 .378 .343	114,150 104,250 94,550	58,820 53,380 48,020	7.76 7.81 7.87	13,034 12,537 11,939	7.37 7.73 8.23	38,010 33,320 28,670

CARNEGIE BEAM SECTIONS—Continued

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 16,000 Pounds—Shearing Stress 10,000 Pounds

-	1		1	1	Volu	og for Enc	l Reaction	V	
	Depth	Weight	Web	Maximum				uckling	End
Section Index and	of Beam	Foot	Thick- ness	Bending Moment	End Reaction	Span Limit	Unit Stress	End Bearing	Reaction a=3½"
Nominal Depth	d		t	M max.	V max.	L min.	fb	a min.	R max.
-	Inches	Pounds	Inches	Foot Pounds	Pounds	Feet	Pounds perSq.In.	Inches	Pounds
CB 142	14.240 14.160 14.080 14.000	42 39 36 33	.342 .318 .294 .270	80,800 75,050 69,200 63,450	48,700 45,030 41,400 37,800	6.64 6.67 6.69 6.72	11,797 11,297 10,715 10,030	8.51 8.99 9.62 10.46	28,480 25,290 22,110 18,960
	14.000	38	.375	68,150	52,500	5.19	12,541	7.66	32,920
CB 141 14"	13.964	30	.270	55,750	37,700	5.91	10,053	10.40	18,980
CB 124	12.000 12.000 12.000 12.000	100 91 83 75	1.121 .900 .704 .508	146,400 139,350 133,050 126,800	134,520 108,000 84,480 60,960	4.35 5.16 6.30 8.32	15,000 15,000 15,000 14,913	5.00 5.00 5.00 5.05	109,300 87,750 68,640 49,240
CB 123 12"	12.258 12.130 12.000	· 50 45 40	.361 .326 .290	87,200 78,400 69,750	44,250 39,540 34,800	7.88 7.93 8.02	13,126 12,563 11,841	6.27 6.62 7.13	31,110 26,750 22,320
CB 122	12.236 12.118 12.000	36 32 28	.308 .274 .240	61,050 54,250 47,450	37,690 33,200 28,800	6.48 6.54 6.59	12,127 11,349 10,350	7.03 7.65 8.59	24,500 20,300 16,150
	12.022	34	.375	52,800	45,080	4.69	13,454	5.93	32,820
CB 121 12"	11.924	25	.240	40,950	28,620	5.72	10,405	8.48	16,180
CB 103 10"	10.000 10.000 10.000	63 56 49	.787 .581 .375	80,150 75,450 70,950	78,700 58,100 37,500	4.07 5.20 7.57	15,000 15,000 14,387	4.17 4.17 4.45	70,830 52,290 32,370
CB 102 10"	10.000 10.000 10.000	42 36 31	.644 .467 .320	50,800 46,800 43,600	64,400 46,700 32,000	$3.16 \\ 4.01 \\ 5.45$	15,000 15,000 13,594	4.17 4.17 4.86	57,960 42,030 26,100
CB 101 10"	10.228 10.098 10.000	30 26 23	.298 .259 .230	42,550 36,800 32,550	30,480 26,150 23,000	5.58 5.63 5.66	13,062 12,255 11,478	5.27 5.72 6.21	23,580 19,120 15,840
	9.902	21	.230	28,950	22,780	5.08	11,552	6.10	15,880

CARNEGIE BEAM SECTIONS—Concluded

MAXIMUM BENDING MOMENTS AND WEB RESISTANCES

Bending Stress 16,000 Pounds—Shearing Stress 10,000 Pounds

						es for End	l Reaction	ı, V	
Section	Depth	Weight	Web Thick-	Maximum Bending	Web Sh	earing	Web B	uckling	End Reaction
Index and	Beam	Foot	ness	Moment	End Reaction	Span Limit	Unit Stress	End Bearing	a=3½"
Nominal Depth	d		t	M max.	V max.	L min.	fb	a min.	R max.
	Inches	Pounds	Inches	Foot Pounds	Pounds	Feet	Pounds perSq.In.	Inches	Pounds
CB 93	9.242 9.122 9.000	48 43 38	.398 .357 .316	63,750 57,200 50,550	36,780 32,570 28,440	6.93 7.03 7.11	14,983 14,580 14,073	3.86 3.98 4.15	34,650 30,090 25,570
CB 92	9.192 9.096 9.000	35 32 29	.335 .307 .279	45,050 41,200 37,350	30,790 27,930 25,110	5.85 5.90 5.95	14,253 13,874 13,419	4.15 4.28 4.46	27,680 24,590 21,530
CB 83	8.360 8.198 8.060	42 36 31	.390 .336 .290	49,850 42,650 36,650	32,600 27,550 23,370	6.12 6.20 6.27	15,000 14,779 14,192	3.48 3.50 3.66	32,700 27,560 22,700
CB 82	8.196 8.098 8.000	30 27 24	.298 .268 .239	35,050 31,600 28,150	24,420 21,700 19,120	5.74 5.82 5.89	14,242 13,773 13,209	3.71 3.86 4.06	23,550 20,390 17,£60

STANDARD MILL SECTIONS

_										
В	40 9"	9.000	25 21	.380 .250	28,250 26,000	34,200 22,500	$\frac{3.31}{4.62}$	14,903 12,772	3.79 4.80	32,560 18,360
В	39 8''	8.000 8.000	21 18	.360 .250	21,200 19,600	28,800 20,000	$\frac{2.94}{3.92}$	15,000 13,464	3.33 3.94	29,700 18,510
н	4 8"	8.000 8.000 8.000	37.7 34.3 32.6	.500 .375 .313	40,250 38,550 37,600	40,000 30,000 25,040	4.03 5.14 6.01	15,000 15,000 14,578	3.33 3.33 3.49	41,250 30,940 25,100
Н	3-A 6"	6.000 6.000	27.5 25.0	.438	21,850 20,950	26,280 18,780	3.33 4.46	15,000 15,000	$\frac{2.50}{2.50}$	32,850 23,480
н	3 6"	6.000 6.000	22.5 20.0	.375 .250	18,250 17,200	22,500 15,000	3.25 4.59	15,000 14,848	2.50 2.54	28,130 18,560
Н	5"	5.000	18.9	.313	12,650	15,650	3,24	15,000	2.08	22,300
Н	1 4"	4.000	13.8	.313	7,050	12,520	2.26	15,000	1.67	21,130

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

	II.			Momi	nol De	nth o	nd Fla	ange V	Vid+b_	Woi	wht no	· Foo			
~				302	30"		nu ri	inge v	TOTAL	CB		30"x1			nt nt
Span	940	lbs.		lhs.	1	lbs.	180	Iba	125	lbs.		lbs.	1	1ha	Coefficient of Deflection
Feet	2780	103.	1 440		rally	103.	100	11)3.	100	108.		rally	113	lbs.	effe
	Fixed	Free	Fired	Free		Free	Fired	Free	Pirad	Free		_	T0:	P	QA
-	FILOU	1100	rizeu	1166	riieu	1100	FIXEG	1166	376	376	347	Free 347	318	Free 318	
12								3	347	347	321	321	295	295	2.383
13				400	450	4.50			$\frac{320}{297}$	$\frac{320}{297}$	$\frac{296}{275}$	296 275	273	273	2.797
14 15	$\frac{547}{525}$	$\frac{547}{525}$	498	498	$\frac{450}{437}$	$\frac{450}{437}$	$\frac{402}{394}$	$\frac{402}{394}$	277	277	257	257	$\frac{253}{236}$	253 236	3.244
16	492	492	451	451	410	410	369	369	260	260	241	241	222	222	4.237
17	463	463	424	424	386	386	347	347	245	245	227	227	209	209	4.783
18 19	437	437	$\frac{401}{380}$	$\frac{401}{380}$	364 345	364 345	328	328 311	$\frac{231}{219}$	$\frac{229}{214}$	214 203	212 198	$\frac{197}{187}$	195 181	5.363 5.975
20	394	394	361	361	328	328	295	295	208	199	193	184	177	170	6.621
$\frac{21}{22}$	375	375	343	343	312 298	312 298	$\frac{281}{268}$	281	198	186	183	172	169	158	7.299
23	$\frac{358}{342}$	358 342	328 314	$\frac{328}{314}$	285	$\frac{298}{285}$	257	$\frac{268}{257}$	189 181	$\frac{174}{164}$	175 167	161 151	161 154	148 139	8.011 8.756
24	328	327	301	299	273	271	246	244	181 173	154	160	142	148	130	9.534
25 26	315	310 293	289 277	$\frac{283}{269}$	262 252	$\frac{257}{243}$	236 227	231 219	166 160	145 136	154 148	134 126	142 136	123	10.345
27	291	279	267	255	243	232	219	208	154	129	143	119	131	116 109	11.189 12.066
28	281	265	258	243	234	220	211	198	149	121	138	112	127	103	12.977
29 30	$\frac{271}{262}$	$\frac{252}{241}$	$\frac{249}{240}$	$\frac{231}{220}$	226 219	$\frac{209}{200}$	$\frac{204}{197}$	188 179	143 139	115 108	133 128	106 100	122 118	97 92	$13.920 \\ 14.897$
31	254	229	233	210	212	190	190	171	134	103	124	95	114	87	15.906
32	246	219	225	200	205	182	184	163	130	97	120	89	111	82	16.949
33 34	$\frac{238}{231}$	$\frac{210}{200}$	$\frac{219}{212}$	191 183	199 193	173 166	179 174	$\frac{156}{149}$	$\frac{126}{122}$	92 87	$\frac{117}{113}$	85	107 104	78 74	18.025 19.134
35	225	191	206	175	187	159	169	142	119	82	110	76	101	70	20.276
36 37	219 213	183 175	$\frac{200}{195}$	$\frac{167}{160}$	182 177	$\frac{152}{145}$	164 160	136 130	$\frac{116}{112}$		$\frac{107}{104}$		98 96		21.451
38	207	168	190	153	173	139	155	125	109		101		93		22.659 23.901
39	202	161	185	147	168	133	151	119	107		99		91		25.175
40 41	$\frac{197}{192}$	154 148	$\frac{180}{176}$	141 135	164 160	128 122	148 144	115	104 101		96 94		89 86		26.483 27.823
42	187	142	172	129	156	118	141	105	99		92		84		29.197
43	183	137	168	125	153	113	137	101	97		90		82		30.604
44 45	$179 \\ 175$	$\frac{131}{126}$	164 160	$\frac{120}{115}$	149 146	108 104	134 131	97	95		88 86		81 79		32.044 33.517
46	171	121	157	110	143	100	128	89	90		84		77		35.023
47	167 164	116	153 150	106	$\frac{140}{137}$		126		89		82		75 74		36.563
48 49	161		147		134		$\frac{123}{120}$		85		80 79		72		38.135 39.741
50	157		144		131		118		83		77		71		41.279
$\begin{array}{c} 51 \\ 52 \end{array}$	154 151		141 139		129 126		116		82 80		76 74		70 68		43.051 44.756
53	149		136		124		1111		78		73		67		46.494
54	146		134		121		109		77		71		66		48.265
55 - 56	143		131 129		119 117		107 105		76 74		70 69	1	64 63		50.069
57	138		127		115		104		73		68		62		53.777
58	136		124		113		102		72		66		61		55.680
59 60	133 131		$\frac{122}{120}$		111 109		100		70 69		65 64		60 59		57.617 59.586
61	129		118		108		97		68	1	63		58		61.589
62	127		116	1	106		95		67		62		57		63.625

CARNEGIE BEAM SECTIONS—Continued ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch City of New York Code

-	1		No	minal	Dept	h and	Flang	e Wid	lth—V	Veigh	t per l	Foot		1	
Span			CB	272	27''x	14"				СВ	271	27"x9	34"		ent
in Feet	_190	lbs.	175	lbs.	160	lbs.	145	lbs.	_112	lbs.		lbs.	91	lbs.	Coefficient of Deflection
				Late							Late	rally			S a
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free		Free		Free	Fixed		
11									$\frac{309}{284}$	309 284	$\frac{277}{257}$	$\frac{277}{257}$	$\frac{249}{231}$	$\frac{249}{231}$	2.003
12									261	261	235	235	212	212	2.383
13 14	$\frac{417}{407}$	$\frac{417}{407}$	$\frac{383}{375}$	$\frac{383}{375}$	348	348	$\frac{313}{311}$	$\frac{313}{311}$	$\frac{241}{223}$	241 223	217 202	$\frac{217}{202}$	196 182	196 182	2.797 3.244
15	380	380	350	350	320	320	290	290	208	208	188	188	169	169	3.724
16	356	356	328	328	300	300	272	272	195	195	176	176	159	159	4.237
17 18	335 317	335 317	309 292	309 292	$\frac{282}{267}$	$\frac{282}{267}$	$\frac{256}{242}$	256 242	184 174	$\frac{182}{168}$	$\frac{166}{157}$	$\frac{164}{152}$	150 141	147 136	4.783 5.363
19	300	300	276	276	253	253	229	229	165	156	149	141	134	126	5.975
20 21	285 272	285 272	263 250	$\frac{263}{250}$	240	240 229	$\frac{218}{207}$	218 207	156 149	146 136	141 134	131 122	$\frac{127}{121}$	118 110	6.621 7.299
22	259	259	239	239	218	218	198	198	142	127	128	114	116	103	8.011
23 24	248 238	$\frac{248}{237}$	$\frac{228}{219}$	$\frac{228}{217}$	209 200	209 199	189 181	189 180	136 130	119 111	123 118	107	111 106	96 90	8.756 9.534
25	228	224	210	206	192	188	174	170	125	105	113	94	102	85	10.345
26 27	$\frac{219}{211}$	$\frac{212}{202}$	$\frac{202}{195}$	196 185	185 178	178 169	167 161	$\frac{162}{153}$	120 116	98	109 105	89	98	79 75	11.189 12.066
28	204	192	188	177	171	161	155	146	112	87	101	78	91	70	12.977
29 30	197 190	183 174	181 175	$\frac{168}{160}$	166 160	153 146	150 145	139 132	108	82	97	74 69	88 85	66	$13.920 \\ 14.897$
31	184	166	169	153	155	139	140	126	101	73	91	65	82	59	15.906
32	178 173	$\frac{159}{151}$	164 159	146 139	$\frac{150}{145}$	133 127	136 132	$\frac{120}{115}$	98 95	69	88 86	62	79 77	55	16.949 18.025
33 34	168	145	155	133	141	121	128	110	92		83		75		19.134
35	163	138	150	127	137	116	124	105	89		81		73		20.276
36 37	158 154	$\frac{132}{127}$	146 142	122 116	133 130	111	121 118	101	87 85		78 76	1	71 69		21.451 22.659
38	150	121	138	112	$\frac{126}{123}$	102 98	115	92	82 80		74 72		67		23.901
39 40	146 143	$\frac{117}{112}$	$\frac{135}{131}$	107	120	93	112 109	88 85	78		71		65 64		25.175 26.483
41	139	107	128	99	117	90	106	81	76		69		62		27.823
42 43	136 133	103	$\frac{125}{122}$	94 91	114 112	86 82	104	78 75	74 73		67	1	61 59		29.197 30.604
44	130	95	119	87	109	79	99	71	71		64		58		32.044
45 46	127 124	91 87	117	83	107	76	97	69	69		63		56 55		33.517 35.023
47	121	84	112	77	102	13	93	00	67		60		54		36.563
48 49	119 116		109 107		100 98		91 89		65		59 58		53 52		38.135 39.741
50	114		105		96		87		63		56		51		41.379
51	112		$\frac{103}{101}$		94 92		85 84		61		55 54	1	50 49		43.051
52 53	110 108		99		91		82		59		53		48	1	44.756 46.494
54	106 104		97		89		81		58		52		47		48.265
55 56	104		96		87 86		79		56		51		46		50.069 51.906
57	100		92		84	1	76		55		49		45		53.777
58	98		1			1			F						55,680

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

				N	omina	al Dep	th an	d Fla	age W	idth—	Weigl	ht per	Foot			
Spa	n			CB	244	24''x	14"				СВ	243	24′′x	12"		Ocefficient of Deflection
in Fed		160	lbs.	150		140	lbs.	130	lbs.	120	lbs.	110		100	lbs.	of of effec
1.00					Late							Later	_			ರ ದ
		Fixed	Free													
										262	262	239	239	216	216	
13 14		$\frac{330}{313}$	$\frac{330}{313}$	$\frac{309}{293}$	$\frac{309}{293}$	$\frac{287}{274}$	$\frac{287}{274}$	$\frac{265}{254}$	$\frac{265}{254}$	$\frac{248}{230}$	248 230	$\frac{227}{211}$	$\frac{227}{211}$	$\frac{207}{192}$	$\frac{207}{192}$	2.797 3.244
15		292				255	$25\overline{5}$	$\frac{237}{237}$	237	215	215	197	197	179	179	3.724
16		274			257	239	239	222	222		201	185	185	168	168	4.237
17 18		$\frac{258}{243}$		$\frac{242}{228}$	$\frac{242}{228}$	$\frac{225}{213}$	$\frac{225}{213}$	209 198	209 198	189 179	189 179	174 164	174 164	158 149	158 149	4.783 5.363
19)	231 219	231	216		$\frac{202}{192}$	$\frac{202}{192}$	187 178	187 178	169 161	$\frac{169}{161}$	155 148	155	141 134	141 134	5.975 6.621
													148			
$\frac{21}{22}$	2	199	199	$\frac{196}{187}$	187	182 174	$\frac{182}{174}$	$\frac{169}{162}$	169 162	153 146	$\frac{152}{142}$	141 134	$\frac{138}{130}$	$\frac{128}{122}$	126 118	7.299 8.011
28 24		191 183	191 181	179 171	179 170	167 160	$\frac{167}{158}$	155 148	$\frac{155}{147}$	140 134	134 126	$\frac{128}{123}$	$\frac{122}{115}$	$\frac{117}{112}$	111 105	8.756 9.534
25			172			153	150	142	139	129	119	118	109	107	99	10.345
26	3	169	163	158	152	147	142	137	132	124	113	114	103	103	94	11.189
27 28		162 156	$\frac{155}{147}$	$\frac{152}{147}$	$\frac{145}{138}$	$\frac{142}{137}$	$\frac{135}{128}$	$\frac{132}{127}$	125 119	119 115	$\frac{107}{101}$	$\frac{109}{105}$	97 92	99	89 84	12.066 12.977
29 30)	151 146	140	$\frac{142}{137}$	$\frac{131}{125}$	132	$\frac{122}{116}$	$\frac{123}{119}$	114 108	111 107	96 91	102 98	88 83	93	80 76	13.920 14.897
$\frac{31}{32}$	2	141 137	$\frac{128}{121}$	$\frac{132}{128}$	$\frac{119}{114}$	120	111 106	115 111	103 98	104 101	86 82	95 92	79 75	87	72 68	15.906 16.949
33 34		133 129	116 111	$\frac{124}{121}$	$\frac{109}{104}$	116 113	101 97	$\frac{108}{105}$	94 90	98 95	78 74	89 87	71 68	81 79	65 62	18.025 19.134
38		125	106	117	99	109	92	102	86	92	71	84	65	77	59	20.276
36		122		114	95	106	89	99	82	89	67	82	62	75	56	21.451
37 38		$\frac{118}{115}$	97 93	111 108	91 87	$\frac{104}{101}$	85 81	96 94	79 75	87	64	80 78	59 56	73	53	22.659 23.901
39 40)	112 110	89 86	$\frac{105}{103}$	83 80	98 96	78 74	91 89	72 69	83 81	58 56	76 74	54 51	69	48	25.175 26.483
					77				1	79	00	72	OI		10	
41	2	$\frac{107}{104}$	82 79	100 98	74	93 91	72 68	87 85	66 64	77		70		65 64		27.823 29.197
44		$\frac{102}{100}$	76 72	95 93	71 68	89 87	66	83	61 58	75 73		69		62		30.604 32.044
45		97	70	91	65	85	61	79	56	72		66		60		33.517
46		95	67	89	62	83	58	77	54	70		64		58		35.023
47		93 91	64	87 86		82 80		76 74		69 67		63 62		57 56		36.563 38.135
49 50	9	89		84		78 77		73 71		66		60 59		55		39.741 41.379
										64				54		
5: 5:		86 84		81 79		75		70		63		58		53		43.051 44.756

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

				Nom	inal D	epth a	and Fl	ange '	Width	-Wei	ght pe	r Foo	t		
Span		СВ	242	24"x	934"			241		CI	3 213	21"x	:13"		ient
in Feet	94	lbs.	85	lbs.	76	lbs.		lbs.	120	lbs.	112	lbs.	104	lbs.	Coefficient of Deflection
				rally			-	rally	-		Late				υ Ă
	Fixed 243	Free 243	Fixed 218	Free 218	Fixed	Free 194	Fixed 192	Free 192	Fixed	Free	Fixed	Free	Fixed	Free	
10	240	240	217	217	194	194	174	174							1.655
11	218	218	197	197	177	177	158	158 145							2.003
12 13	200 185	200 185	181 167	$\frac{181}{167}$	$\frac{162}{149}$	162 149	145 134	134	$\frac{227}{223}$	$\frac{227}{223}$	$\frac{211}{208}$	$\frac{211}{208}$	195	195	2.383 2.797
14 15	171 160	171 160	$\frac{155}{145}$	155 145	139 129	139 129	$\frac{124}{116}$	124 114	$\frac{207}{194}$	$\frac{207}{194}$	194 181	194 181	180 168	180 168	3.244 3.724
16	150	150	136	136	121	121	109	104	181	181	169	169	157	157	4.237
17 18	141 133	140 129	$\frac{128}{121}$	$\frac{126}{117}$	114 108	112 104	102 96	96 88	171 161	$\frac{171}{161}$	159 151	$\frac{159}{151}$	$\frac{148}{140}$	148 140	4.783 5.363
19 20	$\frac{126}{120}$	$\frac{120}{112}$	114 109	108 101	102 97	97 90	91 87	82 76	$\frac{153}{145}$	153 145	143 136	143 136	$\frac{132}{126}$	132 126	5.975 6.621
21	114	104	103	94	92	84	83	70	138	138	129	129	120	120	7.299
22 23	109 104	98	99 94	88 82	88 84	79 74	79 76	65	132 126	131 124	123 118	123 116	$\frac{114}{109}$	114 107	8.011 8.756
24	100	86	90	77	81	69	72 69	57	121	117	113	109	105	101	9.534
25 26	92	80 75	87	73 68	78 75	65	67	53 49	116 112	105	108 104	103 98	101	96	10.345
27	89	71	80	64	72	57 54	64	46	108	100	100	93	93	86	12.066
28 29	86 83	67 63	78 75	60 57	69 67	50	62 60	40	104 100	90	93	88 84	90 87	82 78	$12.977 \\ 13.920$
30	80	59 56	72	53	65	48	,58		97	85	90	80	84	74	14.897
31 32	75	53	70 68	50 47	63 61	42	56 54		91	81 77	87 85	76 72	81 79	70 67	15.906 16.949
33 34	73 71		66 64		59 57		53 51		88 85	74 70	82 80	69 66	76 74	64	18.025 19.134
35	69		62		55		50		83	67	77	63	72	58	20.276
$\frac{36}{37}$	67		60 59		54 52		48 47		81 78	64	75 73	60 57	70 68	55 53	21.451 22.659
38 39	63 62		57 56		51 50		46 45		76 74	58 56	71 69	55 52	66	51 48	23.901 25.175
40	60		54		49		43		73	54	68	50	63	46	26.483
41 42	59 57		53 52		47 46		42 41		71 69	51 49	66 65	48 46	61 60	44 42	27.823 29.197
43	56		50		45		40		68	30	63	40	58	12	30.604
44 45	55 53		49 48		44 43		39 39		66 65		62 60		57 56		32.044 33.517
46	52		47		42		38								35.023
47 48	51 50		46 45		41 40		37 36								36.563 38.135
49 50	49		44		40		35 35								39.741 41.379
51	47		43		38		34								43.051
			1							1		1.			

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

	İ		1	Nomin	al De	pth ar	nd Fla	nge W	idth-	-Wei	ght pe	r Foot	:		1
Span		CI	3 212	21"	x9"				CE	211	21"	x8"			ent
in Feet	92	lbs.		lbs.		lbs.	70	Ibs.	64	lbs.	60	lbs.	58	lbs.	Coefficient of Deflection
	D: 1	In		erally				1 -	1		erally				చి ద
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
9	010	010		400			184	184	167	167	158	158	151	151	
10	$\frac{213}{210}$	$\frac{213}{210}$	$\frac{199}{196}$	$\frac{199}{196}$	$\frac{184}{182}$	$\frac{184}{182}$	$\frac{172}{155}$	$\frac{172}{155}$	$\begin{array}{c} 157 \\ 142 \end{array}$	$\begin{array}{c} 157 \\ 142 \end{array}$	147 132	$\frac{147}{132}$	143 128	143 128	1.341 1.655
11	191	191	178	178	166	166	141	141	129	129	120	120	117	117	2.003
12 13	175 161	175 161	$\frac{163}{151}$	163 151	$\frac{152}{140}$	$\frac{152}{140}$	129 119	129 119	118 109	118 109	$\frac{110}{102}$	$\frac{110}{102}$	107	107	2.383 2.797
14 15	$\frac{150}{140}$	150 140	140 131	$\frac{140}{131}$	$\frac{130}{122}$	$\frac{130}{122}$	111	109	101	100	95	93 85	92	90	3.244
16	131	128	122	120						91	88		86	82	3.724
17	123	118	115	111	$\frac{114}{107}$	$\frac{112}{103}$	97 91	91 84	89 83	83 76	83 78	78 71	80 75	75 69	4.237 4.783
18 19	116 110	$\frac{110}{101}$	$\frac{109}{103}$	$\frac{102}{95}$	101 96	95 88	86 82	77 71	79 75	70 65	74 70	65	71 68	63	5.363 5.975
20	105	94	98	88	91	82	77	66	71	60	66	56	64	54	6.621
$\frac{21}{22}$	100 95	88	93 89	82 76	87 83	76 71	74 70	61 56	67 64	56 52	63 60	52 48	61 58	50	7.299
$\frac{23}{24}$	91 87	81 76 71	85 82	71	79 76	66	67	52	62	48	58	45	56	46	8.011 8.756
25	84	67	78	66 62	73	62 58	65 62	49 45	59 57	45 41	55 53	41 38	53 51	40 37	9.534 10.345
26	81	62	75	58	70	54	60	42	55	39	51	36	49	35	11.189
27 28	78 75	59 55	73 70	55 51	68 65	51 48	57 55		52 51		49		48 46		$\frac{12.066}{12.977}$
29 30	72 70	51 48	68 65	48	63 61	44 42	53 52		49		46 44		44		13.920
31	68		63		59		50		46		43		41		14.897
32 33	65 64		61 59		57 55		48 47		44		41		40		15.906 16.949
34 35	62		58		54'		46		43 42		40 39		39 38		18.025 19.134
	60		56		52		44		40		38		37		20.276
36 37	58 57		54 53		51 49		43 42		39		37 36		36 35		21.451 22.659
38 39	55 54		52 50		48		41 40		37 36		35		34		23.901
40	52		49		46		39		35		33		32		25.175 26.483
41 42	51 50		48 47		44 43		38		35		32		31		27.823
43	49		46		42		37		34		32		31		29.197 30.604
44 45	48 47		45		41		35 34		32 31		30 29		29 28		32.044 33.517
								1					-		00.011

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

			No	minal I	Depth :	and Fla	ange W	idth—	Weight	per Fo	oot		1
Span		Cl	B 183	18"x1	2"			CE	3 182	18"x8	1/2"		Coefficient of Deflection
in Feet	100	lbs.		lbs.	86	lbs.	78	lbs.		lbs.	67	lbs.	Soefficient of Deflection
	-		_	erally			-			rally			ပြိ ရိ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	-
							172	172					
9							171 154	171 154	158	158	146	$\frac{146}{132}$	1.341
											132		1.655
11 12	$\frac{182}{174}$	$\frac{182}{174}$	168	168	154	154	140 129	140 129	129 119	129 119	120 110	120 110	2.003
13	160	160	149	149	138	138	119	119	109	109	102	102	$2.383 \\ 2.797$
14 15	149 139	149 139	139 129	139 129	$\frac{128}{120}$	$\frac{128}{120}$	110 103	110 101	102 95	102 93	95 88	95 87	3.244 3.724
16 17	130 123	$\frac{130}{123}$	121 114	121 114	$\frac{112}{106}$	112 106	96 91	93 85	89 84	85 78	83 78	80 73	4.237 4.783
18	116 110	116 110	108	108	100	100	86	79	79	73	74	67	5.363
19 20	104	104	102 97	102 97	94	94 90	81 77	73 67	75 71	67 62	70 66	62 58	5.975 6.621
21	99	98	92	91	85	84	73	63	68	58	63	53	7.299
22	95	92	88	85	82	79	70	58	65	54	60	50	8.011
23 24	91 87	87 82	84 81	80 76	78 75	74 70	67 64	54 50	62 59	50 47	58 55	46	8.756 9.534
25	83	77	78	72	72	66	62	47	57	43	53	40	10.345
26	80	73	75	68	69	63	59	44	55	41	51	38	11.189
27 28	77 75	69 65	72 69	64	66 64	59 56	57 55	41 39	53 51	38	49 47	35 33	$12.066 \\ 12.977$
29	72	62	67	58	62	53	53	09	49	90	46	99	13.920
30	70	59	65	55	60	50	51		47		44		14.897
31 32	67 65	56 53	63 61	52 49	58	48	50		46		43		15.906
33	63	51	59	47	56 54	46 43	48 47		44 43		41		16.949 18.025
34 35	61	48 46	57 55	45 42	53 51	41 39	45 44		42		39		19.134
									41		38		26.276
36 37	58	44	54	40	50	37	43		40		37		21.451 22.659
38	55		51		47		41		37		35		23.901
39	53		50		46		40		36		34		25.175
	1						1						

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

	1		No	omina	l Dept	th and	Flan	ge Wi	dth—	Weigh	t per	Foot			
G			CB :	181	18"x7	1/2"				СВ	165	16"x1	4"		Coefficient of Deflection
Span	58	lbs.	52	lbs.		lbs.	47	lbs.	115	lbs.		lbs.	100	lbs.	of of effec
Feet					erally							rally			ŏ Á
	Fixed	Free	Fixed	Free	Fixed	Free									
	143	143	128	128	135	135	115	115							
8 9	$\frac{140}{125}$	$\frac{140}{125}$	$\frac{126}{112}$	$\frac{126}{112}$	$\frac{120}{107}$	$\frac{120}{107}$	$\frac{114}{101}$	$\frac{114}{101}$							1.059 1.341
10	112	112	101	101	96	96	91	91							1.655
11	102	102	92	92	87	87	83	83							2.003
12	94	94	84	84	80	80	76	76	173	173	160	160	148	148	2.383
13 14	86	86 77	77 72	77 69	74 68	73 66	70 65	69	$\frac{168}{156}$	$\frac{168}{156}$	157 145	157 145	146 136	146 136	2.797 3.244
15	75	70	67	63	64	60	61	57	146	146		136		127	3.724
16	70	64	63	58	60	55	57	52	137	137	127	127		119	4.237
17 18	66	59 54	59 56	53 48	56 53	50 46	54 51	48	129 122	$\frac{129}{122}$	120 113	120 113	112 106	112 106	4.783 5.363
19	59	50	53	45	50	42	48	40	115	115	107	107	100	100	5.975
20	56	46	50	41	48	39	46	37	109	109	102	102	95	95	6.621
21	53	42	48	38	46	36	43	34	104	104	97	97	91	91	7.299
22 23	51 49	39 36	46	35 32	44 42	33	41 40	32 29	99 95	99 95	93	93 89	86 83	86	8.011 8.756
24	47	34	42	30	40	29	38	27 25	91	90	85	84	79	79	9.534
25	45	31	40	28	38	27	36	25	88	86	81	-80	76	74	10.345
26 27	43		39		37 36		35 34		84	81	78 75	76 72	73 70	71 67	11.189 12.066
28	40		36		34		33		78	73	73	68	68	64	12.977
29 30	39		35 34		33 32		31		75 73	70 67	70 68	65 62	66	61 58	13.920 14.897
	1														
$\frac{31}{32}$	36 35		32		31 30		29 28		71 68	63	66 64	59 56	61 59	55 52	15.906 16.949
33	34		31		29		28		66		62		58		18.025
34 35	33		30 29		28 27		27 26		64		60 58		56 54		19.134 20.276
36	31		28		27		25								21.451
37	30		27	1	26		25								22.659
38 39	30		27 26		25 25		24								23.901 25.175
0.0	1 20	1	1 20	1	20	1	20								20.3.0

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

			Nomina	l Deptl	h and F	lange V	Vidth-	Weigh	t per Fo	oot			
Span		CE	164	16"x12	"			CB	163	16"x8½	2"		Coefficient of Deflection
Feet	90	lbs.		lbs.	76	lbs.	68	lbs.		lbs.	581	bs.	of of sflec
	-			rally					Late	_			ပိုမို
-	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							142.1	142.1	130.8	130.8	120.0	120.0	
9 10	160.8	160.8	147.7	147.7	*01.4				$\overline{125.0}$ 112.5				1.341
					134.1	134.1						103.5	1.655
11 12	152.3	$152.3 \\ 139.6$	128 8	140.5	128.6	128.6	110.4	110.4	$102.3 \\ 93.8$			94.1 86.3	2.003
13	128.9	128.9	118.9	118.9	108.8	108.8	93.4	93.4	86.5	86.5	79.7	79.7	2.797
14 15	$119.7 \\ 111.7$	$119.7 \\ 111.7$	$110.4 \\ 103.0$	$\frac{110.4}{103.0}$	$\frac{101.1}{94.3}$	$101.1 \\ 94.3$	86.7 81.0	86.7	80.4 75.0				
						7							
16 17	$104.7 \\ 98.6$	98.6	96.6 90.9	90.9	83.2	83.2	71.4	67.3				$62.2 \\ 57.1$	4.237 4.783
18 19	93.1 88.2	93.1 88.2	85.9 81.3			78.6 74.5	67.5	61.9				52.6	5.363
20	83.8							53.1	56.3				5.975 6.621
21	79.8	78.9	73.6	72.4	67.4	66.3	57.8	49.3	53.6	45.6	49.3	41.8	7.299
22 23	76.2 72.8	74.1	70.2 67.2	68.1	64.3	62.3	55.2	45.9	51.1	42.4	47.1	39.0	8.011
24	69.8	65.7	64.4	60.4					48.9 46.9			$\frac{36.2}{33.7}$	
25	67.0	62.0	61.8	57.0	56.6	52.2	48.6	37.2	45.0	34.3	41.4		10.345
26	64.4	58.7	59.4								39.8	29.4	11.189
27 28	62.1 59.8	$55.5 \\ 52.6$		51.0 48.3			$45.0 \\ 43.4$			$\frac{30.0}{27.9}$			$12.066 \\ 12.977$
29	57.8	49.9	53.3	45.8	48.8	41.9	41.9		38.8		35.7		13.920
30	55.9	47.3	51.5	43.5	47.2	39.8	40.5		37.5		34.5		14.897
31 32	54.0 52.4	$\frac{45.0}{42.7}$		$\frac{41.3}{39.2}$					$\frac{36.3}{35.2}$		33.4		15.906
33	50.8	42.1	46.8	39.4	42.9	00.9	36.8		34.1		$\frac{32.4}{31.4}$		16.949 18.025
34 35	49.3		45.5		41.6		35.7 34.7		33.1		30.5		19.134
- 00	21.9		42.2		40.4		39.7		32.1		29.6		20.276

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

***************************************	1		Nomi	nal Dej	oth and	Flang	e Widt	h—Wei	ght per	Foot			
Span			C	B 162	16"x7	711			C	B 161	16"x6	6"	Coefficient of Deflection
in Feet	50	lbs.	45			lbs.	40	lbs.	38	lbs.		lbs.	of
1000		1			rally			-		_	rally		O A
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
6 7 8 9		117.7 109.3		98.4	116.9 100.2 87.7	$100.2 \\ 87.7$	92.8	92.8	100.6 90.4 79.1	$\frac{100.6}{90.4}$ 79.1	92.4 83.3 72.9	92.4 83.3 72.9	0.596 0.811 1.059
10	97.1 87.4	97.1 87.4	87.4 78.7	87.4 78.7	77.9 70.1		77.7 69.9	77.7 69.9	70.3 63.3	70.3 63.3	64.8 58.3	64.8 58.3	1.341 1.655
11 12 13 14 15	79.5 72.8 67.2 62.4 58.3	72.6 65.1 58.8	65.6 60.5 56.2	$58.4 \\ 52.7$	58.4 53.9 50.1	58.2 52.3 47.2	63.6 58.3 53.8 50.0 46.6		57.5 52.7 48.7 45.2 42.2	55.7 49.4 44.1 39.6 35.6	53.0 48.6 44.9 41.7 38.9	51.4 45.6 40.7 36.4 32.8	2.003 2.383 2.797 3.244 3.724
16 17 18 19 20	54.6 51.4 48.6 46.0 43.7	$\frac{44.4}{40.6}$	$\frac{46.3}{43.7}$	39.8 36.4 33.3	$\frac{41.3}{39.0}$	35.6 32.6 29.8	43.7 41.1 38.9 36.8 35.0	38.6 35.2 32.3 29.6 27.2	39.6 37.2 35.2 33.3 31.6	32.1 29.2 26.5 24.1 21.9	36.5 34.3 32.4 30.7 29.2	29.6 26.8 24.3 22.1 20.0	4.237 4.783 5.363 5.975 6.621
21 22 23 24 25	41.6 39.7 38.0 36.4 35.0	29.0 26.7		26.0 23.9	31.9	23.3 21.4	33.3 31.8 30.4 29.1 28.0	25.0 23.0 21.1	30.1 28.8 27.5 26.4 25.3		27.8 26.5 25.4 24.3 23.3		$\begin{array}{c} 7.299 \\ 8.011 \\ 8.756 \\ 9.534 \\ 10.345 \end{array}$
26 27 28 29 30	33.6 32.4 31.2 30.1 29.1		30.3 29.1 28.1 27.1 26.2		27.0 26.0 25.0 24.2 23.4		$\begin{array}{c} 26.9 \\ 25.9 \\ 25.0 \\ 24.1 \\ 23.3 \end{array}$		24.3 23.4 22.6 21.8 21.1		22.4 21.6 20.8 20.1 19.4		11.189 12.066 12.977 13.920 14.897
31 32 33 34 35	28.2 27.3 26.5 25.7 25.0		25.4 24.6 23.8 23.1 22.5		22.6 21.9 21.3 20.6		22.6 21.9 21.2 20.6 20.0		20.4 19.8 19.2 18.6 18.1		18.8 18.2 17.7 17.2		15.906 16.949 18.025 19.134 20.276

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

	1		Nomi	inal De	nth and	d Flance	o Widtl	h-Woi	ght per	Pont		-	N.
0		C	B 145		-	a riang	g HIGH						
Span					,				B 144		0′′		Coefficient of Deflection
Feet	105	lbs.		Ibs.	85	lbs.	75	Ibs.	68		61	lbs.	of Gecti
	TV 1	-		rally	1	1				rally			S P
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
10							134.6	134.6	121.0	121.0	107.7	107.7	
10							122.2	122.2	110.7	110.7	99.3	99.3	1.655
11	154.0		137.6	137.6	121.8	121.8	111.0	111.0	100.6	100.6	90.3	90.3	2.003
12 13	144.7 133.6	144.7 133.6	130.8 120.8	130.8	117.0	117.0	$101.8 \\ 94.0$	101.8	92.2	92.2	82.8	82.8	2.383
14	124.0	124.0	112.1	112.1	100.3	100.3	87.3	87.3	79.1		$76.4 \\ 71.0$	$76.4 \\ 71.0$	2.797 3.244
15	115.8	115.8	104.7	104.7	93.6	93.6	81.4	81.4	73.8		66.2	66.2	3.724
16	108.5					87.7		76.3	69.2	69.2	62.1	62.1	4.237
17 18	$102.1 \\ 96.5$	$\frac{102.1}{96.5}$	$92.4 \\ 87.2$			82.6 78.0				64.9	58.4	58.0	4.783
19	91.4	91.4	82.6	82.6	73.9	73.9	64.3				$55.2 \\ 52.3$	$53.9 \\ 50.0$	5.363 5.975
20	86.8	86.8	78.5	78.5	70.2	70.2	61.1	57.5	55.4	51.9	49.7	46.6	6.621
21	82.7	81.7	74.8	73.6		65.8	58.2	53.6	52.7	48.6	47.3	43.4	7.299
22 23	78.9 75.5	$76.8 \\ 72.3$	$71.4 \\ 68.3$	$69.1 \\ 65.1$	$63.8 \\ 61.0$	$61.8 \\ 58.2$			50.3	45.4	45.2	40.6	8.011
24	72.4	68.1	65.4	61.3	58.5	54.8	$53.1 \\ 50.9$	47.1	$\frac{48.1}{46.1}$		43.2	$\frac{38.1}{35.7}$	8.756 9.534
25	69.5	64.3	62.8	57.9	56.2	51.8	48.9	41.4	44.3	37.5		33.5	10.345
26	66.8	60.8	60.4	54.7	54.0	48.9	47.0	38.9	42.6	35.3	38.2	31.5	11.189
27 28	$64.3 \\ 62.0$	57.5 54.5	58.1	51.8	52.0	46.3	45.2	36.8	41.0	33.2	36.8	29.6	12.066
29	59.9	54.5	54.1	49.1	50.1	43.9	43.6	34.6	39.5	31.2	35.5	28.0	12.977 13.920
30	57.9		52.3		46.8		40.7		36.9		34.3		13.920 14.897
31	56.0		50.6		45.3		39.4		35.7		20.0		15.906
					23,0		00.4		00.7		32.0		10.900

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

	1	N	ominal I	Depth ar	d Flang	e Width	-Weigh	nt per F	oot		
Span		-	CB 143	14"x8	"		C:	B 142	14"x63/4	("	Coefficient of Deflection
in Feet	58	lbs.		lbs.	48	lbs.	42			lbs.	of
			Late	erally				Late	rally		J A
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
	1						97.4	97.4	90.1	90.1	
7	117.6	117.6	106.8	106.8	96.0	96.0	92.4	92.4	85.7	85.7	0.811
8 9	$114.1 \\ 101.4$	$\frac{114.1}{101.4}$	$104.3 \\ 92.7$	$104.3 \\ 92.7$	94.5 84.0	94.5	80.8	80.8	75.0 66.7	75.0 66.7	1.059 1.341
10	91.3	91.3	83.5	83.5	75.6	75.6	64.6	64.6	60.0	60.0	1.655
11	83.0	83.0	75.9	75.9	68.7	68.7	58.8	58.8	54.6	54.6	2.003
12	76.1	76.1	69.6	69.6	63.0	63.0	53.9	53.0	50.0	49.0	2.383
13 14	70.2 65.2	70.2 64.4	64.2 59.6	64.2 58.7	58.1 54.0	58.1 53.1	49.7	47.6	46.2	$\frac{44.0}{39.7}$	2.797 3.244
15	60.9	58.7	55.6	53.5	50.4	48.4	43.1	38.7	40.0	35.9	3.724
16	57.1	53.7	52,2	48.9	47.2	44.3	40.4	35.2	37.5	32.7	4.237
17 18	53.7 50.7	49.3 45.4	49.1 46.4	44.9 41.3	44.5	40.6 37.4	38.0	32.1 29.3	35.3 33.3	29.8 27.2	4.783 5.363
19	48.0	41.9	43.9	38.1	39.8	34.5	34.0	26.8	31.6	24.9	5.975
20	45.6	38.7	41.7	35.4	37.8	31.9	32.3	24.6	30.0	22.9	6.621
21	43.5	35.8	39.7	32.8	36.0	29.5	30.8	22.6	28.6	21.0	7.299
22 23	41.5 39.7	33.2	37.9 36.3	$\frac{30.4}{28.2}$	34.4 32.9	27.4	29.4 28.1	20.8	27.3	19.3	8.011 8.756
24	38.0	28.7	34.8	26.2	31.5	23.6	26.9		25.0		9.534
25	36.5	26.7	33.4	24.4	30.2	22.0	25.9		24.0		10.345
26	35.1	24.8	32.1	22.7	29.1	20,4	24.9		23.1		11.189
27 28	33.8 32.6		30.9 29.8		$\frac{28.0}{27.0}$		23.9 23.1		$22.2 \\ 21.4$		12.066 12.977
29	31.5		28.8		26.1		22.3		20.7		13.920
30	30.4		27.8		25.2		21.5		20.0		14.897
31	29.4		26.9		24.4		20.9		19.4		15.906

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

		Non	ninal Dept	h and Fla	inge Widtl	n-Weight	per Foot		1
Span			CB 142	14"x63/4	"		CB 141	14'x6"	ient
in Feet	38	Ibs.		lbs.	33	lbs.	30	lbs.	Coefficient of Deflection
	T2: 1	1		erally	,		Late	erally	ပြိ
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
	105.0	105.0					75.4	75.4	
6	90.8	90.8	82.8	82.8	75.6	75.6	74.3	74.3	0.596
6 7 8 9	77.8 68.1	77.8 68.1	79.1 69.3	79.1 69.3	72.6 63.5	72.6 63.5	63.7	63.7	0.811
9	60.5	60.5	61.6	61.6	56.5	56.5	55.8 49.6	55.8 49.6	1.059 1.341
	54.5	54.5	55.4	55.4	50.8	50.8	44.6	44.6	1.655
11 12	49.5 45.4	49.5 44.7	50.4	50.4	46.2	46.2	40.5	39.3	2.003
13	41.9	40.1	$\frac{46.2}{42.6}$	45.3 40.6	42.3 39.1	41.5 37.3	37.2 34.3	34.8	2.383
14 15	38.9 36.3	36.2 32.8	39.6	36.6	36.3	33.5	31.9	$\frac{31.1}{27.9}$	$\frac{2.797}{3.244}$
			36.9	33.2	33.9	30.3	29.7	25.1	3.724
16 17	34.0 32.0	29.8 27.2	$\frac{34.6}{32.6}$	30.2	31.8	27.5	27.9	22.7	4.237
18	30.3	24.8	30.8	$\frac{27.5}{25.0}$	29.9 28.2	$\frac{25.1}{22.9}$	$\frac{26.2}{24.8}$	20.5 18.6	4.783 5.363
19 20	28.7 27.2	$\frac{22.7}{20.9}$	29.2 27.7	22.9 21.0	26.7	21.0	23.5	16.9	5.975
					25.4	19.3	22.3	15.3	6.621
21 22	25.9 24.8	19.2 17.6	26.4 25.2	19.3 17.7	24.2	17.7	21.2		7.299
23	23.7	11.0	24.1	17.7	$\frac{23.1}{22.1}$	16.2	20.3 19.4		8.011 8.756
24 25	22.7 21.8		23.1 22.2		21.2		18.6		9.534
					20.3		17.8		10.345
26 27	$\frac{21.0}{20.2}$	-	$\frac{21.3}{20.5}$		19.5		17.2		11.189
28	19.5		19.8		18.8 18.1		16.5		12.066 12.977
29 30	18.8		19.1		17.5		15.4		13.920
			18.5		16.9		14.9		14.897
31	17.6		17.9		16.4				15.906

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

	1		Nomi	nal De	oth and	l Flang	e Widt	h—Wei	ght per	Fcot			
Span			C	B 124	12"x1	0''			C	B 123	12"x8	"	Coefficient of Deflection
in Feet	100	lbs.	91		83	lbs.	75	lbs.	501			lbs.	of of effec
rect				Late	rally					Late	rally		2 A
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
	269.0	269.0											
5	234.3	234.3	216.0	216.0							1		0.414
6	195.3												0.596
	167.4								88.5	88.5	$\frac{79.1}{78.5}$	79.1	0.811 1.659
	$146.4 \\ 130.2$								77.5	77.5	69.7	69.7	1.341
10	117.2	117.2	111.5	111.5	106.5	106.5	101.5	101.5		69.7	62.8	62.8	1.655
11	106.5	106.5	101.4	101.4					63.4	63.4	57.1	57.1	2.003
12	97.6			92.9						58.1	52.3	52.3	2.383
.13	90.1 83.7		85.8 79.6						53.6 49.8	53.6	48.3	48.3	2.797 3.244
15	78.1		74.3			71.0	67.6		46.5	44.8	41.8	40.2	3.724
16	73.2								43.6	41.0	39,2	36.8	4.237
17 18	68.9								$\frac{41.0}{38.7}$	$37.6 \\ 34.6$	$36.9 \\ 34.9$	33.8 31.1	4.783 5.363
19	$65.1 \\ 61.7$								36.7	32.0	33.0	28.8	5.975
20	58.6				53.2		50.7	47.6	34.9	29.5	31.4	26.6	6.621
21	55.8								33.2	27.4	29.9	24.6	7.299
$\frac{22}{23}$	53.3 50.9									$25.4 \\ 23.6$	$\frac{28.5}{27.3}$	$\frac{22.8}{21.2}$	8.011 8.756
24	48.8								29.0	21.9	26.2	19.7	9.534
25	46.9		44.6		42.6		40.6		27.9		25.1		10.345
26	45.1		42.9		41.0		39.0		26.8		24.1		11.189
27	43.4		41.3		39.4		37.6		25.8		23.2		12.066

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

	8		Nomin	al Dep	th and	Flang	e Widt	h—We	ight pe	er Foot			
Span		123 'x8''			СВ	122	12"x6	2"				121 'x6''	Coefficient of Deflection
Feet	40	lbs.	36	lbs.	34	Ibs.	32	lbs.	28	lbs.	25	lbs.	of of effect
	Late	erally				Late	rally				Late	rally	D A
	Fixed	Free	Fixed	Free									
5					90.2	90.2					57.2	57,2	0.414
6 7			75.4	75.4		70.4	66.4 62.U	66.4	57.6	57.6		54.6	0.596
8	69.6	69.6		61.0		52.8	54.2			55.2 47.4		$\frac{46.8}{40.9}$	0.811 1.059
9		62.0			46.9	46.9	48.2	48.2	42.2	42.2	36.4	36.4	1.341
10	55.8	55.8	48.8	48.8	42.3	42.3	43.4	43.4	37.9	37.9	32.7	32.7	1.655
11		50.7	44.4	44.4	38.4	38.4	39.4	39.3	34.5	34.4	29.8	28.8	2.003
12 13		$\frac{46.5}{42.9}$	37.6	39.6	$35.2 \\ 32.5$		$\frac{36.1}{33.4}$	35.0	$\frac{31.6}{29.2}$	$\frac{30.5}{27.4}$	$27.3 \\ 25.2$	$\frac{25.6}{22.8}$	$\frac{2.383}{2.797}$
14	39.8	39.2		31.9				28.2	$\frac{29.2}{27.1}$	24.7		$\frac{22.8}{20.5}$	3.244
15	37.2	35.7	32.6	28.9	28.2		28.9	25.5	25.3	22.2		18.4	3.724
16	34.9	32.7	30.5	26.1	26.4	22.7	27.1	23.1	23.7	20.2	20.5	16.6	4.237
17	32.8			23.8	24.9	20.7	25,5	21.0	22.3	18.3	19.3	15.0	4.783
18 19	$\frac{31.0}{29.4}$	$\frac{27.6}{25.5}$	$\frac{27.1}{25.7}$	$\frac{21.7}{19.9}$	$\frac{23.5}{22.2}$	$\frac{18.9}{17.3}$	$\frac{24.1}{22.8}$	$\frac{19.2}{17.5}$	$\frac{21.1}{20.0}$			$13.6 \\ 12.4$	5.363 5.975
20		23.5	24.4	18.1			21.7	16.0	19.0	13.9		11.3	6.621
21	26.6	21.8	23.3	166	20.1	14.5	20.7	14.7	18.1	12.8	17.0		7 000
22	25.4	20.2	22.2	10.0	19.2		19.7	14.7	17.2	12.8	15.6		7.299 8.011
23		18.8	21.2		18.4		18.9		16.5		14.2		8.756
24 25	$\frac{23.2}{22.3}$	17.4	20,3		17.6		18.1		15.8		13.6		9.534
	22.0		19.0		16.9		17.3		15.2		13.1		10.345
26 27	21.5		18,8		16.3		16.7		14.6		12.6		11.189
21	20.7		18.1		15.6		16.1		14.1				12.066

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

Span CB 103 10"x9" CB 102 10"x8" East 10"x8" Span CB 103 10"x9" CB 102 10"x8" Span Span CB 103 10"x9" Span CB 102 10"x8" Span Span
Fixed Free Fixe
Fixed Free Fixe
Fixed Free Fixe
Fixed Free Fixe
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
8 80.1 80.1 75.5 75.5 70.9 70.9 50.8 50.8 46.8 46.8 43.6 43.6 1.05 9 71.2 71.2 67.1 67.1 63.1 63.1 45.1 45.1 41.6 41.6 38.7 38.7 1.34 10 64.1 64.1 60.4 60.4 56.8 56.8 40.6 40.6 37.5 37.5 34.8 34.8 1.65 11 58.3 58.3 54.9 54.9 51.0 51.0 51.0 38.3 33.8 31.2 31.2 29.0 29.0 29.0 2.38 13 49.3 49.3 46.5 46.5 43.7 43.7 31.2 31.2 28.8 28.8 26.8 26.8 26.8 26.8 26.8 26
8 80.1 80.1 75.5 75.5 70.9 70.9 50.8 50.8 46.8 46.8 43.6 43.6 1.05 9 71.2 71.2 67.1 67.1 63.1 63.1 45.1 45.1 41.6 41.6 38.7 38.7 1.34 10 64.1 64.1 60.4 60.4 56.8 56.8 40.6 40.6 37.5 37.5 34.8 34.8 1.65 11 58.3 58.3 54.9 54.9 51.0 51.0 51.0 38.3 33.8 31.2 31.2 29.0 29.0 29.0 2.38 13 49.3 49.3 46.5 46.5 43.7 43.7 31.2 31.2 28.8 28.8 26.8 26.8 26.8 26.8 26.8 26
10
11 58.3 58.3 54.9 54.9 51.6 51.6 36.9 36.9 34.1 34.1 31.7 2.00 12 53.4 53.4 50.3 50.3 47.3 47.3 33.8 33.8 31.2 31.2 29.0 29.0 2.38 13 49.3 49.3 46.5 46.5 43.7 43.7 31.2 31.2 28.8 28.8 26.8 26.8 27.9 14 45.8 45.8 45.8 43.2 43.2 40.5 40.5 29.0 28.9 26.8 26.6 24.9 24.5 3.24 15 42.7 42.7 40.3 40.3 37.8 37.8 27.1 26.4 25.0 24.2 23.2 22.3 3.72 16 40.0 39.7 37.8 37.3 35.5 34.8 25.4 24.2 23.4 22.1 21.8 20.4 4.23
12 53.4 53.4 50.3 50.3 47.3 47.3 33.8 33.8 31.2 31.2 29.0 29.0 23.8 13 49.3 49.3 46.5 46.5 43.7 43.7 31.2 31.2 28.8 28.8 26.8 26.8 26.8 26.8 26.8 26
13
14 45.8 45.8 43.2 43.2 40.5 40.5 29.0 28.9 26.8 26.6 24.9 24.5 3.24 42.7 42.7 40.3 40.3 37.8 37.8 27.1 26.4 25.0 24.2 23.2 22.3 3.72 16 40.0 39.7 37.8 37.3 35.5 34.8 25.4 24.2 23.4 22.1 21.8 20.4 4.23
16 40.0 39.7 37.8 37.3 35.5 34.8 25.4 24.2 23.4 22.1 21.8 20.4 4 23
20.0 00.0 00.0 00.0 00.0 00.0 20.4 20.4
18 35.6 33.9 33.6 31.7 31.5 29.6 22.6 20.4 20.8 18.7 19.4 17.2 5.26
19 33.7 31.5 31.8 29.4 29.9 27.4 21.4 18.9 19.7 17.3 18.3 15.9 5.97
20.1 20.1 20.1 10.0 17.4 14.7 6.62
21 30.5 28.8 27.0 19.3 17.8 16.6 7.29
22 29.1 27.5 25.8 18.5 17.0 15.8 8.01 23 27.9 26.3 24.7 17.7 16.3 15.2 8.75

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

		Non	ninal I	Depth	and	Flang	e Wid	th—W	Veight	per I	oot			
Span		CB	101	10''x	6"				C	B 93	9"x	9′′		Coefficient of Deflection
in Feet	30 lbs.	26	lbs.	23 1	bs.	21	lbs.	48	lbs.		lbs.	38	lbs.	oeffe of effe
reet			Later	rally						Late	rally			OA
	Fixed Fre	e Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
	61.0 61.	0 52.3	52.3	46.0	46.0	45.6	45.6							
6 7 8 9 10 11 12 13 14 15	56.7 56 48.6 48 42.6 42 37.8 37 34.0 34 30.9 30 28.4 26 26.2 23 24.3 21. 22.7 19 21.3 17. 20.0 15. 18.9 14	6 42.1 6 36.8 8 32.7 0 29.5 1 26.8 7 24.6 8 22.7 4 21.1 2 19.6 4 18.4 8 17.3	42.1 36.8 32.7 29.5 26.0 23.0 20.6 18.5 16.7	37.2 32.6 29.0 26.1 23.7 21.7 20.0 18.6 17.4 16.3 15.3	37.2 32.6 29.0 26.1 23.0 20.4 18.2 16.3 14.7	33.1 29.0 25.8 23.2 21.1 19.3 17.8 16.6 15.5 14.5 13.6	33.1 29.0 25.8 23.2 20.4 18.1 16.2 14.5 13.0 11.8 10.7	72.9 63.8 56.7 51.0 46.4 42.5 39.3 36.5 34.0 31.9 30.0	72.9 63.8 56.7 51.0 46.4 42.5 39.3 36.5 34.0 31.3 28.8	57.2 50.8 45.7 41.6 38.1 35.2 32.7 30.5 28.6 26.9	57.2 50.8 45.7 41.6 38.1 35.2 32.7 30.5 28.0 25.8	50.5 44.9 40.4 36.7 33.7 31.1 28.9 26.9 25.2 23.8	50.5 44.9 40.4 36.7 33.7 31.1 28.9 26.9 24.8 22.7	1.655 2.003 2.383 2.797 3.244 3.724 4.237
19 20	17.9 13. 17.0 11					12.2	8.8	26.9 25.5		24.1 22.9		21.3		$5.975 \\ 6.621$
21 22 23	16.2 15.5 14.8	14.0 13.4 12.8		12.4 11.8 11.3		11.0		24.3		21.8		19.2		7.299 8.011 8.756

CARNEGIE BEAM SECTIONS—Concluded

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch City of New York Code

			Nomin	nal De	pth an	d Flan	ge Wid	th—W	eight n	er Foo	t		1
Span		C	B 92				1		B 83				ent
in	35	lbs.	32	lbs.	29	lbs.	42	lbs.	36	lbs.	31	lbs.	Coefficient of Deflection
Feet			Late	rally					Late	erally			Coe
	Fixed	Free	Fixed	l Free									
	61.6	61.6	55.9	55.9	50.2	50.2							
6	60.1	60.1	54.9	54.9	49.8	49.8	65.2	65.2	55.1	55.1	46.7	46.7	0.596
7 8			47.1	47.1	42.7	42.7	57.0	57.0	48.8	48.8	41.9	41.9	0.811
9			$\frac{41.2}{36.6}$	$\frac{41.2}{36.6}$	37.3 33.2	$\frac{37.3}{33.2}$	49.8 44.3	$\frac{49.8}{44.3}$	$\frac{42.7}{38.0}$	$\frac{42.7}{38.0}$	$\frac{36.7}{32.6}$	$\frac{36.7}{32.6}$	1.059 1.341
10				33.0	29.9	29.9		39.9		34.2	29.4		1.655
11		32.7	30.0	29.8	27.2	27.0	36.2	36.2	31.1	31.1	26.7	26.7	2.003
$\frac{12}{13}$			27.5	26.6	24.9	24.0	33.2	33.2	28.5	28.5	24.5	24.5	2.383
14				$23.8 \\ 21.4$	$\frac{23.0}{21.3}$	$\frac{21.5}{19.4}$	$\frac{30.7}{28.5}$	$\frac{30.7}{28.1}$	$\frac{26.3}{24.4}$	$\frac{26.3}{24.0}$	$\frac{22.6}{21.0}$	$\frac{22.6}{20.6}$	2.797 3.244
15	24.1	21.2		19.4	19.9	17.5		25.6	22.8		19.6	18.8	3.724
16			20.6	17.5	18.7	15.9	24.9	23.5	21.4	20.1	18.3	17.2	4.237
17 18			19.4	16.0	17.6	14.4	23.5		20.1		17.3		4.783
19	19.0	16.0	18.5	14.8	16.6	13.2	22.2		19.0 18.0		16.3		5.363 5.975
20	18.0		16.5		14.9		21.0		10.0		19,5		6.621
21	17.2		15.7		14.2								7.299
			Nomin	nal De	pth an	d Flan	ge Wid	th-W	eight p	er Foo	t		
Span			CB 8	82 8'	'x6½"				*B 4	10 9"	x51/4"		Coefficient of Deflection
in Feet	30	lbs.		27 lbs		24 1	bs.	2	5 lbs.		21 lb	98.	Coefficient of Deflection
		-	I	atera	lly				I	ateral	ly		Coe
	Fixed	Free	Fix	ed_l	Free	Fixed	Free	Fixe			ixed	Free	
3 4								68.4 56.6			45.0	45.0	$0.149 \\ 0.265$
5	48.8	48.8	43	.4	43.4	38.2	38.2	45.3	3 45		1.5	41.5	0.414
6	46.8	46.8	3 42	.1 4	2.1	37.4	37.4	37.3	7 37	7 3	4.6	34.6	0.596
6 7	40.1	40.1	1 36	.1 3	6.1	32.1	32.1	32.3	3 32	.3 2	9.7	29.7	0.811
8 9	$\frac{35.1}{31.2}$	35.1				$\frac{28.1}{25.0}$	$\frac{28.1}{25.0}$	28.3 25.3		$\frac{.3}{1}$ $\frac{2}{2}$	6.0	$\frac{26.0}{22.9}$	1.059 1.341
10	28.1	28.1				22.5	22.5	22.6	3 21		0.8	19.9	1.655
11	25.5	25.4		.0 2	2.9	20.4	20.3	20.6	3 19	1 1	8.9	17.3	2.003
12 13	$\frac{23.4}{21.6}$	$\frac{22.7}{20.3}$	21.	0 2	0.4	18.7 17.3	18.1	18.9	16	.9 1	7.3	15.3	2.383
14	20.1	18.3				16.0	$16.2 \\ 14.6$	17.4 16.2		$\begin{array}{c c} .0 & 1 \\ 3 & 1 \end{array}$	6.0	$\frac{13.5}{12.0}$	$\frac{2.797}{3.244}$
15	18.7	16.5	16.			15.0	13.2	15.1			3.8	10.8	3.724
16	17.5	15.0	15.	.8 1	3.4	14.0	12.0	14.1	1 10	7 1	3.0	9.6	4.237
17 18	16.5		14.	9		13.2		13.3	3 9	.6 1	2.2	8.6	4.783
19	15.6 14.8		14.			12.5		12.6			1.5		5.363 5.975
20								11.3			10.4		6.621
21								10.8		1.	9.9		7.299
36C14	. 3 3 40	11 0					-						

STANDARD MILL SECTIONS

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of New York Code

			Nomin	al Depth	and Fla	nge W	idth—	Weigh	t per F	oot		
Span		B 39	8"x5"		9		Н	4 8"	x8''			ient
in Feet	21	Ibs.		B Ibs.	37.	7 lbs.		34.3 lb		32.6	Ibs.	Ccefficient of Deflection
2 000	-		terally				-	Lateral	ly			රි රී
· ·	Fixed	Free	Fixed	Free	Fixed	Free	Fiz	ced 1	Free	Fixed	Free	
3 4 5	57.6 56.4 42.3 33.8	57.6 56.4 42.3 33.8	$\frac{40.0}{39.2}$ 31.3		80.0	80.0	-	0.0	60.0			$0.149 \\ 0.265 \\ 0.414$
6 7 8 9 10	28.2 24.2 21.1 18.8 16.9	28.2 24.2 21.1 18.4 16.0	26.1 22.4 19.6 17.4 15.7	26.1 22.4 19.6 17.0 14.7	53.7 46.0 40.3 35.8 32.2	53.3 46.6 40.3 35.3 32.3	0 44 3 38 3 34	1.0 4 3.5 3 1.3 3	51.4 14.0 38.5 34.3 30.8	50.1 43.0 37.6 33.4 30.1	50.1 43.0 37.6 33.4 30.1	0.596 0.811 1.059 1.341 1.655
11 12 13 14 15	15.4 14.1 13.0 12.1 11.3	14.0 12.3 10.9 9.6 8.6	14.2 13.1 12.1 11.2 10.4	12.8 11.3 9.9 8.8 7.8	29.3 26.8 24.8 23.0 21.4	29.3 26.8 24.8 22.7 20.7	3 25 3 23 7 22	$ \begin{array}{c c} .7 & 2 \\ .7 & 2 \\ .0 & 2 \\ \end{array} $	3.7	27.3 25.1 23.1 21.5 20.1	27.3 25.1 23.1 21.1 19.2	2.003 2.383 2.797 3.244 3.724
16 17 18 19	10.6 10.0 9.4 8.1	7.7	9.8 9.2 8.7 7.5	7.0	20.1 19.0 17.9 15.3	19.0	19 18 17 14	.1	8.1	18.8 17.7 16.7 14.3	17.6	4,237 4,783 5,363 5,975
			Nomin	al Depth	and Fl	ange W	/idth-	-Weigl	ht per l	Foot		
Span	Н	3-A	6"x6"		Н 3	6"x6"		H2	5"x5"	H1	4"x4"	on
in Feet	27.5 1	bs.	25 lbs.	22.5	b lbs.	20	lbs.	18.9	9 lbs.	13.8	lbs.	Coefficient of Deflection
reet		Latera	lly		Late	rally		Late	erally	Late	erally	Coe
	Fixed	Free Fi	ixed Fr	ee Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
3 4 5	$\frac{52.6}{43.8}$ $\frac{4}{3}$ $\frac{3}{3}$ $\frac{5}{3}$		$\frac{17.6}{3.4} = \frac{37}{33}$		45.0 36.5 29.2	30.0 27.6	$\frac{30.0}{27.6}$	$\frac{31.3}{25.3}$ $\frac{20.3}{20.3}$	$\frac{31.3}{25.3}$ 20.3	$ \begin{array}{r} 25.0 \\ \hline 18.8 \\ 14.1 \\ 11.3 \end{array} $	$ \begin{array}{r} 25.0 \\ \hline 18.8 \\ 14.1 \\ 11.3 \end{array} $	0.149 0.265 0.414
6 7 8 9 10	29.2 2 25.0 2 21.9 2 19.5 1 17.5 1	$ \begin{bmatrix} 25.0 & 23 \\ 21.9 & 26 \\ 19.5 & 13 \end{bmatrix} $	7.9 27 3.9 23 0.9 20 8.6 18 6.7 16	.9 20.8 .9 18.2 .6 16.2		19.7 17.2 15.3	23.0 19.7 17.2 15.3 13.7	16.9 14.5 12.7 11.3 10.1	16.9 14.5 12.7 11.0 9.5	9.4 8.1 7.1 6.3 5.7	9.4 8.0 6.6	0.596 0.811 1.059 1.341 1.655
11 12 13 14 15	15.9 14.6 13.5 12.5 11.7	13.7	5.2 14 3.9 13 2.9 1.1		11.4	11.5 10.6 9.9 9.2	12.1 10.7	9.2 8.4 7.8	o bla ch	5.1	waha	2.003 2.383 2.797 3.244 3.724

CARNEGIE BEAM SECTIONS—Continued ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch City of Chicago Code

	1		Nor	ninal	Depth	and	Flang	e Wid	lth—V	Veight	per I	oot		1	
Span			CB	302	30"x	14''				CB :	301	30"x1	0½"		Coefficient of Deflection
in	240	lbs.	220	lbs.	200	lbs.	180	lbs.	135	lbs.	125	lbs.	115	lbs.	of
Feet				Later	rally						Late	rally			Coe Def
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
12									$\frac{376}{347}$	$\frac{376}{347}$	$\frac{347}{321}$	$\frac{347}{321}$	$\frac{318}{295}$	318	2.383
13									320	320	296	296	273	273	$\frac{2.363}{2.797}$
14	547	547	498	498	450	450	402	402	297	297	275	275	253	253	3.244
15	525	525	481	481	437	437	394	394	277	277	257	257	236	236	3.724
16 17	492	492	451	451	410	410	369	369	260	260	241	241	$\frac{222}{209}$	222	4.237
18	463 437	$\frac{463}{437}$	424	424 401	386 364	386 364	347 328	$\frac{347}{328}$	$\frac{245}{231}$	$\frac{245}{231}$	$\frac{227}{214}$	$\frac{227}{214}$	197	209 197	4.783 5.363
19	414	414	380	380	345	345	311	311	219	219	203	203	187	187	5.975
20	394	394	361	361	328	328	295	295	208	208	193	193	177	177	6.621
$\frac{21}{22}$	375	375	343	343	312	312	281	281	198	198	183	183	169	169	7.299
23	358 342	358 342	328 314	$\frac{328}{314}$	298	$\frac{298}{285}$	$\frac{268}{257}$	$\frac{268}{257}$	189 181	189 179	$\frac{175}{167}$	175 165	161 154	161 152	8.011 8.756
24	328	328	301	301	$\frac{285}{273}$	273	246	246	173	170	160	157	148	144	9.534
25	315	315	289	289	262	262	236	236	166	161	154	149	142	137	10.345
26	303	303	277	277	252	252	227	227	160	153	148	141	136	130	11.189
27 28	291 281	291 281	$\frac{267}{258}$	$\frac{267}{258}$	$\frac{243}{234}$	243 234	$\frac{219}{211}$	$\frac{219}{211}$	154 149	145 139	143 138	134 128	$\frac{131}{127}$	124 118	12.066
29	271	271	249	249	226	226	204	204	143	132	133	122	122	112	12.977 13.920
30	262	262	240	239	219	217	197	195	139	126	128	117	118	107	14.897
31	254	251	233	230	212	209	190	187	134	121	124	111	114	102	15.906
32 33	246	$\frac{241}{232}$	$\frac{225}{219}$	221	205	200	184	180	130	115	120	107	111	98	16.949
34	$\frac{238}{231}$	223	$\frac{219}{212}$	212 204	199 193	193 185	179 174	173 166	$\frac{126}{122}$	$\frac{110}{106}$	117 113	102	$\frac{107}{104}$	94	18.025
35	225	215	206	196	187	178	169	160	119	101	110	94	101	86	20.276
36	219	207	200	189	182	172	164	154	116		107		98		21.451
37	213	199	195	183	177	166	160	149	112		104		96		22.659
38 39	$\begin{vmatrix} 207 \\ 202 \end{vmatrix}$	192 186	190 185	176 170	173 168	$\frac{160}{154}$	155 151	144 139	109		101 99		93		23.901 25.175
40	197	180	180	164	164	149	148	134	104		96		89		26.483
41	192	174	176	159	160	144	144	129	101		94		86		27.823
42	187	168	172	153	156	139	141	125	99		92		84		29.197
43 44	183 179	$ 162 \\ 157 $	168 164	148 144	153 149	135 130	137 134	$\frac{121}{117}$	97		90		82		30.604 32.044
45	175	152	160	139	146	126	131	113	92		86		79		33.517
46	171	147	157	135	143	122	128	110	90		84	1	77		35.023
47	167	143	153	131	140		126	1	89		82	1	75		36.563
48 49	164 161		150 147		137 134	1	123 120	1	87		80		74 72		38.135 39.741
50	157		144		131		118	1	83		77	1	71	1	41.379
51	154		141		129		116		82		76		70		43.051
52	151	1	139		126	1	114	1	80		74		68		44.756
53 54	149 146		136 134		$\frac{124}{121}$		111	1	78 77		73		66		46.494 48.265
55	143		131		119		107		76		70	1	64		50.069
56	141		129		117		105		74		69	1	63		51.906
57	138		127		115		104		73		68	1	62		53.777
58 59	136 133		$\frac{124}{122}$		113 111		$\frac{102}{100}$		72 70	1	66	1	61		55.680
60	131		120		109		98		69		64		59		57.617 59.586
61	129		118	1	108		97		68		63	1	58		61.589
62	127		116		106		95		67	1	62		57	}	63.625

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

	1			Nomi	nal D	epth a	and F	lange '	Width	—We	ight p	er Fo	ot	1	
Span			CE	272	27"x				1	-	271		93/4"		t d
in Feet	190	lbs.	175	lbs.	160	lbs.	145	ilbs.	112	lbs.	101	lbs.	91	lbs.	fficier of lectio
				Late	rally						Late	eraly			Coefficient of Deflection
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free			Fixed	Free	Fixed	Free	D
11									309	309	277	277	249	249	0.000
11 12									$\frac{284}{261}$	284 261	$\frac{257}{235}$	$\frac{257}{235}$	$\frac{231}{212}$	$\frac{231}{212}$	$\frac{2.003}{2.383}$
13	417	417	383	383	348	348	313	313	241	241	217	217	196	196	2.797
14 15	407 380	407 380	375 350	375 350	$\frac{343}{320}$	343 320	$\frac{311}{290}$	$\frac{311}{290}$	$\frac{223}{208}$	$\frac{223}{208}$	$\frac{202}{188}$	202 188	182 169	182 169	$\frac{3.244}{3.724}$
16	356	356	328	328	300	300	272	272	195	195	176	176	159	159	4.237
17 18	335 317	335	309 292	309 292	$\frac{282}{267}$	282 267	256	$\frac{256}{242}$	184 174	184 174	166 157	$\frac{166}{157}$	150 141	150 141	4.783 5.363
19	300	300	276	276	253	253	$\frac{242}{229}$	229	165	165	149	149	134	134	5.975
20 21	285 272	285 272	263	263	240	240	218	218	156	156	141	141	127	127	6.621
22	259	259	$\frac{250}{239}$	$\frac{250}{239}$	$\frac{229}{218}$	229 218	$\frac{207}{198}$	207 198	149 142	148	134 128	133 126	121 116	120 113	7.299 8.011
23 24	248 238	248 238	$\frac{228}{219}$	228 219	$\frac{209}{200}$	$\frac{209}{200}$	189 181	189	136	132	123	119	111	107	8.756
25	228	228	$\frac{219}{210}$	210	192	192	174	181 174	$\frac{130}{125}$	125 118	118 113	$\frac{112}{107}$	$\frac{106}{102}$	101	9.534 10.345
26	219	219	202	202	185	185	167	167	120	112	109	101	98	91	11.189
27 28	$\frac{211}{204}$	$\frac{211}{204}$	195 188	195 188	178 171	178 171	161 155	$\frac{161}{155}$	116 112	$\frac{107}{102}$	$\frac{105}{101}$	96 91	94 91	86 82	12.066 12.977
29	197	197	181	181	166	166	150	150	108	97	97	87	88	78	13.920
30 31	190 184	189 182	175 169	174 167	160 155	159 153	145 140	144	104 101	92	94	83	85 82	75	14.897 15.906
32	178	174	164	161	150	147	136	133	98	84	88	76	79	68	16.949
33 34	173 168	168	$\frac{159}{155}$	154 148	145 141	$\frac{141}{136}$	132 128	$\frac{128}{123}$	95		86		77 75		18.025 19.134
35	163	155	150	143	137	131	124	118	89		81		73		20.276
36 37	158 154	150 144	146 142	138 133	133 130	$\frac{126}{121}$	$\frac{121}{118}$	114	87		78		71		21.451
38	150	139	138	128	126	117	115	110	85 82		76 74		69 67		22.659 23.901
39 40	$\frac{146}{143}$	135 130	135 131	$\frac{124}{120}$	$\frac{123}{120}$	113 109	$\frac{112}{109}$	102 99	80		72		65		25.175 26.483
41	139	126	128	116	117	105	106	95	78 76		71 69		64 62		27.823
42	136 133	121	125	112	114	102	104	92	74		67		61		29.197
43 44	130	117	$\frac{122}{119}$	108 105	112 109	99 95	101	89	73 71		66		59 58		30.604 32.044
45	127	110	117	101	107	92	97	84	69		63		56		33.517
46 47	$\frac{124}{121}$	$\frac{107}{103}$	114 112	98	$\frac{104}{102}$	89	95 93	81	68 67		61		55 54		35.023 36.563
48	119	100	109		100		91		65		59		53		38.135
49 50	116 114		$\frac{107}{105}$		98 96		89 87		64 63		58 56		52 51		39.741 41.379
51	112		103		94		85		61		55		50		43.051
52 53	110 108		101 99		92 91		84 82		60		54		49		44.756 46.494
54	106		97		89		81		59 58		53 52		48		48.265
55	104	1	96		87		79		57		51		46		50.069
56 57	102		94		86 84		78 76		. 56 55		50 49		45 45		51.906 53.777
_ 58	98		92		0.4		10		33	1	40	1	43		55.680

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

	1		No	minal	Deptl	h and	Flang	ge Wid	lth-V	Veight	per I	Poot			1
Span			CB	3 244	24">	14"				CB	243	24"x	12"		ion
in Feet	160	lbs.	150	lbs.		lbs.	130	lbs.	120	Ibs.	110	lbs.	100	lbs.	Coefficient of Deflection
1000			luce a		erally			7-				rally	,		ပိုင်
-	Fixed	Free	Fixed	Freo											
13	330	330	309	309	287	287	265	265	$\frac{262}{248}$	$\frac{262}{248}$	$\frac{239}{227}$	$\frac{239}{227}$	216	216	9.707
14 15	313	$\frac{313}{292}$	$\frac{293}{274}$	$\frac{293}{274}$	$\frac{274}{255}$	$\frac{274}{255}$	254	254	230	230	211	211	192	192	2.797 3.244
	292				1		237	237	215	215	197	197	179	179	3.724
16 17	$\frac{274}{258}$	$\frac{274}{258}$	$\frac{257}{242}$	$\frac{257}{242}$	225	$\frac{239}{225}$	$\frac{222}{209}$	222 209	201 189	$\frac{201}{189}$	185 174	185 174	$\frac{168}{158}$	168 158	4.237
18 19	$\frac{243}{231}$	$\frac{243}{231}$	$\frac{228}{216}$	$\frac{228}{216}$	$\frac{213}{202}$	$\frac{213}{202}$	$\frac{198}{187}$	198 187	$\frac{179}{169}$	179 169	164 155	164 155	149 141	149	5.363 5.975
20	219	219	205	205	192	192	178	178	161	161	148	148	134	134	6.621
$\frac{21}{22}$	209 199	209 199	196 187	196 187	$\frac{182}{174}$	182 174	$\frac{169}{162}$	$\frac{169}{162}$	153 146	153 146	$\frac{141}{134}$	141 134	$\frac{128}{122}$	$\frac{128}{122}$	7.299 8.011
$\frac{23}{24}$	191 183	191 183	$\frac{179}{171}$	179 171	167 160	167 160	155 148	155 148	140 134	140 134	128 123	128 123	117	117	8.756
25	175						142	142	129	129		118	107	107	9.534 10.345
26 27	169	169	158	158	147	147	137	137	124	123		113	103	102	11.189
28	162 156	162 156	$\frac{152}{147}$	$\frac{152}{147}$	142 137	142 137	$\frac{132}{127}$	$\frac{132}{127}$	115	$\frac{117}{112}$	$\frac{109}{105}$	107 102	99 96	97 93	$12.066 \\ 12.977$
29 30	151 146	$\frac{151}{145}$	$\frac{142}{137}$	142 136	132 128	$\frac{132}{127}$		$\frac{123}{118}$	$\frac{111}{107}$	$\frac{107}{102}$	102 98	98 94	93 89	89 85	13.920 14.897
31	141	139	132	131	124	122	115	113	104	98	95	90	87	81	15.906
32 33	137 133	134 129	128 124	$\frac{125}{121}$	120 116	$\frac{117}{112}$	111 108	109 104	101	94	92 89	86 82	84 81	78 75	16.949 18.025
34 35	$\frac{129}{125}$	124 119	121	116	113	108	$\frac{105}{102}$	100 97	95 92	86 83	87 84	79 76	79 77	72 69	19.134 20.276
36	122	115	114			100	99	93	89	80	82	73	75	66	21.451
37 38	118 115	$\frac{111}{107}$	111	104	104 101	97 93	96 94	90	87	77	80	70	73	64	22.659
39	112	103	105	97	98	90	91	87 84	85 83	74 71	78 76	68 65	71 69	61 59	$23.901 \\ 25.175$
40	110	100	103	93	96	87	89	81	81	69	74	63	67	57	26.483
41 42	$\frac{107}{104}$	96 93	100 98	90 87	93 91	84 81	87 85	78 75	79 77		72 70		65 64		27.823 29.197
43 44	$\frac{102}{100}$	90 87	95 93	84 82	89 87	$\frac{79}{76}$	83 81	73 71	75 73		69 67		62 61		30.604 32.044
45	97	84	91	79	85	74	79	68	72		66		60		33.517
46 47	95 93	82 79	89 87	77	83 82	71	77 76	66	70 69		64 63		58 57		35.023 36.563
48 49	91 89		86		80		74		_67		62		56		38.135
50	88		82		78 77		73 71		66 64		60 59		55 54		$39.741 \\ 41.379$
51	86		81		75		70		63		58		53		43.051
52	84		79		11:	-:11	1			- 11	11	1		,	44.756

CARNEGIE BEAM SECTIONS—Continued ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch City of Chicago Code

	1		N	omina	l Den	th and	Flan	go Wi	dth	Woigh	t nor	Foot			II
Span		СВ	242		93/1"	OII CHIAC	∦ CB	241	1		213	21"	13"		nt
in			7		-			x8½"			,		1		Coefficient of Deflection
Feet	94	lbs.		lbs.	76	lbs.		lbs.	_120	lbs.		2 lbs.	104	lbs.	Soef
	Fire	i Free	-	Free	River	Free		Free	Pivod	Free	4	Free	Piro	Free	
	243	243	218	218	194	194	192	192	FIAGO	1100	FILEC	FICE	FILE	Lies	
10	240	240	217	217	194	194	174	174							1.655
11 12	$\frac{218}{200}$	$\frac{218}{200}$	197 181	197 181	$\frac{177}{162}$	177 162	158 145	158 145							2.003
13	185	185	167	167	149	149	134	134	$\frac{227}{223}$	$\frac{227}{223}$	$\frac{211}{208}$	$\frac{211}{208}$	195	$\frac{195}{193}$	2.383 2.797
	$\frac{171}{160}$	$\frac{171}{160}$	155 145	155 145	139 129	139 129	124 116	$\frac{124}{116}$	207	207	194	194	180	180	3.244
		1							194	194	181	181		168	3.724
	$\frac{150}{141}$	$\frac{150}{141}$	136 128	136 128	121	121 114	$\frac{109}{102}$	$\frac{109}{102}$	181 171	$\frac{181}{171}$	169 159	169 159	157	157 148	4.237 4.783
18	133	133	121	121	108	108	96	96	161	161	151	151	140	140	5.363
	$\frac{126}{120}$	$\frac{126}{120}$	114 109	$\frac{114}{109}$	$\frac{102}{97}$	$\frac{102}{97}$	91 87	90 84	$\frac{153}{145}$	153 145	143 136	143 136	132 126	132 126	$5.975 \\ 6.621$
	114	114	103	103	92	92		79							
22	109	107	99	97	88	86	83 79 76	74	$\frac{138}{132}$	138 132	$\frac{129}{123}$	$\frac{129}{123}$	$\frac{120}{114}$	120 114	7.299 8.011
	104 100	101 96	94	91 86	84 81	82 77	76 72	70 66	$\frac{126}{121}$	$\frac{126}{121}$	118 113	118 113	$\frac{109}{105}$	109 105	8.756
25	96	91	87	82	78	73	69	62	116	116	108	108		103	9.534 10.345
26	92	86	83	78	75	69	67	59	112	112	104	104	97	97	11.189
27	89	82	80	74	72	66	64	56	108	108	100	100	93	93	12.066
28 29	86 83	78 74	78 75	70 67	69 67	63	62 60	53	104	103	97 93	96 92	90 87	89 85	12.977 13.920
30	80	71	72	64	65	57	58		97	94	90	88	84	82	14.897
31	77	68	70	61	63	54	56		94	90	87	84	81	78	15.906
32 33	75 73	64	68 66	58	61 59	52	54 53		91 88	87 83	85 82	81 78	79 76	75 72	16.949 18.025
34	71		64		57		51		85	80	80	75	74	69	19.134
35	69		62		55		50		83	77	77	72	72	67	20.276
36 37	67 65		60 59		54 52		48 47		81 78	74 71	75 73	69	70 68	64 62	21.451
38	63		57		51		46		76	69	71	64	66	60	$22.659 \\ 23.901$
39 40	62 60		56 54		50 49		45		74 73	$\frac{66}{64}$	69 68	62 60	64 63	57 55	25.175 26.483
	59				47			-	71						
41 42	57		53 52		46		42 41		69	62 60	66 65	58 56	61	53 52	27.823 29.197
43	56		50		45		40		68		63		58		30.604
44 45	55 53		49 48		44 43		39 39		66		62 60		57 56	1	$32.044 \\ 33.517$
46	52		47		42		38								35.023
47	51		46		41		37	-							36.563
48 49	50 49		45		40		36								38.135 39.741
50	48		43		39		35								41.379
51	47		43		38	-	34								43.051

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

			No	minal	Dept	h and	Flan	ge Wie	dth—	Weigh	t per	Foot			
Span		CE	3 212	21"	x9"				CB	211	21"x	8"			Coefficient of Deflection
in Feet	92	lbs.	86	lbs.	80	lbs.	70	lbs.	64	lbs.		lbs.	58	lbs.	of of effec
reet				rally						Late					ŭ Ā
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							184	184	167	167	158	158	151	151	
9	213	213	199	199	184	184	172	172	157	157	147	147	143	143	1.341
10	210	210	196	196	182	182	155	155	142	142	132	132	128	128	1.655
11	191	191	178	178	166	166	141	141	129	129			117	117	2.003
12	175	175	163	163	152	152 140	129 119	$\frac{129}{119}$	$\frac{118}{109}$	118 109	$\frac{110}{102}$	$\frac{110}{102}$	107	107	$\frac{2.383}{2.797}$
13 14	161 150	161 150	151 140	151 140	$\frac{140}{130}$	130	111	111	101	101	95	95	92	92	3.244
15	140	140	131	131	122	122	103	103	94	94	88	88	86	86	3.724
16	131	131	122	122	114	114	97	97	89	89	83	83	80	80	4.237
17	123 116	123 116	115 109	115 109	$\frac{107}{101}$	$\frac{107}{101}$	91 86	91 85	83	83	78 74	78 72	75 71	75 70	4.783 5.363
18 19			103	103	96	96	82	79	75	72	70	67	68	65	5.975
20	105	103	98	96	91	90	77	74	71	67	66	63	64	61	6.621
21	100	97	93	91	87	84	74	69	67	63	63	59	61	57	7.299
22	95 91	91 86	89 85	85 80	83 79	79 75	70 67	65	64	59 56	60 58	55 52	58 56	54 50	8.011 8.756
23 24	87	81	82	76	76	71	65	58	59	53	55	49	53	48	9.534
25	84	77	78	72	73	67	62	54	57	50	53	46	51	45	10.345
26	81	73	75	68	70	63	60	51	55	47	51	44	49	42	11.189
27 28	78 75	69	73 70	65	68	57	57 55		52		49		48		12.066 12.977
29	72	63	68	58	63	54	53		49		46		44		13.920
30	70	60	65	56	61		52		47		44		43		14.897
31	68		63		59		50		46		43		41		15.906
32 33	65		61 59		57		48		44 43		41 40		39		16.949 18.025
34	62		58		54	,	46		42		39		38		19.134
35	60		56		52		44		40		38		37		20.276
36	58	1	54		51		43		39		37		36		21.451
37 38	57 55		53 52		49 48		42		38 37		36		35 34		22.659 23.901
39	54		50		47		40		36		34		33		25.175
40	52		49		46		39		35		33		32		26.483
41	51	1	48		44		38		35		32		31		27.823
42	50	-	47	-	43		37		34	-	32		31		29.197 30.604
43 44	49 48		46		42		35		32		30		29		32.044
45	47		44		41		34		31		29		28	1	33.517

CARNEGIE BEAM SECTIONS—Continued ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

Span			B 183	18"x	12"			CI	3 182	18"x8	1/2"		ant a
in Feet	100	lbs.		lbs.	86	lbs.	78	lbs.	.72	lbs.		lbs.	Coefficient of Deflection
	-		7	erally					Later		01	1100.	Coe
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	-
							172	172					
9							171	171	158	158	146	146	1.34
							154	154	142	142	132	132	1.65
11	182	182	168	168	154	154	140	140	129	129	120	120	0.00
12 13	$\frac{174}{160}$	174 160	162 149	$\frac{162}{149}$	150	150	129	129	119	119	110	110	2.00
14	149	149	139	139	$\frac{138}{128}$	$\frac{138}{128}$	119 110	119 110	$\frac{109}{102}$	109	102	102	2.79
15	139	139	129	129	120	120	103	103	95	$\frac{102}{95}$	95 88	95 88	3.24
16	130	130	121	121	112	112	96	96	89	89	00		
17 18	123 116	$\frac{123}{116}$	114 108	114	106	106	91	91	84	84	83 78	83 78	4.23
19	110	110	108	$\begin{array}{c c} 108 \\ 102 \end{array}$	100 94	100 94	86 81	85	79	79	74	73	5.36
20	104	104	97	97	90	90	77	80 75	$\frac{75}{71}$	74 69	70 66	68	5.97 6.62
21	99	99	92	92	85	85	73	70	68	65			
22 23	95 91	95	88	88	82	82	70	66	65	61	63	60 57	7.29 8.01
24	87	87	84 81	84 81	78 75	78 75	67	62 59	62	57	58	53	8.75
25	83	83	78	78	72	72	62	56	59 57	54 51	55 53	50 48	9.53 10.34
26	80	80	75	74	69	68	59	53	55	48	51	45	
27 28	77	$\frac{76}{72}$	72 69	70 67	66	65	57	50	53	46	49	43	$\frac{11.18}{12.06}$
29	72	69	67	64	64 62	62 59	55 53	47	51 49	44	47	40	12.97
30	70	66	65	62	60	57	51		47		46		13.92 14.89
31	67	63	63	59	58	54	50		46		43		
32 33	65	61 58	61 59	56 54	56	52	48		44		41		15.900 16.949
34	61	56	57	52	54 53	50 48	47 45		43		40		18.023
35	60	54	55	50	51	46	44		42		39		$\frac{19.134}{20.276}$
36	58	52	54	48	50	44	43		40		37	1	
37	56		52		49	-	42	-	38	-	36		21.451 22.659
39	55		51		47		41		37	1	35		23.901

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

			N	lomin	al Dej	oth an	d Fla	nge W	idth-	-Weig	ht per	Foot			
Span			CB	181	18"x	71/2"				СВ	165	16''x	14''		Ccefficient of Deflection
in Feet	58	Ibs.	52	lbs.	51	lbs.	47	lbs.	115	lbs.	107		100	lbs.	of effe
reet				Lati	erally						Late				ŭ A
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
	143	143	128	128	135	135	115	115							
8	140	140	126	126	120	120	114	114							$\frac{1.059}{1.341}$
9 10	$\frac{125}{112}$	$\frac{125}{112}$	$\frac{112}{101}$	$\frac{112}{101}$	107 96	107 96	101 91	$\frac{101}{91}$							1.655
11	102	102	92	92	87	87	83	83							2.003
12	94	94	84	84	80	80	76	76	173	173	160	160	148	148	2,383
13 14	86 80	86 80	77 72	77 72	74 68	74 68	70 65	70 65	$\frac{168}{156}$	168 156	$\frac{157}{145}$	$\frac{157}{145}$	146 136	$\frac{146}{136}$	$\frac{2.797}{3.244}$
15	75	75	67	67	64	64	61	61	146	146	136		127	127	3.724
16	70	70	63	63	60	60	57	57	137	137	127	127		119	4.237
17 18	66 62	65 60	59 56	58 54	56 53	55 51	54 51	52 49	129 122	$\frac{129}{122}$	$\frac{120}{113}$	$\frac{120}{113}$	$\frac{112}{106}$	112 106	4.783 5.363
19	59	56	53	50	50	48	48	45	115	115	107	107	100	100	5.975
20	56	52	50	4.7	48	45	46	42	109	109	102	102	95	95	6.621
21	53	49	48	44	46	42	43	40	104 99	104 99	97 93	97 93	91 86	91	7.299
22 23	51 49	46 43	46	41 39	44 42	39 37	41 40	37 35	95	95	89	89	83	86 83	8.011 8.756
24	47	41 38	42	36 34	40 38	35 33	38 36	33	91 88	91 88	85	85 81	79 76	79	9.534 10.345
25	45	30		94		00		91							
$\frac{26}{27}$	43		39 37		37 36		35 34		84	84 81	78 75	78 75	73 70	73 70	11.189 12.066
28	40		36		34		33		78	78	73	73	68	68	12.977
29 30	39		35		33 32	1	31 30		75 73	75 73	70 68	70 67	66	66	13.920 14.897
31	36		32		31		29		71	70	66	65	61	60	15.906
32	35		31		30		28		68	67	64	62	59	58	16.949
33 34	34		31 30		29 28		28 27		66 64		62 60		58 56		18.025 19.134
35	32		29		27		26		63		58		54		20.276
36	31		28		27		25								21.451
37	30		27		26		25		1						22.659 23.901
38 39	30 29		27 26		25 25		24		-						25.175
	1	1	1	1	1])		1		1	1		

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

			No	ominal	Depth	and Fla	ange Wi	dth—V	Veight 1	per Foo	t		1
Span		C		16"x1			Í		-	16"x8			ich
Feet	90	lbs.		lbs.	76	lbs.	68	lbs.		lbs.	58	Ibs.	Coefficient of Deflection
		1 -		rally					Late	rally			වී බී
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							142.1	142.1	130.8	130.8	120.0	120.0	
9 10	160,8	160.8					134.9	134.9	125.0	125.0	115.1	115 1	1.341
			147.7	147.7	134.1		121.4					103.5	1.655
11 12	152.3	152.3	140.5	140.5	128.6	128.6	110.4	110.4	102.3	102.3	94.1	94.1	2.003
13						$\frac{117.9}{108.8}$		$\frac{101.2}{93.4}$	93.8	93.8	86.3	86.3	2.383
14 15	1119.7	119.7	110.4	110.4	101 1	101 1	26 7	86.7			$79.7 \\ 74.0$		
15	111.7	111.7	103.0	103.0	94.3	94.3	81.0	81.0	75.0	75.0			
16	104.7							75.9	70.3	70.3	64.7	64.7	4.237
17 18	$98.6 \\ 93.1$	98.6 93.1	90.9 85.9					71.4	66.2	66.2	60.9	60.9	4.783
19	88.2	88.2	81.3	81.3			$67.5 \\ 63.9$		$62.5 \\ 59.2$	$62.3 \\ 58.2$	57.5 54.5	57.3 53.5	5.363
20	83.8	83.8	77.3	77.3	70.8	70.8	60.7	58.9		54.5	51.8		
21	79.8	79.8	73.6	73.6	67.4	67.4	57.8	55.3	53.6	51.1	49.3	47.0	7.299
22 23	$76.2 \\ 72.8$	$76.2 \\ 72.8$	70.2	70.2	64.3	64.3	55.2	52.0	51.1	48.1	47.1	44.2	8.011
24	69.8	69.8	$67.2 \\ 64.4$	$67.2 \\ 64.4$		$61.5 \\ 59.0$		49.0	48.9 46.9	$\frac{45.2}{42.8}$	45.0		8.756
25	67.0	67.0	61.8	61.8	56.6	56.6		43.7	45.0	40.4	$\frac{43.1}{41.4}$	39.3 37.2	9.534 10.345
26	64.4	63.9	59.4	58.9	54.4	53.9	46.7	41.4	43.3	38.3	20.0		
27 28	62.1	60.9	57.2	56.1	52.4	51.4	45.0	39.2	41.7	36.3	$\frac{39.8}{38.4}$		$\begin{array}{c} 11.189 \\ 12.066 \end{array}$
29	$\frac{59.8}{57.8}$	58.2 55.6	$55.2 \\ 53.3$	$53.6 \\ 51.2$	$50.5 \\ 48.8$	$\frac{49.0}{46.8}$		37.2	40.2	34.4	37.0	31.6	12.977
30	55.9	53.2	51.5	49.0	47.2	44.8	40.5		$\frac{38.8}{37.5}$		$35.7 \\ 34.5$		$13.920 \\ 14.897$
31	54.0	50.9	49.9	46.9	45.6	42.9	39.2					1	
32	52.4	48.8	48.3	45.0	44.2	41.1	38.0		$\frac{36.3}{35.2}$		$\frac{33.4}{32.4}$		15.906 16.949
33 34	50.8		46.8		42.9		36.8		34.1		31.4		18.025
35	47.9		44.2		41.6		35.7		33.1		30.5		19.134
									02.1		29.6	l'	20.276

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

-			Nomin	al Dep	th and	Flange	Width	-Weig	ht per I	Foct			-
Span			C:	B 162	16"x7	"			C:	B 161	16"x6	"	Coefficient of Deflection
in Feet	50 1	lbs.	45 l		43 1	bs.	40 1	bs.	38 1		35 1	bs.	of of effec
rect				Late	rally					Later	ally		0 0
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
					110 K	119.5							
6					116.9				100.6	100.6	92.4	92.4	0.596
7	117.7	117.7	105.2		100.2	100.2	92.8	92.8	90.4	90.4	83.3	83.3	0.811
8	109.3		98.4	98.4 87.4		87.7	87.4 77.7	87.4 77.7	79.1	$79.1 \\ 70.3$	$72.9 \\ 64.8$	$72.9 \\ 64.8$	1.059 1.341
9 10	97.1 87.4	97.1 87.4	87.4 78.7	78.7			69.9	69.9	63.3	63.3	58.3	58.3	1.655
											***	FO 0	0.000
11	79.5						63.6 58.3	$63.6 \\ 58.3$	57.5 52.7	57.5 52.7	53.0 48.6	53.0 48.6	2.003
12 13	$72.8 \\ 67.2$					53.9	53.8	53.8	48.7	48.3	44.9	44.4	2.797
14	62.4	62.4	56.2	56.2	50.1	50.1	50.0	50.0	45.2	43.9	41.7	40.4	3.244
15	58.3	58.0	52.5	52.2	46.8	46.6	46.6	46.3	42.2	40.1	38.9	36.9	3.724
16	54.6	53.5	49.2	48.1	43.8	42.9	43.7	42.7	39.6	36.8	36.5	33.9	4.237
17	51.4	49.4	46.3	44.4	41.3		41.1	39.4	37.2	33.9	34.3	31.2	4.783
18	48.6				39.0 36.9	36.8	$\frac{38.9}{36.8}$	36.6	35.2 33.3	$\frac{31.3}{29.0}$	$\frac{32.4}{30.7}$	$28.8 \\ 26.7$	5.363 5.975
19 20	$\frac{46.0}{43.7}$						35.0	31.7	31.6	27.0	29.2	24.8	6.621
						000	00.0	00.0	00.1		27.8		7.299
$\frac{21}{22}$	$\frac{41.6}{39.7}$						33.3	$\frac{29.6}{27.8}$	$\begin{vmatrix} 30.1 \\ 28.8 \end{vmatrix}$		26.5		8.011
23	38.0						30.4	26.0	27.5		25.4		8.756
24	36.4		32.8		29.2		29.1		26.4		24.3		9.534
25	35.0		31.5		28.1		28.0		25.3		23.3		10.345
26	33.6		30.3		27.0		26.9		24.3		22.4		11.189
27	32.4	Ł.	29.1		26.0		25.9		23.4		$\frac{21.6}{20.8}$		12.066 12.977
28 29	31.2		28.1 27.1		25.0		$25.0 \\ 24.1$		$\begin{vmatrix} 22.6 \\ 21.8 \end{vmatrix}$		$\frac{20.8}{20.1}$		13.920
30	29.1		26.2		23.4		23.3		21.1		19.4		14.897
			0"		00.0		22.6		20.4		18.8		15.906
$\frac{31}{32}$	28.2 27.3		25.4 24.6		22.6	-	$\frac{22.6}{21.9}$		19.8		18.2		16.949
33	26.5		23.8		21.9		21.2		19.2		17.7		18.025
34	25.7		23.1	1	20.6		20.6		18.6		17.2		19.134
35	25.0		22.5				20.0		18.1				20.276
	W.			1	1	1	1	1			J.		

CARNEGIE BEAM SECTIONS-Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

	1		Nomi	nal De	pth and	Flange	e Width	-Weig	ght per	Foot			1
Span		C	B 145	14"x1	2"			C	B 144	14"x1	0''		Coefficient of Deflection
Feet	105	lbs.		lbs.	85	lbs.	75	lbs.	68	lbs.	61	lbs.	Coefficient of Deflection
	-			erally					Late	rally			De Co
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							134.6	134.6	101.0	121.0	108 8		
10								122.2		110.7	99.3	$\frac{107.7}{99.3}$	1.655
11	154.0	154.0	137.6	137.6	121.8	191 8		111.0				90.3	
12	144.7	144.7	130.8	130.8	117.0	117.0	101.8	101.8	92.2	92.2	82.8	82.8	2.003 2.383
13 14	133.6 124.0	133.6 124.0	$\frac{120.8}{112.1}$	$\frac{120.8}{112.1}$	$\frac{108.0}{100.3}$	108.0	94.0 87.3		85.2	85.2	76.4	76.4	2.797
15	115.8	115.8	104.7	104.7	93.6	93.6	81.4		$73.1 \\ 73.8$		$71.0 \\ 66.2$		$3.244 \\ 3.724$
16	108.5	108.5	98.1	98.1	87.7	87.7	76.3	76.3	69.2				
17 18	102.1	102.1	92.4	92.4	82.6	82.6	71.9	71.9	65.1		58.4	62.1 58.4	$\frac{4.237}{4.783}$
19	91.4	$96.5 \\ 91.4$	$87.2 \\ 82.6$	87.2 82.6	$78.0 \\ 73.9$					61.5	55.2	55.2	5.363
20	86.8	86.8	78.5	78.5	70.2			61.1		55.4	$\frac{52.3}{49.7}$	52.3 49.7	5.975 6.621
21	82.7	82.7	74.8	74.8	66.9	66.9	58.2	58.2	52.7	F0.77	47.0		
22 23	78.9	78.9	71.4	71.4	63.8	63.8	55.5	54.9	50.3	$52.7 \\ 49.7$		$\frac{47.2}{44.5}$	7.299 8.011
23	$75.5 \\ 72.4$	75.5 72.4	$68.3 \\ 65.4$	$68.3 \\ 65.4$	$61.0 \\ 58.5$	$\frac{61.0}{58.5}$	$53.1 \\ 50.9$	$51.9 \\ 49.1$		46.9	43.2	42.1	8.756
25	69.5	69.5	62.8	62.8	56.2	56.2	48.9	46.5	$\frac{46.1}{44.3}$	$\frac{44.4}{42.1}$	$\frac{41.4}{39.7}$	39.8 37.7	9.534 10.345
26	66.8	66.3	60.4	59.9	54.0	53.5	47.0	44.2	42.6	1	1		
27 28	64.3	63.2	58.1	57.1	52.0	51.0	45.2	42.0	41.0	$\frac{40.0}{38.0}$			11.189 12.066
28	62.0	60.3	54.1	54.5	50.1	48.6	43.6	40.0	39.5	36.2	35.5		12.977
30	57.9		52.3		46.8		42.1		38.2		34.3		13.920 14.897
31	56.0		50.6		45.3		39.4		35.7		32.0		15.906
											02.0	1	10.900

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

	1	N	ominal :	Depth a	nd Flang	ge Widtl	a-Weigh	ht per F	oot		
Span		(CB 143	14"x8"	,		C	B 142	14"x63/4	"	Soefficient of Deflection
in Feet	58	lbs.	53 1		48 1	bs.	42		39 1	bs.	of of effec
1000			Late	rally				Late	rally		ರೆ 4
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
							97.4	97.4	90.1	90.1	
7	117.6	117.6	106.8	106.8	96.0	96.0	92.4	92.4	85.7	85.7	0.811
8 9	$\frac{114.1}{101.4}$	114.1	$104.3 \\ 92.7$	$\frac{104.3}{92.7}$	94.5 84.0	94.5 84.0	80.8	80.8	75.0 66.7	75.0 66.7	1.059 1.341
10	91.3	91.3	83.5	83.5	75.6	75.6	64.6	64.6	60.0	60.0	1.655
11	83.0	83.0	75.9	75.9	68.7	68.7	58.8	58.8	54.6	54.6	2.003
12	76.1	76.1	69.6	69.6	63.0	63.0	53.9	53.9	50.0	50.0	2.383
13 14	$70.2 \\ 65.2$	$70.2 \\ 65.2$	64.2 59.6	64.2 59.6	58.1 54.0	58.1 54.0	49.7 46.2	49.7 46.2	46.2	46.2 42.9	2.797 3.244
15	60.9	60.9	55.6	55.6	50.4	50.4	43.1	42.5	40.0	39.4	3.724
16	57.1	57.1	52.2	52.2	47.2	47.2	40.4	39.1	37.5	36.3	4.237
17	53.7	53.5	49.1	48.9	44.5	44.2	38.0	36.2	35.3	33.5	4.783
18 19	50.7 48.0	49.8	46.4 43.9	45.5 42.4	$\frac{42.0}{39.8}$	$\frac{41.2}{38.4}$	35.9 34.0	33.5	33.3	31.1 28.9	5.363 5.975
20	45.6	43.5	41.7	39.7	37.8	35.9	32.3	29.0	30.0	26.9	6.621
21	43.5	40.8	39.7	37.2	36.0	33.7	30.8	27.1	28.6	25.1	7.299
22	41.5	38.3	37.9	35.0	34.4	31.6	29.4	25.4	27.3	23.5	8.011
23 24	39.7 38.0	$\frac{36.0}{34.0}$	36.3 34.8	$\frac{32.9}{31.0}$	$\frac{32.9}{31.5}$	29.7 28.0	28.1 26.9		$\frac{26.1}{25.0}$		8.756 9.534
25	36.5	32.1	33.4	29.3	30:2	26.5	25.9		24.0		10.345
26	35.1	30.3	32.1	27.7	29.1	25.0	24.9		23.1		11.189
27	33.8	00.0	30.9	27.1	28.0	20.0	23.9		22.2		12.066
28 29	$\frac{32.6}{31.5}$		$\frac{29.8}{28.8}$		27.0		$\frac{23.1}{22.3}$		21.4		12.977 13.920
30	31.5		28.8		25.2		21.5		20.7		13.920
31	29.4		26.9		24.4		20.9		19.4		15.906

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS

Maximum Bending Stress, 16,000 Pounds per Square Inch City of Chicago Code

	1	Nomin	nal Depth	and Flans	ge Width-	-Weight p	er Foot		
Span				14"x63/4"			CB 141	14"x6"	ent
in Feet	38	lbs.	36	lbs.	33	lbs.	30	lbs.	Coefficient of Deflection
2000			Late	rally			Late	erally	De Co
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
	105.0	105.0					75.4	75.4	
6 7	90.8	90.8	82.8	82.8	75.6	75.6	74.3	74.3	0.596
7 8	77.8 68.1	77.8 68.1	79.1 69.3	79.1 69.3	72.6 63.5	72.6 63.5	63.7	63.7	0.811
9	60.5	60.5	61.6	61.6	56.5	56.5	55.8 49.6	55.8 49.6	1.059 1.341
10	54.5	54.5	55.4	55.4	50.8	50.8	44.6	44.6	1.655
11	49.5	49.5	50.4	50.4	46.2	46.2	40.5	40.5	2.003
12 ₁₃	45.4 41.9	45.4 41.9	46.2 42.6	46.2 42.6	42.3 39.1	42.3 39.1	37.2 34.3	37.2 34.0	2.383
14	38.9	38.9	39.6	39.6	36.3	36.3	31.9	30.9	2.797 3.244
15	36.3	35.9	36.9	36.4	33.9	33.3	29.7	28.2	3.724
16	34.0	33.0	34.6	33.5	31.8	30.7	27.9	25.9	4.237
17 18	32.0 30.3	$\frac{30.5}{28.3}$	32.6 30.8	$\frac{30.9}{28.7}$	29.9 28.2	28.3 26.3	26.2 24.8	$\frac{23.9}{22.1}$	4.783
19	28.7	26.3	29.2	26.6	26.7	24.4	23.5	20.4	5.363 5.975
20	27.2	24.5	27.7	24.8	25.4	22.7	22.3	19.0	6.621
21 22	$25.9 \\ 24.8$	$\frac{22.9}{21.4}$	26.4	23.2	24.2	21.2	21.2		7.299
23	23.7	41.4	$25.2 \\ 24.1$	21.7	$\frac{23.1}{22.1}$	19.8	20.3 19.4		8.011 8.756
24 25	22.7		23.1		21.2		18.6		9.534
	21.8		22.2		20.3		17.8		10.345
26 27	$\frac{21.0}{20.2}$		21.3		19.5		17.2		11.189
28	19.5		20.5 19.8		18.8 18.1		16.5		12.066 12.977
29 30	18.8		19.1		17.5		15.4		13.920
	18,2		18.5		16,9		14.9		14.897
31	17.6		17.9		16.4				15.906

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

			Nom	inal De	pth an	d Flang	ge Widt	h—We	ight per	Foot			
Span			CI	3 124	12"x1	0''			C	B 123	12"x8	"	Coefficient of Deflection
in Feet	100	lbs.	91 1		83	lbs.	75 1	bs.	50 1	bs.	45 1	bs.	Coefficient of Deflection
1000				Late	rally					Late	rally		Coe
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
	269.0	269,0											
5	234.3		216.0	216.0									0.414
0	105 2	105 2	105 0	107.0									0.500
6 7				$185.8 \\ 159.3$		169.0			88.5	88.5	79.1	79.1	$0.596 \\ 0.811$
8							121.9	121.9		87.1	78.5	78.5	1.059
9	130.2	130.2	123.9	123.9	118.3	118.3	112.7	112.7	77.5	77.5	69.7	69.7	1.341
10	117.2	117.2	111.5	111.5	106.5	106.5	101.5	101.5	69.7	69.7	62.8	62.8	1.655
11	106.5	106.5	101.4	101.4	96.8	96.8			63.4			57.1	2.003
12 13	97.6 90.1			92.9	88.7	88.7	84.5		58.1	58.1	52.3	52.3	2.383
14	83.7			79.6	76.1	$81.9 \\ 76.1$	$78.0 \\ 72.5$	72.5	53.6 49.8	49.8		48.3	2.797 3.244
15	78.1						67.6	67.6	46.5	46.5		41.8	3.724
16	73.2	73.2	69.7	69.7	66.5	66.5	63.4	63.4	13 6	43.6	39.2	39.2	4.237
17	68.9				62.6	62.6			41.0			36.8	4.783
18	65.1		61.9	61.9					38.7	38.0			5.363
19 20	61.7 58.6					$56.0 \\ 53.2$				35.5	33.0 31.4	31.9 29.9	5.975 6.621
	00.0	00.0	00.1	00.1	00.2	00.2	50.1	00.1	04.9	30.2	31.4	29.9	0.021
21	55.8								33.2	31.1	29.9	28.0	7.299
$\frac{22}{23}$	53.3 50.9									$\frac{29.2}{27.5}$	$28.5 \\ 27.3$	$26.3 \\ 24.7$	8.011 8.756
24	48.8									25.9	26.2	23.3	9.534
25	46.9		44.6		42.6		40.6		27.9		25.1		10.345
26	45.1		42.9		41.0		39.0		26.8		94.1		11.189

Loads above upper horizontal lines will produce maximum allowable shear in webs.

Loads below lower horizontal lines will produce excessive deflections.

For maximum safe loads, see tables of Maximum Bending Moments and Web Resistances.

37.6

25.8

23.2

39.4

12.066

27

43.4

41.3

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

			Nomin	al Der	th and	Flang	e Widt	h—We	ight pe	r Foot			
Span	CB 12"				СВ	122	12"x6	1/2"			CB 12"	121 x6"	Coefficient of Deflection
Feet	40	lbs.	36	lbs.	34	lbs.	32	lbs.	28	lbs.	25	lbs.	Soeff Jeff
	Later	ally				Late	erally				Late	rally	O
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	69.6 62.0 55.8 50.7 46.5 42.9 39.8 37.2 34.9 32.8 31.0 29.4 27.9	69.6 62.0 55.8 50.7 46.5 42.9 39.8 37.2 34.9 32.6 30.4 28.3 26.5 24.8	75.4 69.8 61.0 54.3 48.8 44.4 40.7 37.6 34.9 32.6 30.5 28.7 27.1 25.7	75.4 69.8 61.0 54.3 48.8 44.4 40.7 37.6 34.7	90.2 84.5 70.4 60.4 52.8 46.9 42.3 38.4 35.2 32.5 30.2 28.2 26.4	90.2 84.5 70.4 60.4 52.8 46.9 42.3 38.4 35.2 32.5 30.1 27.6 25.4 21.7 20.2 18.8	66.4 62.0 54.2 43.4 39.4 33.4 33.4 31.0 28.9 27.1 25.5 24.1 22.8 21.7 20.7	66.4 62.0 54.2 48.2 43.4 39.4 36.1 33.4	57.6 53.2 47.4 42.2 37.9 34.5 31.6 29.2 27.1 25.3 23.7 22.3 21.1 20.0	57.6 53.2 47.4 42.2 37.9 34.5	57.2 54.6 46.8 40.9 32.7 29.8 27.3 25.2 23.4 21.8 20.5 19.3 18.2 17.2 16.4	57.2 54.6 46.8 40.9 36.4 32.7 29.8 27.3 24.9 22.7 20.7 19.0 17.5 16.2 15.0	0.414 0.596 0.811 1.059 1.341 1.655 2.003 2.383 2.797 3.244 3.724 4.237 4.783 5.363 5.975 6.621 7.299 8.011
23	24.2	21.9	21.2		18.4		18.9		16.5		14.2		8.756 9.534
$\frac{24}{25}$	$\frac{23.2}{22.3}$	20.7	20.3		$\frac{17.6}{16.9}$	-	$\frac{18.1}{17.3}$	-	15.8	-	13.6		10.345
26 27	21.5		18.8		16.3 15.6		16.7		14.6		12.6		11.189 12.066

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

	Nominal Depth and Flange Width—Weight per Foot												
Span	CB 103 10"x9"						CB 102 10"x8"						ion
in Feet				lbs. 49 lbs.						lbs. 31 lbs.			Coefficient of Deflection
	ļ	Laterally					Laterally					ပြိ ဂိ	
	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	Fixed	Free	
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	157.4 128.2 106.8 91.5 80.1 71.2 64.1 58.3 53.4 49.3 45.8 42.7 40.0 37.7 35.6 33.7 32.0	157.4 128.2 106.8	116.2 100.7 86.3 75.5 67.1 60.4 54.9 50.3 46.5 43.2 40.3 37.8 35.5 33.6 31.8 30.2	116.2 100.7 86.3 75.5 67.1 60.4 54.9 50.3 46.5 43.2 40.3 37.8 35.5 33.6 631.8	75.0 70.9 63.1 56.8 51.6 47.3 43.7 37.8 35.5 33.4 31.5 29.9 28.4	76.0 70.9 63.1 56.8 51.6 47.3 43.7 37.8 35.5 33.4 31.5 29.8 27.9	128.8 101.5 81.2 67.7 58.0 50.8 45.1 40.6 36.9 33.8 31.2 29.0 27.1 25.4 23.9 22.6 21.4 20.3	128.8 101.5 81.2 67.7 58.0 50.8 45.1 40.6 36.9 33.8 31.2 29.0 27.1 25.4 23.9	93.4 74.9 62.4 53.5 46.8 41.6 37.5 34.1 31.2 28.8 26.8 25.0 23.4 22.0 20.8 19.7 18.7	93.4 74.9 62.4 53.5 46.8	58.1 49.8 43.6 38.7 34.8 31.7 29.0 26.8 24.9 23.2 21.8 20.5 19.4 18.3 17.4	58.1 49.8 43.6 38.7 34.8 31.7 29.0 26.8 24.9 23.2 21.8 20.4 19.0	0.265 0.414 0.596 0.811 1.059 1.341 1.655 2.003 2.383 2.797 3.244 4.237 4.783 5.363 5.975 6.621
22	30.5		28.8 27.5		27.0 25.8		19.3 18.5		17.8 17.0		16.6 15.8		7.299 8.011
23	27.9	1	26.3		24.7		17.7		16.3		15.2		8.756

CARNEGIE BEAM SECTIONS—Continued

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch

City of Chicago Code

		Nomin	al Depth a	nd Flange	Width-We	ight per Foo	t	
Span		CB 101	10"x6"		(CB 93 9"x	9"	ion
Feet	30 lbs.	26 lbs.	23 lbs.	21 lbs.	48 lbs.	43 lbs.	38 lbs.	Coefficient of Deflection
			erally			Laterally		Coe
	Fixed Free	Fixed Free	Fixed Free	Fixed Free	Fixed Free	Fixed Free	Fixed Free	
	61.0 61.0	52.3 52.3	46.0 46.0	45.6 45.6		0		
10 11 12 13 14	48.6 48.6 42.6 42.6 37.8 37.8 34.0 34.0 30.9 30.9 28.4 28.4 26.2 26.0 24.3 23.7	342.1 42.1 36.8 36.8 32.7 32.7 29.5 29.5 26.8 26.8 24.6 24.6 22.7 22.5 21.1 20.4	32.632.6 $29.029.0$ $26.126.1$ $23.723.7$ $21.721.7$ $20.019.8$ $18.618.1$	33.1 33.1 29.0 29.0 25.8 25.8 23.2 23.2 21.1 21.1 19.3 19.3 17.8 17.7 16.6 16.1	72.9 72.9 63.8 63.8 56.7 56.7 51.0 51.0 46.4 46.4 42.5 42.5 39.3 39.3 36.5 36.5	65.1 65.1 57.2 57.2 50.8 50.8 45.7 45.7 41.6 41.6 38.138.1 32.7 32.7 30.5 30.5	50.550.5 44.944.9 40.440.4 36.736.7 33.733.7 31.131.1	2.383 2.797 3.244
16 17 18 19	21.3 19.9 20.0 18.3 18.9 16.9 17.9 15.7	18.4 17.2 17.3 15.8 16.4 14.6 15.5 13.5	16.3 15.1 15.3 14.0	14.5 13.5 $13.6 12.4 $ $12.9 11.5 $ $12.2 10.6$	31.931.9 30.030.0 28.428.4	28.6 28.6 26.9 26.9 25.4 24.1 22.9 21.8	25.2 25.2	3.724 4.237 4.783 5.363 5.975 6.621 7.299 8.011 8.756

Loads above upper horizontal lines will produce maximum allowable shear in webs.

Loads below lower horizontal lines will produce excessive deflections.

For maximum safe loads, see tables of Maximum Bending Moments and Web Resistances.

CARNEGIE BEAM SECTIONS—Concluded ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch City of Chicago Code

		1	Nominal I	Depth an	d Flang	e Widtl	ı—Wei	ight pe	r Foot		1	
Span				61/2"				CB 83	8"x8			ion
in	35 1	bs.	32 lbs.	29	lbs.	42 1	bs.	36	lbs.	31	lbs.	Coefficient of Deflection
Feet			Laterall	ly				Late	erally			De Co
	Fixed			ee Fixed		Fixed	Free	Fixed	Free	Fixed	Free	
	61.6	61.6	55.9 55	.9 50.2	50.2					1		
6 7			54.9 54			65.2	65.2	55.1	55.1	46.7	46.7	0.596
8		51.5 45.1	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\frac{42.7}{37.3}$	57.0 49.8	57.0 49.8	$\frac{48.8}{42.7}$	$\frac{48.8}{42.7}$	$\frac{41.9}{36.7}$	$\frac{41.9}{36.7}$	0.811 1.059
9 10			$\begin{array}{c c} 36.6 & 36 \\ \hline 33.0 & 33 \end{array}$		33.2 29.9	44.3 39.9	44.3 39.9	$\frac{38.0}{34.2}$	$\frac{38.0}{34.2}$	$\frac{32.6}{29.4}$	$\frac{32.6}{29.4}$	1.341 1.655
$\frac{11}{12}$			$\begin{array}{c c} 30.0 & 30 \\ 27.5 & 27 \end{array}$		$27.2 \\ 24.9$	$\frac{36.2}{33.2}$	$\frac{36.2}{33.2}$	$\frac{31.1}{28.5}$	$\frac{31.1}{28.5}$	$26.7 \\ 24.5$	$26.7 \\ 24.5$	2.003 2.383
13 14	27.8	27.8	25.4 25	4 23.0	23.0	30.7	30.7	26.3	26.3	22.6	$\frac{22.6}{21.0}$	2.797
15			$\begin{bmatrix} 23.5 & 23 \\ 22.0 & 21 \end{bmatrix}$			$\frac{28.5}{26.6}$	$\frac{28.5}{26.6}$	$\frac{24.4}{22.8}$	$\frac{24.4}{22.8}$	$\frac{21.0}{19.6}$	19.6	3.244 3.724
16	22.5		20.6 19		17.8		24.9	21.4		18.3	18.3	4.237
17	21.2	19.9	19.4 18	.2 17.6	16.4	23.5	24.0	20.1	21,4	17,3	. 10.0	4.783
18 19	$\frac{20.0}{19.0}$	18.5	$\frac{18.5}{17.3}$ 17	$0 16.6 \over 15.7$	15.2	22.2		19.0		16.3		5.363 5.975
20	18.0		16.5	14.9		21.0		18.0		10.0		6.621
21	17.2		15.7	14.2								7.299
		1	Nominal 1		d Flang	e Widt	h—We	ight pe	er Foot	t		
Span			CB 82	8"x61/2"			1	*B		'x5½"		ent
in	30	lbs.	27	lbs.	24	lbs.		25 lbs.		21 1	bs.	Coefficient of Deflection
Feet			Late	erally					Latera	lly		Coe
	Fixed	Free	Fixed	Free	Fixed	Free	Fixe			ixed	Free	
3 4							56.		5.6	45.0	45.0	$0.149 \\ 0.265$
5	48.8	48.8	43,4	43.4	38.2	38.2	45.			1.5	41.5	0.414
6	46.8	46.8	42.1	42.1	37.4	37.4	37.	7 37	7.7 3	34.6	34.6	0.596
6 7 8	40.1	$\begin{vmatrix} 40.1 \\ 35.1 \end{vmatrix}$		36.1	$\frac{32.1}{28.1}$	32.1	32.	3 32	2.3 2	29.7	29.7	0.811
9	$\frac{35.1}{31.2}$	31.2		$\begin{vmatrix} 31.6 \\ 28.1 \end{vmatrix}$	$\frac{28.1}{25.0}$	$28.1 \\ 25.0$	28. 25.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		26.0	$\frac{26.0}{23.1}$	1.059 1.341
10	28.1	28.1		25.3	22.5	22,5	22.			20.8	20.8	1.655
11	25.5	25.5		23.0	20.4	20.4	20.		0.6 1	18.9	18.8	2.003
12 13	$\frac{23.4}{21.6}$	23.4	21.0	$\begin{vmatrix} 21.0 \\ 19.4 \end{vmatrix}$	$\frac{18.7}{17.3}$	18.7 17.3	18. 17.			7.3	$16.9 \\ 15.2$	$2.383 \\ 2.797$
14	20.1	19.9	18.0	17.9	16.0	15.9	16.	2 15	5.2 1	4.8	13.8	3.244
15	18.7	18.3	16.8	16.4	15.0	15.6	15.	1 13	3.8 1	3.8	12.6	3.724
16 17	17.5	16.8		15.1	14.0	13.4	14.		2.6	3.0	11.5	4.237
18	16,5 15.6		14.9 14.0		13.2 12.5		13. 12.			2.2	10.5	4.783 5.363
19 20	14.8		13.3		11.8		11.	9		10.9		5.975
							11.			10.4		6.621
21 *Stand	and Mi	II Spoti	1	1			10.	8		9.9		7.299

*Standard Mill Section.

Loads above upper horizontal lines will produce maximum allowable shear in webs.

Loads below lower horizontal lines will produce excessive deflections.

For maximum safe loads, see tables of Maximum Bending Moments and Web Resistances.

STANDARD MILL SECTIONS

ALLOWABLE UNIFORM LOADS IN THOUSANDS OF POUNDS Maximum Bending Stress, 16,000 Pounds per Square Inch City of Chicago Code

	1		Nor	minal I	Depth ar	nd Flan	ge Wie	lth—V	Veight	per Fo	ot		-
Span	-		39 8	8"x5"				I	I 4 8	"x8"			Coefficient of Deflection
in Feet	-	21 lbs.			lbs.	37	7 lbs.		34.3]	bs.	32.6	B lbs.	Coefficient of Deflection
	-	17	Latera		,				Latera	lly			Coe
	Fix	ed F	ree	Fixed	Free	Fixed	Fre	e Fi	xed	Free	Fixed	Free	
	57.		7.6										
3 4	56. 42.		2.3	40.0 39.2	40.0								0.149
5	33.			31.3	39.2 31.3	80.0		THE REAL PROPERTY.	0.0	60.0			0.265 0.414
6	28.	9 90	3.2	26.1	26.1								0.414
7	24.	2 2	1.2	$\frac{20.1}{22.4}$	$\frac{26.1}{22.4}$	53.7 46.0				51.4 44.0	50.1 43.0	43.0	0.596 0.811
8 9	21. 18.	1 21		$19.6 \\ 17.4$	19.6 17.4	40.3	40.	3 38	8.5	38.5	37.6	37.6	1.059
10	16.			15.7	15.7	$\begin{vmatrix} 35.8 \\ 32.2 \end{vmatrix}$	35. 32.	$\begin{array}{c c} 8 & 34 \\ 2 & 30 \end{array}$		34.3	33.4 30.1	33.4 30.1	1.341 1.655
11	15.	4 15	5.3	14.2	14.0	29.3	29.	2 20	3.0	28.0	27.3		
12 13	14. 13.	1 13	3.7	13.1	12.6	26.8	26.	8 28	5.7 2	25.7	25.1	$27.3 \\ 25.1$	2.003 2.383
14	12.	1 11	1.1	$12.1 \\ 11.2$	11.3 10.2	$\frac{24.8}{23.0}$	$\begin{vmatrix} 24. \\ 23. \end{vmatrix}$		$\begin{array}{c c} 3.7 & 2 \\ 2.0 & 3 \end{array}$	$\begin{bmatrix} 23.7 \\ 22.0 \end{bmatrix}$	$\frac{23.1}{21.5}$	$\frac{23.1}{21.5}$	2.797 3.244
15	11.	3 10	0.1	10.4	9.3	21.4	21.			20.6	20.1	20.1	3.724
16	10.		0.2	9.8	8.5	20.1	20.	1 19	0.3	19.3	18.8	18.8	4.237
17 18	10.			9.2 8.7		19.0		1	8.1	-	17.7	10,0	4.783
19	8.			7.5		17.9 15.3			7.1	- 1	16.7		5.363 5,975
	-		NT.	1 17						1			
	-	** - 1			epth an		ge Wid	th—W	eight	per Foo	t		
Span	-	H 3-A	T		-		6"x6"		H 2		"H 1	4"x4"	Coefficient of Deflection
Feet	21.0	lbs.	erally	5 lbs.	22.5	lbs.		lbs.		.9 lbs.		8 lbs.	Coefficient of Deflection
	Fixed	-		l Free	TEX I		rally	(p		terally	-	erally	P P
	Pixeu	1100	FIXEC	1 Free	Fixed	Free	Fixed	Free	Fixed	Free		- 410	
3	52.6	52.6		1	45.0	45.0			31.3	31.3	$\frac{25.0}{18.8}$	$\frac{25.0}{18.8}$	0.149
4 5	43.8 35.0	$\frac{43.8}{35.0}$	37.6	37.6	$\frac{36.5}{29.2}$	36.5	30.0	30.0	25.3	25.3	14.1	14.1	0.265
				1		29.2	27.6	27.6	20.3	20.3	11.3	11.3	0.414
6 7	$\frac{29.2}{25.0}$	$\frac{29.2}{25.0}$	$\frac{27.9}{23.9}$		$24.3 \\ 20.8$	$\frac{24.3}{20.8}$	$\frac{23.0}{19.7}$	$\frac{23.0}{19.7}$	16.9		9.4	9.4	0.596
8	21.9	21.9	20.9	20.9	18.2	18.2	17.2	17.2	$14.5 \\ 12.7$	$14.5 \\ 12.7$	8.1 7.1	8.1 7.1	0.811 1.059
9	$\frac{19.5}{17.5}$	$\frac{19.5}{17.5}$	$\frac{18.6}{16.7}$	$18.6 \\ 16.7$	16.2 14.6	$16.2 \\ 14.6$	15.3 13.8	$15.3 \\ 13.8$	$\frac{11.3}{10.1}$		6.3		1.341
									10.1	10.1	5.7		1.655
11 12	15.9 14.6	15.9 14.6	$15.2 \\ 13.9$	$15.2 \\ 13.9$		$\frac{13.3}{12.2}$	$\frac{12.5}{11.5}$	$\frac{12.5}{11.5}$	9.2		5.1		2.003
13 14	13.5		12.9		11.2		10.6	23.0	7.8				2.383 2.797
15	12.5 11.7		11.9		9.7		9.9						3.244 3.724
					11		0.2						3.724

Loads above upper horizontal lines will produce maximum allowable shear in webs.

Loads below lower horizontal lines will produce excessive deflections.

For maximum safe loads, see tables of Maximum Bending Moments and Web Resistances.

COLUMNS AND STRUTS

A compression member, subjected to longitudinal pressure, is shortened by the compression and also tends to deflect laterally, due to the fact that the load cannot be applied coincident with the longitudinal axis and that the material is not perfectly homogeneous. This flexure occurs generally in the direction of the least resisting moment of the section; the load which will cause a column to fail decreases in the ratio of length to least lateral resistance of the section, the ultimate failure being the result of combined stresses due to compression, transverse shear and flexure.

Column Formulas. Under ideal conditions, when it can be assumed that the load is applied axially and that the material is perfectly homogeneous, the resistance of the column would equal its resistance to compressive forces up to the elastic limit, and there would not be any flexure; if, however, a deflection be imparted to the column by a lateral force, the column would ultimately fail by bending.

Euler's Formula, $P=k\frac{\pi^2 E I}{l^2}$ or $\frac{P}{A}=k\frac{\pi^2 E}{(l/r)^2}$, is based upon the foregoing theory, and gives results close to the ultimate strength found for long and slender struts, when k is a constant varying with the condition of end bearing, (k=4 for columns fixed both ends). For shorter and heavier columns, or for lower ratios of l/r the results do not correspond with actual tests.

Rankine's Formula, $P = \frac{Af}{1+c\;(1/r)^2}$ or $\frac{P}{A} = \frac{f}{1+c\;(1/r)^2}$, represents the type of formula now in general use and the various formulas for proportioning columns which are based upon this general formula agree with actual tests within certain limits. In this formula a certain compressive unit stress for direct crushing is assumed and reduced in ratio of length of column and least radius of gyration, 1/r; value of c is an empirical factor, varying with the resistance of the material and with conditions of end bearing.

Straight Line Formulas. In practice, compression members of a greater ratio of slenderness, 1/r, than 120 are rarely used, and within this limit the curve can be represented by a straight line, the general formula assuming the simpler form: $\frac{P}{A} = f - c \left(\frac{1}{r}\right)$.

Compression formulas determining the resistance of webs in rolled beams or riveted girders against buckling, or the necessary reduction of safe loads due to lateral deflection of unbraced beams, are likewise based on one or the other type of column formulas.

Ratio of Slenderness. 1/r is ratio of the unsupported length of a compression member to its radius of gyration, generally the least radius, excepting when the unsupported length is rigidly braced to prevent deflection in the direction which corresponds to the least radius of gyration. It is, therefore, necessary to determine the radii of gyration and to use the proper ratio of slenderness in every case.

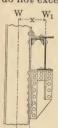
Usual practice limits the maximum ratio of l/r for main members under permanent stress, permitting a higher ratio for secondary members under temporary stress, as in wind bracing.

Compressive Unit Stresses. The tables of allowable loads of column sections have been computed in accordance with the formula for steel columns of the building codes of New York and of Chicago.:

New York: Maximum unit stress at 1/r=0 : 16,000 lb. per sq. inch Maximum l/r: Primary and Secondary members=120.

Chicago: {Maximum unit stress l/r=28.57 : 14,000 lb. per sq. inch. Max.l/r: Primary members=120; Secondary members=150

Combined Bending and Compression Stresses. Generally the loads are concentric and equally distributed over the cross section of the column or balanced on opposite sides thereof. In the case of beams carried on brackets or other forms of eccentric loading, bending stresses are produced which should be taken into consideration and the column sections so proportioned that the combined stresses do not exceed the allowable axial compressive stress.



W = Concentric load. W1=Eccentric load.

M =Bending moment due to eccentric load=W1x.

I -Moment of inertia in direction of bending.

n =Distance from extreme fiber in direction of bending.

A =Area of column section, in square inches.

f =Allowable axial unit stress; f should be equal to or greater than $\frac{W+W_1}{\Lambda} + \frac{Mn}{I}$, the fiber stresses due to compression and bending respectively.

EXAMPLE:—Required a beam column, 23 feet long, to sustain a balanced load of 200,000 pounds and an eccentric load of 28,000 pounds applied 17 inches from the column center on axis 1-1.

Assume Carnegie Beam Section CB-165, 16"x14", 100 lb.

A = 29.41 $I_{1-1} = 1426.8$ $r_{2-2} = 3.53$ 1/r = 23x12 + 3.53 = 78.2

Actual fiber stress = $\frac{200,000+28,000}{29.41} + \frac{28,000x17x8}{1426.8} = 10,424$ pounds.

This stress is within the limits of the allowable fiber stress for ratio of 1/r = 78.2, 10,526 pounds, obtained from the column formula.

ALLOWABLE UNIT STRESSES IN POUNDS PER SQUARE INCH

by Compression Formula of New York Building Law: 16000—70 $\frac{1}{r}$

The following tables give the unit stresses for ratios of 1/r in intervals of 5/10. Intermediate values may be found by interpolation from the figures given for the tenth units of 1/r by adding or deducting from the nearest tabulated figure the corresponding multiple.

Example: Unit stress for 1/r=38.2 and 1/r=112.8 1/r=38.2 13305+21 or 13340-14=13326 1/r=112.8 8090+14 or 8125-21=8104

MAIN AND SECONDARY MEMBERS-Ratios of 1/r up to 120

STATE AND SECONDARY MANAGEMENT AND SECONDARY M													
Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10		
	1.0000		1.5	14950		30	13900	1	45	12850			
0	16000			14930		.5	13865			12815			
.5	15965		.5 16	14880		31	13830		46	12780			
1	15930		.5	14845		.5	13795		.5	12745			
.5	15895		17	14810		32	13760		47	12710			
2	15860		.5	14775		.5	13725		.5	12675			
.5	15825 15790		18	14740		33	13690		48	12640			
.5	15755		.5	14705		.5	13655		.5	12605			
4	15720		19	14670		34	13620		49	12570			
.5	15685		.5	14635		.5	13585		.5	12535			
5	15650		20	14600		35	13550		50	12500			
.5	15615		.5	14565		.5	13515		.5	12465			
6	15580		21	14530		36	13480		51	12430			
.5	15545		.5	14495		.5	13445		.5	12395			
7	15510		22	14460		37	13410		52	12360			
.5	15475	7	.5	14425	7	.5	13375	7	.5	12325	7		
8	15440		23	14390		38	13340		53	12290			
.5	15405		.5	14355		.5	13305		.5	12255			
9	15370		24	14320		39	13270		54	12220			
.5	15335		.5	14285		.5	13235	1	.5	12185			
10	15300		25	14250		40	13200		55	12150			
.5	15265		.5	14215		.5	13165		.5	12115			
11	15230		26	14180		41	13130		56	12080			
.5	15195		.5	14145		.5	13095	1		12045			
12	15160		27	14110		42	13060		57	12010			
.5			.5	14075		.5		1	Al.	11975			
13	15090		28	14040		43	12990	1	58	11940			
.5	15055		.5	14005		.5	12955			11905	1		
14	15020		29	13970		44	12920		59	11870			
.5	14985		.5	13935			12885			11835			
15	14950		30	13900		45	12850) [60	11800	1		

ALLOWABLE UNIT STRESSES IN POUNDS PER SQUARE INCH

by Compression Formula of New York Building Law: 16000—70 $\frac{1}{r}$

MAIN AND SECONDARY MEMBERS-Ratios of 1/r up to 120

	Unit	1	1	Unit		II	TT 1		1	77 1	
Ratio,	Stress.	Diff.	Ratio,	Stress,	Diff.	Ratio,	Unit Stress,	Diff.	Ratio,	Unit Stress,	Diff.
1/r	Pounds	0.10	1/r	Pounds	0.10	1/r	Pounds	0.10	l/r	Pounds	0.10
0.0	11000										
60	11800		75	10750		90	9700		105	8650	
.5	11765		.5	10715		.5	9665		.5	8615	
61	11730		76	10680		91	9630		106	8580	
.5	11695		.5	10645		.5	9595		.5	8545	
62	11660		77	10610		92	9560		107	8510	
.5	11625		.5	10575		.5	9525		.5	8475	
63	11590		78	10540	-	93	9490		108	8440	
.5	11555		.5	10505		.5	9455		.5	8405	
64	11520		79	10470		94	9420		109	8370	
.5	11485		.5	10435		.5	9385		.5	8335	
65	11450		80	10400		95	9350		110	8300	
.5	11415		.5	10365		.5	9315		.5	8265	
66	11380	1	81	10330		96	9280		111	8230	
.5	11345		.5	10295		.5	9245	1	.5	8195	
67	11310		82	10260		97	9210		112	8160	
.5	11275	7	.5	10225	7	.5	9175	7	.5	8125	7
68	11240		83	10190		98	9140		113	8090	
.5	11205		.5	10155		.5	9105		.5	8055	
69	11170		84	10120	0 8	99	9070		114	8020	
.5	11135		.5	10085		.5	9035		.5	7985	
70	11100		85	10050		100	9000		115	7950	
.5	11065			10015		.5	8965		.5	7915	
71	11030		86	9980		101	8930		116	7880	
.5	10995		.5	9945		.5	8895		.5	7845	
72	10960		87	9910		102	8860		117	7810	
	10925		.5	9875		.5	8825		.5	7775	
73	10890		88	9840		103	8790		118	7740	
	10855		.5	9805		.5	8755		.5	7705	
	10820		89	9770		104	8720		119	7670	
	10785		.5	9735		.5	8685		.5	7635	
75	10750	-	90	9700		105	8650		120	7600	
		- 30		1							

CARNEGIE BEAM SECTIONS

18-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

	1		Nominal	Depth ar	nd Flange	Width-	Weight p	er Foot		
Effective Length	СВ	183 18"	x12"	CB 1	.82 18"x	81/2"		CB 181	18"x7½"	,
in Feet	100 lbs.	93 lbs	786 1bs.	78 lbs.	72 1bs.	67 lbs.	58 lbs.	52 1bs.	51 lbs.	47 lbs.
1 2 3 4 5	462 454 445 437 428	430 422 414 406 398	397 390 383 375 368	357 348 338 328 319	330 321 312 303 294	307 298 290 282 273	264 256 248 239 231	237 230 222 214 207	232 225 217 209 202	214 207 200 193 186
6 7 8 9	420 412 403 395 386	390 383 375 367 359	361 354 346 339 332	309 299 290 280 270	285 276 267 258 249	265 256 248 240 231	222 214 205 197 189	199 191 184 176 168	194 186 179 171 163	180 173 166 159 152
11 12 13 14 15	378 369 361 353 344	351 343 335 328 320	324 317 310 302 295	261 251 241 231 222	240 231 222 213 204	223 214 206 198 189	180 172 163 155 146	161 153 145 138 130	155 148 140 132 125	145 138 131 124 117
16 17 18 19 20	336 327 319 311 302	312 304 296 288 281	288 281 273 266 259	212 202 193 183	195 186 177 168	181 172 164 156	138 130	122	117	110
21 22 23 24 25	294 285 277 268 260	273 265 257 249 241	251 244 237 229 222				•			
26 27 28 29	252 243 235 226	233 226 218 210	215 208 200 193							
Area, in.2	29.40	27.35	25.29	22.94	21.17	19.69	17.05	15.30	15.00	13.82
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	1783.4 7.79 253.4 2.94	1648.4 7.76 234.0 2.93	1514.1 7.74 214.7 2.91	1318.8 7.58 90.9 1.99	1208.1 7.55 82.9 1.98	1117.1 7.53 76.4 1.97	960.8 7.51 49.0 1.70	855.1 7.48 43.3 1.68	810.0 7.35 40.5 1.64	768.6 7.46 38.7 1.67
Weight Lbs. per Foot	100	93	86	78	72	67	58	52	51	47

Safe load values above are for ratios of I/r not over 120, for both main and secondary members.

So-

CARNEGIE BEAM SECTIONS—Continued

16-INCH COLUMNS

Allowable Concentric Loads in Thousands of Pounds

Unit Stress-City of New York Code

				No	minal	Depth	and l	Flange	Widt	h—V	Veigh	t pe	r Foo	t	-	
Effectiv Length in Feet		CB 16"x			CB :	164		CB 1 16"x8	163				162			3 161 "x6"
	lbs						68 1bs					45 bs.	43 1bs.	40 lbs		35 lbs.
1 2 3 4 5	53 52 51 50 50	5 48 7 48 9 47	38 45 31 45 4 44	$ \begin{array}{c c} 7 & 40 \\ 0 & 40 \\ 3 & 39 \end{array} $	8 37 1 37 3 36	7 345 0 338 3 332	30. 29. 2 28	$\begin{array}{ccc} 3 & 28 \\ 5 & 27 \\ 7 & 26 \end{array}$	$ \begin{array}{ccc} 1 & 25 \\ 3 & 25 \\ 5 & 24 \end{array} $	$ \begin{array}{c c} 9 & 2 \\ 1 & 2 \\ 4 & 2 \end{array} $	$ \begin{array}{cccc} 20 & 1 \\ 12 & 1 \\ 05 & 1 \end{array} $	205 198 191 184 177	188 183	8 17 1 16 4 16	6 16 9 15 3 15	4 151 7 145 0 138
6 7 8 9 10	49 48 47 46 46	5 45 7 44 9 43	1 42: 4 41: 6 408	37 36 36 35	1 34: 3 33: 6 32:	2 312 5 306 8 300	262 253 243	2 24 3 23 5 22	$ \begin{array}{cccc} 2 & 22 \\ 4 & 21 \\ 7 & 20 \end{array} $	3 1; 5 1; 8 10	89 1 82 1 74 1 66 1	.70 .63 .56 49		15 3 14 5 13 9 13	1 136 5 129 8 121 2 114	125 118 111 105
11 12 13 14 15	453 443 433 429 421	41- 40- 399	4 387 6 380 9 373	333 323 318	3 303 3 300 3 293	$7280 \\ 274 \\ 267$		$ \begin{array}{c c} 203 \\ 196 \\ 188 \end{array} $	3 187 3 180 8 173	14 13 12 12	13 1 35 1 28 1	35 28 21 14 07	125 118 111 104 97	120 114 107 101	0 100 4 93 7 86	92
16 17 18 19 20	413 405 397 389 381	376 369 362	352 345 2 338	295	$ \begin{array}{r} 272 \\ 265 \\ 258 \\ \end{array} $	248 242 235	187 179 170 162 154	$165 \\ 157 \\ 149$	151 144 137	11		01				
21 22 23 24 25	373 365 357 349 341	339	317 310 303	265 258 250 243 235	$ \begin{array}{r} 237 \\ 230 \\ 223 \end{array} $	$ \begin{array}{r} 216 \\ 210 \\ 203 \end{array} $						1				
26 28 30 32 34	333 317 301 285 269	$\frac{294}{279}$ $\frac{264}{264}$	275 261 247	227 212	209 195											
			29.41	26.46	24.41	22.34	20.00	18.52	17.06	14.7	0 13.2	23 1	2.65	11.75	11.17	10.29
I ₂₋₂ , in.4	7.02	6.99	1426.8 6.97 366.0 3.53	1275.5 6.94	1167.7 6.92	1061.3 6.89 191.1	923.7 6.80 81.3 2.02	849.9 6.77 74.6 2.01	776.6 6.75 68.0 2.00	666. 6.73 38.2 1.61	595 6.7	.0 5 1 6 0 2	23.8 .44 8.9	524.6 6.68 29.8 1.59	475.1 6.52	435.5 6.50 17.5 1.30
Foot	115	107	100	90	83	76 f l/r no	68	63	58	50	45		43	40	38	35

CARNEGIE BEAM SECTIONS—Continued

14-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

			Nominal	Depth a	nd Flange	e Width-	-Weight	per Foot		
Effective Length					CB 146	14"x15"	,			
in Feet	305	295	285	275	265	255	245	235	225	215
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
1	1417	1371	1324	1277	1231	1184	1138	1091	1045	998
2	1399	1353	1307	1261	1215	1169	1123	1077	1031	985
3	1381	1335	1290	1244	1199	1154	1108	1063	1017	972
4	1362	1318	1273	1228	1183	1138	1093	1048	1004	959
5	1344	1300	1256	1211	1167	1123	1079	1034	990	946
6	1326	1282	1239	1195	1151	1107	1064	1020	976	933
7	1308	1265	1221	1178	1135	1092	1049	1005	962	919
8	1290	1247	1204	1161	1119	1076	1034	991	949	906
9	1271	1229	1187	1145	1103	1061	1019	977	935	893
10	1253	1212	1170	1128	1087	1045	1004	962	921	880
11 12 13 14 15	$\begin{array}{c} 1235 \\ 1217 \\ 1199 \\ 1180 \\ 1162 \end{array}$	1194 1176 1159 1141 1123	1153 1136 1119 1102 1085	1112 1095 1079 1062 1045	$1071 \\ 1055 \\ 1039 \\ 1023 \\ 1007$	1030 1015 999 984 968	989 974 959 944 930	948 934 919 905 891	907 894 880 866 852	867 853 840 827 814
16	1144	1106	1068	1029	991	953	915	876	839	801
17	1126	1088	1051	1012	975	937	900	862	825	787
18	1108	1071	1034	996	959	922	885	848	811	774
19	1089	1053	1016	979	943	906	870	833	797	761
20	1071	1035	999	963	927	891	855	819	784	748
22	1035	1000	965	929	895	860	825	790	756	721
24	998	965	931	896	863	829	796	762	729	695
26	962	929	897	863	831	798	766	733	701	669
28	926	894	863	830	799	768	736	704	673	642
30	889	859	828	797	767	737	706	676	646	616
32	853	823	794	764	735	706	676	647	618	589
34	816	788	760	731	703	675	647	618	591	563
36	780	753	726	697	671	644	617	590	563	537
38	744	718	692	664	639	613	587	561	536	510
40	707	682	658	631	607	582	557	532	508	484
Area, in.2	89.70	86.76	83.82	80.87	77.93	74.99	72.06	69.11	66.17	63.23
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	4121.5	3948.1	3778.1	3607.8	3442.4	3280.0	3119.6	2961.9	2806.2	2654.7
	6.78	6.75	6.71	6.68	6.65	6.61	6.58	6.55	6.51	6.48
	1539.1	1479.4	1420.7	1362.0	1304.2	1247.1	1190.6	1134.5	1079.1	1024.5
	4.14	4.13	4.12	4.10	4.09	4.08	4.06	4.05	4.04	4.03
Weight Lbs. per Foot	305	295	285	275	265	255	245	235	225	215

CARNEGIE BEAM SECTIONS—Continued

14-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

			Nom	inal Dep	oth and l	Flange V	Vidth-V	Weight p	er Foot		
Effectiv Length	1				CB	146 14	4"x15"				
in Feet	205	195	185	175	165	155	145	135	131	125	115
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	Ibs.	lbs.	lbs.	lbs.	lbs.
1	952	905	859	813	766	720	673	627	608	580	534
2	939	893	848	802	756	710	664	618	599	572	527
3	927	881	836	791	745	700	655	610	591	564	519
4	914	869	825	780	735	690	646	601	582	556	512
5	901	857	813	769	725	681	637	593	573	548	505
6	889	845	802	758	715	671	628	584	565	541	497
7	876	833	790	747	704	661	618	576	556	523	490
8	863	821	779	736	694	652	609	567	548	525	483
9	851	809	767	726	684	642	600	559	539	517	475
10	838	797	756	715	673	632	591	550	530	509	468
11	826	785	744	704	663	622	582	542	522	501	461
12	813	773	733	693	653	613	573	533	513	493	453
13	800	761	721	682	643	603	564	524	505	485	446
14	788	749	710	671	632	593	555	516	496	477	439
15	775	737	699	660	622	584	546	507	488	469	432
16	762	725	687	649	612	574	536	499	479	461	424
17	750	713	676	638	601	564	527	490	470	453	417
18	737	701	664	627	591	554	518	482	462	446	410
19	725	689	653	617	581	545	509	473	453	438	402
20	712	677	641	606	570	535	500	465	445	430	395
22	687	653	618	584	550	515	482	448	428	414	380
24	661	628	595	562	529	496	464	431	410	398	366
26	636	604	572	540	509	477	445	414	393	382	351
28	611	580	549	519	488	457	427	397	376	366	337
30	586	556	526	497	468	438	409	380	359	351	322
32 34 36 38 40	560 535 510 485 459	532 508 481 460 436	504 481 458 435	475 453 431 410	447 426 406 385	418 399 379 360	391 372 354 336	363 346 329 312	342 325 307	335 319 303 287	307 293 278 264
Area, in.2	60.28	57.34	54.41	51.47	48.52	45.58	42.64	39.70	38.52	36.75	33.82
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	2505.0	2358.2	2213.5	2071.7	1932.6	1796.8	1662.7	1530.4	1358.4	1402.1	1275.9
	6.45	6.41	6.38	6.34	6.31	6.28	6.24	6.21	5.94	6.18	6.14
	970.3	916.8	863.9	811.6	759.9	709.0	658.5	608.4	547.3	559.4	510.9
	4.01	4.00	3.98	3.97	3.96	3.94	3.93	3.92	3.77	3.90	3.89
Weight Lbs. per Foot	205	195	185	175	165	155	145	135	131	125	115

CARNEGIE BEAM SECTIONS—Continued

14-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

				Nomi	nal De	pth a	nd Fla	nge W	idth-	-Weigh	at per	Foot			
Effective Length		CB 145 4"x12"			B 144			CB 143 14"x8"		(CB 14	2 14'	'x63/4'	,	CB 141 14"x6"
in Feet	105 lbs.	95 lbs.	85 lbs.	75 lbs.	68 lbs.	61 lbs.	58 lbs.	53 Ibs.	48 Ibs.	42 lbs.	39 lbs.	38 lbs.	36 lbs.	33 lbs.	30 lbs.
1 2 3 4 5	486 477 469 460 452	439 432 424 416 409	393 386 379 372 365	345 338 330 323 315	313 306 299 293 286	281 275 269 262 256	265 258 250 243 236	236 229 222	220 213 207 201 195	191 184 178 171 164	177 171 165 159 153	172 166 160 153 147	164 158 152 146 141	150 145 139 134 129	136 130 124 119 113
6 7 8 9 10	444 435 427 418 410	401 393 386 378 370	359 352 345 338 331	308 300 293 285 278	279 272 265 258 252	250 244 238 231 225	228 221 213 206 198	208 201 195 188 181	188 182 176 170 163	158 151 144 138 131	146 140 134 128 122	$\frac{134}{128}$ $\frac{121}{121}$	135 129 128 118 112	124 118 113 168 102	108 102 97 91 85
11 12 13 14 15	401 393 385 376 368	363 355 347 340 332	324 317 310 303 297	270 263 255 248 240	245 238 231 224 217	219 213 207 201 194	191 183 176 168 161		157 151 145 139 132	124 118 111 105 98	116 109 103 97 91	109 102 96 89	106 100 95 89 83	97 92 87 81 76	80 74 69
16 17 18 19 20	359 351 342 334 326	$\frac{317}{309}$ $\frac{301}{301}$	290 283 276 269 262	233 225 218 210 203	211 204 197 190 183	188 182 176 170 164	153 146 139 131	133	$\frac{120}{114}$,				
21 22 23 24 25	317 309 300 292 284	$\frac{271}{263}$	255 248 242 235 228	195 188 180 173	$\frac{170}{163}$	145									
26 27 28 29 30	275 267 258 250 241	$\frac{240}{232}$	214												
Area, in.2	30.88	27.93	24.99	22.05	19.99	17.94	17.05	15.59	14.12	12.35	11.47	11.18	10.58	9.71	8.82
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	6.15	6.11	6.07	823.5 6.11 134.5 2.47	6.08	656.2 6.05 107.1 2.44	609.4 5.98 62.8 1.92	552.5 5.95 56.8 1.91	496.0 5.93 50.8 1.90	431.5 5.91 30.2 1.56	398.3 5.89 27.7 1.56	357.5 5.66 24.2 1.47	365.6 5.88 25.4 1.55	333.4 5.86 23.0 1.54	292.0 5.75 15.5 1.33
Weight Lbs. per Foot	105	95	85	75	68	61	58	53	48	42	39	38	36	33	30

CARNEGIE BEAM SECTIONS—Continued

12-INCH COLUMNS

Allowable Concentric Loads in Thousands of Pounds

Unit Stress-City of New York Code

73.00				Nomin	al Dept	h and	Plange	Width-	-Weigh	t per F	oot		
Effective Length		CB	127 13	2"x14"			CB 126	12"x	14''	1	B 125	12"x	12''
in Feet	230	220	210	200	190	180	170	160	150	140	130	120	110
	lbs.	lbs.	lbs.	lbs.	lbs.								
1	1067		974	928	881	835	788	742	696	647	601	555	509
2	1052		960	914	869	823	777	731	686	636	591	545	500
3	1037		946	901	856	810	765	721	676	624	580	535	491
4	1021		932	888	843	798	754	710	666	613	569	526	482
5	1006		918	875	831	786	742	699	656	601	559	516	474
6	991	948	904	861	818	774	731	688	646	590	548	506	465
7	976	933	891	848	806	762	719	678	636	578	538	497	456
8	961	919	877	835	793	749	708	667	626	567	527	487	447
9	946	904	863	821	780	737	696	656	616	555	516	477	438
10	930	889	849	808	768	725	685	645	605	544	506	468	430
11	915	875	835	795	755	713	673	634	595	532	495	458	421
12	900	860	821	781	742	700	662	624	585	521	485	448	412
13	885	846	807	768	730	688	650	613	575	509	474	439	403
14	870	831	793	755	717	676	639	602	565	498	463	429	395
15	854	817	779	741	704	664	627	591	555	486	453	419	386
16	839	802	765	728	692	652	616	581	545	475	442	410	377
17	824	788	751	715	679	639	604	570	535	464	432	400	368
18	809	773	737	701	666	627	593	559	525	452	421	390	359
19	794	758	723	688	654	615	581	548	515	441	410	380	351
20	778	744	709	675	641	603	570	538	505	429	400	371	342
22	748	715	681	648	616	578	547	516	486	406	379	351	324
24	718	686	653	621	590	554	524	494	465	383	357	332	307
26	687	656	626	595	565	529	501	473	445	360	336	313	289
28	657	627	598	568	540	505	478	451	425	337	315	293	272
30	626	598	570	542	515	481	455	430	405	314	294	274	254
32 34 36	596 566 535	569 540 511	542 514 486	515 488 462	489 464 439	456 432 407	432 409 386	408 387 365	385 364 344			·	
Area,in.2	67.64	64.70	61.76	58.82	55.88	52.94	50.00	47.06	44.12	41.18	38.24	35.28	32.34
I ₁₋₁ , in. ⁴	1461.9	1426.6	1391.3	1356.1	1320.8	1218.1	1182.8	1147.5	1112.2	934.8	899.5	864.1	828.8
r ₁₋₁ , in.	4.65	4.70	4.75	4.80	4.86	4.80	4.86	4.94	5.02	4.76	4.85	4.95	5.06
I ₂₋₂ , in. ⁴	945.5	898.2	852.9	809.5	767.8	702.4	666.9	633.0	600.4	372.4	350.5	329.6	309.9
r ₂₋₂ , in.	3.74	3.73	3.72	3.71	3.71	3.64	3.65	3.67	3.69	3.01	3.03	3.06	3.10
Weight Lbs. per Foot Safe loa	230	220	210	200	190	180	170	160	150	140	130	120	110

CARNEGIE BEAM SECTIONS—Continued

12-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

			Nom	inal De	pth and	Flange	Width	-Weigh	t per F	oot		
Effective Length	CB	124 1	2"x10"		CB 1	23 12'	'x8"	CF	3 122	12"x6½	"	CB 121 12"x6"
in Feet	100 lbs.	91 lbs.	83 1bs.	75 lbs.	50 lbs.	45 lbs.	40 lbs.	36 lbs.	34 lbs.	32 lbs.	28 lbs.	25 lbs.
1 2 3 4 5	460 450 440 429 419	419 410 400 391 382	382 374 365 357 349	345 338 331 323 316	229 223 216 210 204	206 200 195 189 183	183 178 173 168 163	164 158 152 146 141	154 148 142 137 131	145 140 135 130 125	127 122 118 113 109	113 108 104 99 95
6 7 8 9 10	409 398 388 378 367	372 363 354 344 335	340 331 324 315 307	309 301 294 286 279	198 191 185 179 173	178 172 167 161 155	158 153 148 143 138	135 129 124 118 112	125 119 114 108 102	120 115 109 104 99	104 100 95 91 86	90 86 81 77 72
11 12 13 14 15	357 347 336 326 316	326 316 307 298 288	298 290 282 273 265	272 264 257 249 242	166 160 154 148 142	150 144 138 133 127	133 128 122 117 112	106 101 95 89 83	96 90 85 79	94 89 84 79 73	82 77 73 68, 64	68 63 59
16 17 18 19 20	305 295 285 274 264	279 270 260 251 242	257 248 240 232 223	235 227 220 213 205	135 129 123 117	121 116 110 104	107 102 97 92					
21 22 23 24 25	253 243 233	232 223 214 204	215 206 198 190	198 190 183 176 168								
Area, in.	29.41	26.76	24.41	22.05	14.69	13.23	11.76	10.59	9.99	9.40	8.22	7.34
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	659.0 4.73 167.5 2.39	627.2 4.84 155.9 2.41	598.9 4.95 147.0 2.45	570.7 5.09 138.5 2.51	400.5 5.22 57.5 1.98	356.9 5.19 51.2 1.97	313.7 5.17 44.9 1.95	280.1 5.14 25.4 1.55	238.1 4.88 21.0 1.45	246.3 5.12 22.3 1.54	213.4 5.10 19.2 1.53	183.0 4.99 13.8 1.37
Weight Lbs. per Foot	100	91	83	75	50	45	40	36	34	32	28	25

CARNEGIE BEAM SECTIONS—Continued

10-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

77.00]	Nomina	l Depti	h and F	lange V	Width-	Weigh	t per F	oot		
Effective Length		(CB 105	10"x1	2"		1	CB 104	10''x	10"	CB	103 1	0"x9"
in Feet	140	132	124	116	108	100	92	84	77	70	63	56	49
	lbs.	1bs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
1	647	610	574	537	500	463	424	387	355	323	289	257	225
2	636	600	564	527	491	455	415	378	347	316	282	251	220
3	625	589	554	518	483	447	406	370	340	309	275	245	215
4.	614	579	544	509	474	439	397	362	332	302	267	238	209
5	603	568	534	500	466	431	387	353	325	296	260	232	204
6	591	558	524	491	457	424	378	345	317	289	253	226	199
7	580	547	514	481	449	416	369	337	309	282	246	220	193
8	569	537	504	472	440	408	360	328	302	275	239	213	188
9	558	526	494	463	432	400	351	320	294	268	231	207	183
10	.546	516	484	454	423	392	342	312	287	262	224	201	177
11	535	505	474	445	415	385	333	303	279	255	216	194	172
12	524	494	465	435	406	377	324	295	271	248	209	188	167
13	513	484	455	426	397	369	315	286	264	241	202	182	161
14	502	473	445	417	389	361	306	278	256	234	195	175	156
15	490	463	435	408	380	353	297	270	249	228	187	169	151
16	479	452	$\begin{array}{c} 425 \\ 415 \\ 405 \\ 395 \\ 385 \end{array}$	399	372	345	287	261	241	221	180	163	145
17	468	442		389	363	338	278	253	234	214	173	157	140
18	457	431		380	355	330	269	245	226	207	166	150	135
19	445	421		371	346	322	260	236	218	201	158	144	129
20	434	410		362	338	314	251	228	211	194	151	138	124
21 22 23 24 25	423 412 400 389 378	399 389 378 368 357	375 365 355 346 336	352 343 334 325 316	329 321 312 304 295	306 299 291 283 275	242 233 224 215 206	220 211 203 194	203 196 188 180 173	187 180 173 167 160	144	131 125	119 113
26 27 28 29 30	367 356 344 333 322	347 336 326 315 304	326 316 306 296 286	306 297 288 279 269	287 278 270 261 253	267 259 252 244 236							
Area, in.2	41.17	38.81	36.46	34.11	31.76	29.40	27.06	24.70	22.65	20.59	18.53	16.47	14.41
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	623.2	603.5	583.9	564.3	544.8	525.1	423.2	403.6	386.5	369.3	300.4	283.2	266.0
	3.89	3.94	4.00	4.07	4.14	4.23	3.96	4.04	4.13	4.24	4.03	4.15	4.30
	391.4	369.6	349.0	329.4	310.7	292.8	163.1	152.0	142.9	134.3	85.2	79.5	74.2
	3.08	3.09	3.09	3.11	3.13	3.16	2.50	2.48	2.51	2.55	2.14	2.20	2.27
Weight Lbs. per Foot Safe loa	140	132	124	116	108	100	92	84	77	70	63	56	49

CARNEGIE BEAM SECTIONS—Continued

10 AND 9-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

			N	ominal	Depth	and Fla	inge W	idth—\	Veight	per Foo	ot		
Effective Length	CB 1	.02 10	"x8"	C	B 101	10''x6	"	СВ	93 9"	x9"	CB 9	2 9"x	6½"
in Feet	42 lbs.	36 lbs.	31 lbs.	30 1bs.	26 lbs.	23 lbs.	21 lbs.	48 1bs.	43 lbs.	38 1bs.	35 lbs.	32 lbs.	29 Ibs.
1 2 3 4 5	192 186 180 174 168	164 159 154 150 145	142 138 134 130 126	136 131 126 121 116	118 113 109 104 100	104 100 96 92 88	95 91 88 84 80	$\begin{array}{c} 221 \\ 215 \\ 210 \\ 205 \\ 200 \end{array}$	198 193 188 184 179	175 170 166 162 158	159 154 149 143 138	145 141 136 131 126	132 127 123 118 114
6 7 8 9 10	162 156 150 144 138	$140 \\ 135 \\ 130 \\ 125 \\ 120$	121 117 113 109 105	110 105 100 95 90	95 91 86 82 77	84 80 76 72 68	76 73 69 65 61	195 190 184 179 174	174 170 165 160 156	154 150 146 141 137	132 127 122 116 111	121 116 111 106 101	109 105 100 96 91
11 12 13 14 15	132 126 120 114 108	115 110 105 100 95	101 97 93 89 85	85 80 75 70	73 68 64 59	64 61 57 53	58 54 50	169 164 158 153 148	151 146 142 137 132	133 129 125 121 116	106 100 95 89 84	96 91 86 81 76	87 82 78 73 69
16 17 18 19 20	102 96	90 85 80	81 77 73					143 138 133 127 122	128 123 118 114 109	112 108 104 100 96	79	71	
21 22								117 112	104 100	92 87			
Area, in.2	12.35	10.58	9.11	8.82	7.64	6.76	6.17	14.11	12.65	11.17	10.29	9.40	8.53
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	190.4 3.93 36.8 1.73	175.6 4.07 34.4 1.80	163.4 4.23 32.5 1.89	163.2 4.30 18.5 1.45	139.5 4.27 15.7 1.43	122.2 4.25 13.7 1.43	107.6 4.18 12.0 1.39	221.1 3.96 73.8 2.29	195.5 3.93 65.4 2.28	170.4 3.91 57.1 2.26	155.4 3.89 26.6 1.61	140.5 3.87 24.0 1.60	126.0 3.84 21.5 1.59
Weight Lbs. per Foot	42	36	31	30	26	23	21	48	43	38	35	32	29

CARNEGIE BEAM SECTIONS—Concluded

8-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

				Nomin	al Dep	oth and	Flang	e Wid	thW	eight p	er Foo	t		
Effective Length					СВ	83 8	"x8"					CB8	2 8"x	6½"
in Feet	90	84	78	72	66	60	54	48	42	36	31	30	27	24
	lbs.	lbs.	lbs	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lts.	1bs.	lbs.
1	413	386	358	330	303	275	247	220	192	165	142	136	123	109
2	403	376	349	322	295	268	241	214	187	160	138	132	119	106
3	393	366	340	314	287	261	235	208	182	156	134	127	115	102
4	383	357	331	305	280	254	228	203	177	152	130	123	110	98
5	372	347	322	297	272	247	222	197	172	147	127	118	106	95
6	362	337	313 304 295 286 277	288	264	240	215	191	167	143	123	114	102	91
7	352	328		280	256	232	209	185	162	138	119	109	98	87
8	342	318		272	249	225	202	180	157	134	115	105	94	83
9	331	308		263	241	218	196	174	152	130	111	100	90	80
10	321	299		255	233	211	190	168	147	125	108	96	86	76
11	311	289 280 270 260 251	268	246	225	204	183	162	142	121	104	91	82	72
12	301		259	238	218	197	177	157	136	116	100	86	78	69
13	290		250	230	210	190	170	151	131	112	96	82	73	65
14	280		241	221	202	183	164	145	126	108	92	77	69	61
15	270		232	213	195	176	157	139	121	103	89	73	65	58
16 17 18 19 20	260 249 239 229 219 208	241 231 222 212 202 193	223 214 205 196 187	205 196 188 179 171 163	187 179 171 164 156	169 162 155 147 140	151 144 138 132 125	134 128 122 116 111	116 111 106 101 96	99 94 90 86 81	85 81 77 73 70	68	61	54
Area, in.2	26.47	24.71	22.93	21.17	19.40	17.63	15.87	14.10	12.34	10.58	9.10	8.81	7.93	7.06
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	391.2	358.6	326.5	295.9	265.9	237.1	209.2	182.2	156.2	131.3	110.9	107.8	95.9	84.3
	3.84	3.81	3.77	3.74	3.70	3.67	3.63	3.59	3.56	3.52	3.49	3.50	3.48	3.46
	124.4	114.5	104.7	95.3	86.1	77.1	68.3	59.7	51.4	43.4	36.7	23.4	20.8	18.3
	2.17	2.15	2.14	2.12	2.11	2.09	2.07	2.06	2.04	2.02	2.01	1.63	1.62	1.61
Weight Lbs. per Foot	90	84	78	72	66	60	54	48	42	36	31	30	27	24

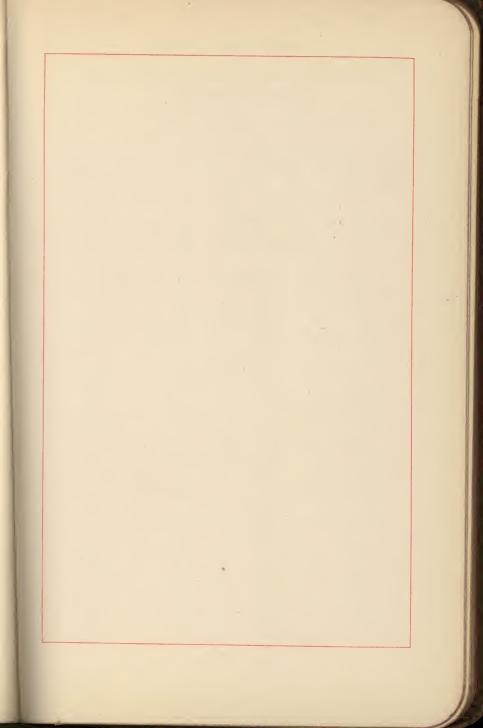
· STANDARD MILL SECTIONS

MISCELLANEOUS SMALL COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of New York Code

			N	ominal	Denth	and Fla	ange W	idth—I	Veight	per Foo	ot		
Effective Length	B 4		В	39	Н			H 3	A	H 6"2	3	H 2 5"x5"	H 1 4"x4"
in Feet	25 lbs.	21 lbs.	21 lbs.	18 lbs.	37.7 lbs.	34.3 lbs.	32.6 lbs.	27.5 lbs.	25 lbs.	22.5 lbs.	20 lbs.	18.9 lbs.	10.8 lbs.
1 2 3 4 5	112 106 100 95 89	94 90 85 81 76	94 89 84 79 74	80 76 72 68 64	171 166 161 156 151	156 151 147 142 138	148 144 139 135 131	124 120 115 110 105	113 109 104 100 96	102 98 94 89 85	90 87 83 80 76	84 80 76 72 68	60 57 53 50 46
6 7 8 9 10	84 78 72 67 61	71 67 62 58 53	69 63 58 53 48	60 56 51 47 43	146 141 136 131 126	133 129 124 120 115	127 123 118 114 110	100 96 91 86 81	91 87 83 - 79 74	81 77 73 69 65	73 69 65 62 58	65 61 57 53 49	43 39 36 32
11 12 13 14 15		49			120 115 110 105 100	111 106 102 97 93	106 102 97 93 89	76 72 67 62	70 66 61 57	61 57 53	55 51 48	45 42	
16 17 18 19					95 90 85	88 84 79	85 81 76 72						
Area, in.2	7.34	6.17	6.17	5.29	11.00	10.00	9.50	8.08	7.33	6.61	5.86	5.47	3.99
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	95.5 3.61 8.8 1.09	87.6 3.77 8.1 1.14	63.4 3.21 6.6 1.03	58.7 3.33 6.1 1.07	120.8 3.31 36.9 1.83	115.5 3.40 35.1 1.87	112.8 3.45 34.2 1.90	49.3 2.47 16.0 1.41	47.0 2.53 14.9 1.43	41.0 2.49 12.2 1.36	38.8 2.57 11.4 1.39	23.8 2.08 7.8 1.20	10.7 1.64 3.6 0.95
Weight Lbs. per Foot	25	21	21	18	37.7	34.3	32.6	27.5	25	22.5	20	18.9	13.8



ALLOWABLE UNIT STRESSES IN POUNDS PER SQUARE INCH

by Compression Formula of

Chicago Building Law: 16000-70 $\frac{1}{r}$

The following tables give the unit stresses for ratios of l/r in intervals of 5/10. Intermediate values may be found by interpolation from the figures given for the tenth units of l/r by adding or deducting from the nearest tabulated figure the corresponding multiple.

Example: Unit stress for 1/r=38.2 and 1/r=112.8

1/r = 38.2 13305 + 21 or 13340 - 14 = 13326

1/r=112.8 8090 +14 or 8125-21= 8105

MAIN MEMBERS-Ratios of 1/r up to 120

SECONDARY MEMBERS-Ratios of 1/r up to 150

Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10
			275	13375		50	12500		62.5	11625	
			38	13340			12465		63	11590	
				13305		51	12430			11555	
			39	13270			12395			11520	
	Maximum			13235		52	12360			11485	
			40	13200		.5	12325		65	11450	
28.57	14000			13165		53	12290		.5	11415	
20.0.			41	13130		.5	12255		66	11380	
29	13970		.5	13095		54	12220		.5	11345	
.5	13935		42	13060		,5	12185		67	11310	
30	13900		.5	13025		55	12150		.5	11275	
.5	13865		43	12990		.5	12115		68	11240	
31	13830	7	.5	12955	7	56	12080	7	.5	11205	7
.5	13795		44	12920		.5	12045		69	11170	
32	13760		.5	12885		57	12010		.5	11135	
.5	13725		45	12850		.5	11975		70	11100	
33	13690		.5	12815		58	11940		.5	11065	
.5	13655		46	12780		.5	11905		71	11030	
34	13620		.5	12745		59	11870		.5	10995	
.5	13585		47	12710		.5	11835		72	10960	
35	13550		.5	12675		60	11800			10925	
.5	13515		48	12640		.5	11765		73	10890	
36	13480		.5	12605		61	11730			10855	
.5	13445		49	12570			11695		74	10820	
37	13410		.5	12535		62	11660			10785	
.5	13375	1	50	12500		.5	11625		75	10750	

ALLOWABLE UNIT STRESSES IN POUNDS PER SQUARE INCH by Compression Formula of

Chicago Building Law: $16000-70\frac{1}{r}$

MAIN MEMBERS—Ratios of 1/r up to 120 SECONDARY MEMBERS—Ratios of 1/r up to 150

Translation Control											
Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio.	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10	Ratio,	Unit Stress, Pounds	Diff. 0.10
	Tourida			1 ounds			1 Ounces			1 ounus	
75	10750		95	9350		115	7070		105	2770	
5	10735			9315		115	7950		135	6550	
76	10680		.5	9313		.5 116	7915		.5	6515	
.5	10645		.5	9245			7880		136	6480	
77	10610		97	9210		.5	7845 7810		.5	6445	
.5	10575		.5	9175		.5	7775			6410 6375	
78	10540		98	9140		118	7740		.5	6340	
.5	10505		.5	9105		.5	7705		.5	6305	
79	10470		99	9070		119	7670		139	6270	
.5	10435		.5	9035		.5	7635		.5	6235	
80	10400		100	9000		120	7600		140	6200	
.5	10365		.5	8965		.5	7565		.5	6165	
81	10330		101	8930		121	7530		141	6130	
,5	10295		.5	8895		.5	7495		.5	6095	
82	10260		102	8860		122	7460		142	6060	
.5	10225		.5	8825		.5	7425		.5	6025	
83	10190		103	8790		123	7390		143	5990	
.5	10155		.5	8755		.5	7355		.5	5955	
84	10120		104	8720		124	7320		144	5920	
.5	10085		.5	8685		.5	7285		.5	5885	
85	10050	7	105	8650	7	125	7250	7	145	5850	7
.5	10015		.5	8615		.5	7215		.5	5815	
86	9980		106	8580	16	126	7180		146	5780	
.5	9945		.5	8545		.5	7145		.5	5745	
87	9910		107	8510		127	7110		147	5710	
.5	9875		.5	8475		.5	7075		.5	5675	
88	9840		108	8440		128	7040		148	5640	
.5	9805		.5	8405		.5	7005		.5	5605	
89	9770		109	8370		129	6970		149	5570	
.5 90	9735		.5	8335		.5	6935		.5	5535	
	9700 9665		110	8300		130	6900		150	5500	
.5 91	9630		.5 111	8265		.5	6865				
.5	9595			8230 8195		131	6830				
92	9560		.5 112	8160		.5	6795 6760				
.5	9525		.5	8125		.5	6725				
93	9490		113	8090		133	6690				
.5	9455		.5	8055		.5	6655				
94	9420		114	8020		134	6620				
.5	9385		.5	7985		.5	6585				
95	9350		115	7950		135	6550				
	1 0000		110	1000		100	3000		4		

CARNEGIE BEAM SECTIONS

18-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of Chicago Code

			Nominal	Depth an	d Flange	Width-	Weight pe	r Foot		
Effective	CB 1	83 18"x	12"	CB 18	32 18"x8	31/2"	C:	B 181	18"x7½"	,
Length in Feet	100 lbs.	93 1bs.	86 lbs.	78 lbs.	72 1bs.	67 lbs.	58 lbs.	52 lbs.	51 lbs.	47 lbs.
3 4 5	412 412 412	383 383 383	354 354 354	321 321 319	296 296 294	276 276 273	239 239 231	214 214 207	210 209 202	194 193 186
6 7 8 9	412 412 403 395	383 383 375 367	354 354 346 339	309 299 290 280	285 276 267 258	265 256 248 240	222 214 205 197	199 191 184 176	194 186 179 171	180 173 166 159
10 11 12	386 378 369	359 351 343	332 324 317	270 261 251	249 240 231	231 223 214	189 180 172	161 153	163 155 148	152 145 138
13 14 15	361 353 344	335 328 320	310 302 295	241 231 222 212	222 213 204	206 198 189	163 155 146	145 138 130	140 132 125	131 124 117
16 17 18 19 20	336 327 319 311 302	312 304 296 288 281	288 281 273 266 259	202 193 183 173	186 177 168 159	172 164 156 147	130 121 113 104	115 107 99 92	109 102 94 86	103 96 89 82
21 22 23 24 25	294 285 277 268 260	273 265 257 249 241	251 244 237 229 222	164 154 144 135	150 141 132 123	139 130 122 114	96	84		
26 27 28 29	252 243 235 226	233 226 218 210	215 208 200 193							
30 32 34 36	218 201 184 167	186 171 155	186 171 156 142							
Area, in.	29.40	27.35	25.29	22.94	21.17	19.69	17.05	15.30	15.00	13.82
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	1783.4 7.79 253.4 2.94	1648.4 7.76 234.0 2.93	1514.1 7.74 214.7 2.91	1318.8 7.58 90.9 1.99	1208.1 7.55 82.9 1.98	1117.1 7.53 76.4 1.97	960.8 7.51 49.0 1.70	855.1 7.48 43.3 1.68	810.0 7.35 40.5 1.64	768.6 7.46 38.7 1.67
Weight Lbs. per Foot		93	86	78	72	67	58	52	51	47

CARNEGIE BEAM SECTIONS—Continued

16-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of Chicago Code

	1			Nom	inal D	epth a	and Fla	ange V	Vidth-	-Weig	ht per	Foot			
Effective Length		CB 16 16"x14			CB 16 6"x12			CB 16				162 'x7''		CB 16"	
in Feet	115 lbs.	107 lbs.	100 lbs.	90 lbs.	83 lbs.	76 lbs.	68 lbs.	63 lbs.	58 lbs.	50 lbs.	45 lbs.	43 lbs.	40 lbs.	38 lbs.	35 lbs.
3 4 5 6 7	473 473 473 473 473	440 440 440	412 412 412	370 370 370	342 342 342	313 313 313	$ \begin{array}{ c c c c c } $	$\frac{259}{258}$ $\frac{250}{250}$	$\frac{239}{237}$	197	185 184 177 170 163	$\frac{174}{167}$		156 150 143 136 129	138 131 125
8 9 10 11 12	473 469 461 453 445	$\frac{436}{429}$ $\frac{421}{421}$	408 401 394	363 356 348 340 333	$\frac{328}{321}$ $\frac{314}{314}$	300 293	253 245 237 229 220	234 227 219 211 203	208	174 166 159 151 143	156 149 142 135 128	146 139 132 125 118	132	121 114 107 100 93	111 105 98 92 85
13 14 15 16 17	437 429 421 413 405	391 384	373 366 359	325 318 310 303 295	293 286 279	$267 \\ 261 \\ 255$	212 204 195 187 179	196 188 180 172 165		135 128 120 112 105	121 114 107 101 94	111 104 97 90 83	107 101 95 89 82	86 78 71 64	78 72 65 58
18 19 20 22 24	397 389 381 365 349	354		288 280 273 258 243	265 258 251 237 223	$ \begin{array}{r} 235 \\ 229 \\ 216 \end{array} $	170 162 154 137 120	$ \begin{array}{r} 157 \\ 149 \\ 142 \\ \hline 126 \\ 111 \end{array} $	$144 \\ 137 \\ 130 \\ 115 \\ 101$	97 89 82	87 80 73	76	76 70		
26 28 30 32 34	333 317 301 285 269	294 279	275	227 212 197 182 167	209 195 181 167 153	177 165 152									
36 38 40 42 44	253 237 221 205 189	235 220 205 190 175	$\frac{191}{177}$	152	139	126									
Area, in.2	33.82	31.46	29.41	26.46	24.41	22.34	20.00	18.52	17.06	14.70	13.23	12.65	11.75	11.17	10.29
	1665.6 7.02	1537.2 6.99	1426.8	1275.5 6.94 230.0 2.95	1167.7 6.92	1061.3				666.0 6.73 38.2 1.61		-			
Weight Lbs. per Foot	115	107	100	90	83	76	68	63	58	50	45	43	40	38	35

CARNEGIE BEAM SECTIONS—Continued

14-Inch Columns

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of Chicago Code

			Nominal	Depth a	nd Flange	Width-	-Weight p	er Foot		
Effective					CB 146	14"x15"	''			
in Feet	305 lbs.	295 1bs.	285 lbs.	275 lbs.	265 lbs.	255 lbs.	245 lbs.	235 lbs.	225 lbs.	215 lbs.
6 7 8 / 9	1256 1256 1256 1256	1215 1215 1215 1215	1173 1173 1173 1173	1132 1132 1132 1132	1091 1091 1091 1091	1050 1050 1050 1050	1009 1009 1009 1009	968 968 968 968	926 926 926 926	885 885 885 885
10 11 12 13 14	1253 1235 1217 1199 1180	1212 1194 1176 1159 1141	1170 1153 1136 1119 1102	1128 1112 1095 1079 1062	1087 1071 1055 1039 1023	1045 1030 1015 999 984	989 974 959 944	962 948 934 919 905	921 907 894 880 866	867 853 840 827
15 16 17 18 19	1162 1144 1126 1108 1089	1123 1106 1088 1071 1053	1085 1068 1051 1034 1016	1045 1029 1012 996 979	991 975 959 943 927	968 953 937 922 906 891	930 915 900 885 870 855	891 876 862 848 833 819	852 839 825 811 797 784	814 801 787 774 761 748
20 22 24 26 28 30	1071 1035 998 962 926 889	1035 1000 965 929 894 859	999 965 931 897 863 828	963 929 896 863 830 797	895 863 831 799 767	860 829 798 768 737	825 796 766 736 706	790 762 733 704 676	756 729 701 673 646	721 695 669 642 616
32 34 36 38 40	853 816 780 744 707	823 788 753 718 682	794 760 726 692 658	764 731 697 664 631	735 703 671 639 607	706 675 644 613 582	676 647 617 587 557	647 618 590 561 532	618 591 563 536 508	589 563 537 510 484
42 44 46 48 50	671 634 598 562 525	647 612 576 541 506	623 589 555 521 487	598 565 532 499 465	575 543 511 479 447	551 521 490 459 428	528 498 468 438 408	504 475 446 418 389	481 453 426 398 371	457 431 405 378 352
Area, in.2	89.70	86.76	83.82	80.87	77.93	74.99	72.06	69.11	66.17	63.23
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	4121.5 6.78 1539.1 4.14	3948.1 6.75 1479.4 4.13	3778.1 6.71 1420.7 4.12	3607.8 6.68 1362.0 4.10	3442.4 6.65 1304.2 4.09	3280.0 6.61 1247.1 4.08	3119.6 6.58 1190.6 4.06	2961.9 6.55 1134.5 4.05	2806.2 6.51 1079.1 4.04	2654.7 6.48 1024.5 4.03
Weight Lbs. per Foot	305	295	285	275	265	255	245	235	225	215

CARNEGIE BEAM SECTIONS—Continued

14-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—City of Chicago Code

	1		Nomi	nal Dept	h and F	lange W	idth—W	eight pe	Foot		
Effective Length					CB:	146 14'	'x15''				
in Feet	205	195	185	175	165	155	145	135	131	125	115
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
6	844	803	762	$\begin{array}{r} 721 \\ 721 \\ 721 \\ 721 \\ 721 \end{array}$	679	638	597	556	539	515	473
7	844	803	762		679	638	597	556	539	515	473
8	844	803	762		679	638	597	556	539	515	473
9	844	803	762		679	638	597	556	539	515	473
10	838	797	756	715	673	632	591	550	530	509	468
11	826	785	744	704	663	622	582	542	522	501	461
12	813	773	733	693	653	613	573	533	513	493	453
13	800	761	721	682	643	603	564	524	505	485	446
14	788	749	710	671	632	593	555	516	496	477	439
15	775	737	699	660	622	584	546	507	488	469	432
16	762	725	687	649	612	574	536	499	479	461	424
17	750	713	676	638	601	564	527	490	470	453	417
18	737	701	664	627	591	554	518	482	462	446	410
19	725	689	653	617	581	545	509	473	453	438	402
20	712	677	641	606	570	535	500	465	445	430	395
22	687	653	618	584	550	515	482	448	428	414	380
24	661	628	595	562	529	496	464	431	410	398	366
26	636	604	572	540	509	477	445	414	393	382	351
28	611	580	549	519	488	457	427	397	376	366	337
30	586	556	526	497	468	438	409	380	359	351	322
32	560	532	504	475	447	418	391	363	342	335	307
34	535	508	481	453	426	399	372	346	325	319	293
36	510	481	458	431	406	379	354	329	307	303	278
38	485	460	435	410	385	360	336	312	290	287	264
40	459	436	412	388	365	341	318	294	270	271	249
42 44 46 48 50	434 409 384 358 333	412 388 364 339 315	389 366 343 320	366 344 323 301	344 323 303 282	321 302 282 263	299 281 263 245	277 260 243 226	256 239 222	256 240 224 208	234 220 205 191
Area, in.2	60.28	57.34	54.41	51.47	48.52	45.58	42.64	39.70	38.52	36.75	33.82
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	2505.0	2358.2	2213.5	2071.7	1932.6	1796.8	1662.7	1530.4	1358.4	1402.1	1275.9
	6.45	6.41	6.38	6.34	6.31	6.28	6.24	6.21	5.94	6.18	6.14
	970.3	916.8	863.9	811.6	759.9	709.0	658.5	608.4	547.3	559.4	510.9
	4.01	4.00	3.98	3.97	3.96	3.94	3.93	3.92	3.77	3.90	3.89
Weight Lbs. per Foot	205	195	185	175	165	155	145	135	131	125	115

CARNEGIE BEAM SECTIONS-Continued

14-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of Chicago Code

				Nomi	nal De	pth a	nd Fla	nge W	idth-	-Weigl	ht per	Foot			
Effective Length		B 145			B 144			B 143 4"x8"			CB 14"	142 x63/4"			CB 141 14"x6"
in Feet	105 lbs.	95 lbs.	85 lbs.	75 lbs.	68 lbs.	61 lbs.	58 lbs.	53 lbs.	48 lbs.	42 lbs.	39 lbs.	38 lbs.	36 lbs.	33 lbs.	30 lbs.
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 22 24 26 28 28 28 28	432 432 432 432 427 418 410 401 393 385 376 368 359 351 342 334 320 292 277 258	391 391 391 391 386 378 370 363 355 347 340 332 324 301 294	350 350 350 350 350 345 338 331 324 310 303 297 266 262 262 248 232 222 222 222 222 222 222 222 222 22	308 300 293 285 278 270 263 255 248 240 203 210 203 8 188 173 113 7 143	258 252 245 238 231 224 217 211 204 197 196 183 176 156 143 124	251 ¹ 2500 244 238 231 225 219 213 207 201 194 188 182 176 3 164 3 15 3 13 2 12 3 11	221 213 206 198 191 183 176 168 161 1 153 14 124 1 109 9	218 208 201 195 188 181 174 167 160 153 147 111 111 111 111 111 111 111 111 111	198 195 188 182 176 163 157 151 145 132 132 126 114 0 103	164 158 151 144 138 131 124 118 111 105 98 91 85 77	159 153 146 140 134 128 122 116 109 103 97 91 85 79	134 128 121 115 109 102 96 89 83 77 70 64	118 112 106 100 95 89 83 72	113 108 102 97 92 87 81 76 65 60	102 97 91 85 80 74 69 63 58
30 32 34 36 38 Area, in I ₁₋₁ , in. I ₁₋₁ , in. I ₁₋₂ , in. I ₂₋₂ , in.	241 223 203 19 17- 230.8 1169 6.18 292 3.00	1 217 5 202 8 186 1 177 4 156 8 27.9 6 1044 5 6.11 6 262.	7 193 2 186 5 16 1 15 6 13 3 24.9 .0 921 1 6.0 0 232	3 123 0 6 6 2 8 8 9 22.0 3 823.7 6.1 0 134	5 19.9 5 738 1 6.0 .5 120	99 17.9 .8656 8 6.0	2 04 17.0 2 609. 5 5.9 .1 62.	4 552 8 5.9 8 56	5 496 5 5.9 8 50.	0 431 3 5.9 8 30.	5 398. 1 5.89 2 27.	3 357. 9 5.66 7 24.	5 365. 6 5.88 2 25.4	6333. 5.86 4 23.0	4 292.0 5 5.75 15.5
Weigh Lbs. pe Foot		5 9.	5 8	5 7	5 6	8 6	1 5	8 3	3 4	8 42	39	38	36	33	30

CARNEGIE BEAM SECTIONS—Continued

12-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—City of Chicago Code

7700	1		N	Icmina	l Depth	and F	lange W	/idth—	Weight	per Fo	ot		
Effective Length	е	СВ	127 1	2"x14"			CB 126	12"x	14"	C	B 125	12"x	12"
in Feet	230	220	210	200	190	180	170	160	150	140	130	120	110
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
6	947	906	865	823	782	741	700	659	618	577	535	494	453
7	947	906	865	823	782	741	700	659	618	577	535	494	453
8	947	906	865	823	782	741	700	659	618	567	527	487	447
9	946	904	863	821	780	737	696	656	616	555	516	477	438
	930	889	849	808	768	725	685	645	605	544	506	468	430
11	915	875	835	795	755	713	673	634	595	532	495	458	421
12	900	860	821	781	742	700	662	624	585	521	485	448	412
13	885	846	807	768	730	688	650	613	575	509	474	439	403
14	870	831	793	755	717	676	639	602	565	498	463	429	395
15	854	817	779	741	704	664	627	591	555	486	453	419	386
16	839	802	765	728	692	652	616	581	545	475	442	410	377
17	824	788	751	715	679	639	604	570	535	464	432	400	368
18	809	773	737	701	666	627	593	559	525	452	421	390	359
19	794	758	723	688	654	615	581	548	515	441	410	380	351
20	778	744	709	675	641	603	570	538	505	429	400	371	342
22	748	715	681	648	616	578	547	516	486	406	379	351	324
24	718	686	653	621	590	554	524	494	465	383	357	332	307
26	687	656	626	595	565	529	501	473	445	360	336	313	289
28	657	627	598	568	540	505	478	451	425	337	315	293	272
30	626	598	570	542	515	481	455	430	405	314	294	274	254
32 34 36 38	596 566 535 505	569 540 511 482	542 514 486 458	515 488 462 435	489 464 439 413	456 432 407 383	432 409 386 363	408 387 365	385 364 344	291 268 245	273 251 230	255 235 216	237 219 201
42 44 46	475 444 414 383	452 452 423 394 365	402 375 347	382 355 329	363 337 312	358 358 334 309	317 294	344 322 301 279	324 304 284 264 244			196	184
Area, in.2	67.64	64.70	61.76	58.82	55.88	52.94	50.00	47.06	44.12	41.18	38.24	35.28	32.34
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	1461.9	1426.6	1391.3	1356.1	1320.8	1218.1	1182.8	1147.5	1112.2	934.8	899.5	864.1	828.8
	4.65	4.70	4.75	4.80	4.86	4.80	4.86	4.94	5.02	4.76	4.85	4.95	5.06
	945.5	898.2	852.9	809.5	767.8	702.4	666.9	633.0	600.4	372.4	350.5	329.6	309.9
	3.74	3.73	3.72	3.71	3.71	3.64	3.65	3.67	3.69	3.01	3.03	3.06	3.10
Weight Lbs. per Foot	230	220	210	200	190	180	170	160	150	140	130	120	110

CARNEGIE BEAM SECTIONS—Continued

12-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of Chicago Code

	Nominal Depth and Flange Width—Weight per Foot											
Effective Length in Feet	CI	B 124	12"x10	,	CB 1	23 12'	'x8''	CH		CB 121 12"x6"		
In Peet	100 lbs.	91 lbs.	83 lbs.	75 lbs.	50 lbs.	45 lbs.	40 lbs.	36 1bs.	34 1bs.	32 lbs.	28 lbs.	25 - lbs.
3 4 5	412 412 412	375 375 375	342 342 342	309 309 309	206 206 204	185 185 183	165 165 163	148 146 141	140 137 131	132 130 125	115 113 109	103 99 95
6 7 8 9	409 398 388 378 367	372 363 354 344 335	340 331 324 315 307	309 301 294 286 279	198 191 185 179 173	178 172 167 161 155	158 153 148 143 138	135 129 124 118 112	125 119 114 108 102	120 115 109 104 99	104 100 95 91 86	90 86 81 77 72
11 12 13 14 15	357 347 336 326 316	326 316 307 298 288	298 290 282 273 265	272 264 257 249 242	166 160 154 148 142	150 144 138 133 127	133 128 122 117 112	106 101 95 89 83	96 90 85 79	94 89 84 79 73	82 77 73 68 64	68 63 59 54 50
16 17 18 19 20	305 295 285 274 264	279 270 260 251 242	257 248 240 232 223	235 227 220 213 205	135 129 123 117	$ \begin{array}{r} 121 \\ 116 \\ 110 \\ 104 \\ \hline 99 \end{array} $	107 102 97 92 87	78 72 66 60	67 61 56	68 63 58 53	59 55 50 46	45 41
21 22 23 24 25	253 243 233 222 212	232 223 214 204 195	215 206 198 190 181	198 190 183 176 168	104 98 92 85	93 88 82 76	82 77 72 67					
26 27 28 29 30 31	202 191 181 171	186 176 167 158 148	173 165 156 148 139 131	161 154 146 139 131 124						-		
Area, in.	29.41	26.76	24.41	22.05	14.69	13.23	11.76	10.59	9.99	9.40	8.22	7.34
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	659.0 4.73 167.5 2.39	4.84	4.95	5.09	5.22 57.5	5.19 51.2	5.17 44.9	280.1 5.14 25.4 1.55	238.1 4.88 21.0 1.45	246.3 5.12 22.3 1.54	213.4 5.10 19.2 1.53	4.99 13.8
Weight Lbs. per Foot		91	83	75	50	45	40	36	34	32	28	25

CARNEGIE BEAM SECTIONS—Continued

10-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of Chicago Code

	Nominal Depth and Flange Width—Weight per Foot												
Effective Length		СВ	105	10"x12	"		Cl	3 104	10"x1	0"	CB 1	03 10	"x9"
in Feet	140 lbs.	132 lbs.	124 lbs.	116 lbs.	108 lbs.	100 lbs.	92 lbs.	84 lbs.	77 1bs.	70 lbs.	63 1bs.	56 lbs.	49 1bs
5 6 7 8 9	576 576 576 569 558 546	543 543 543 537 526 516	511 511 511 504 494 484	478 478 478 472 463 454	445 445 445 440 432 423	418 418 418 408 400 392	379 378 369 360 351 342	346 345 337 328 320 312	317 317 309 302 294 287	288 288 282 275 268 262	259 253 246 239 231 224	231 226 220 213 207 201	202 199 193 188 183 177
11 12 13 14 15	535 524 513 502 490	505 494 484 473 463	474 465 455 445 435	445 435 426 417 408	415 406 397 389 380	385 377 369 361 353	333 324 315 306 297	303 295 286 278 270	279 271 264 256 249	255 248 241 234 228	216 209 202 195 187	194 188 182 175 169	172 167 161 156 151
16 17 18 19 20	479 468 457 445 434	452 442 431 421 410	425 415 405 395 385	399 389 380 371 362	372 363 355 346 338	345 338 330 322 314	287 278 269 260 251	261 253 245 236 228	241 234 226 218 211	221 214 207 201 194	180 173 166 158 151	163 157 150 144 138	145 140 135 129 124
21 22 23 24 25	423 412 400 389 378	399 389 378 368 357	375 365 355 346 336	352 343 334 325 316	329 321 312 304 295	306 299 291 283 275	242 233 224 215 206	220 211 203 194 186	203 196 188 180 173	187 180 173 167 160	144 136 129 122 115	131 125 119 113 106	119 113 108 103 97
26 27 28 29 30	367 356 344 333 322	347 336 326 315 304	326 316 306 296 286	306 297 288 279 269	287 278 270 261 253	267 259 252 244 236	197 187 178 169 160	178 169 161 153 144	165 158 150 143 135	153 146 140 133 126	107	100 94	92 87 81
32 34 36 38	299 277 255 232	283 262 241 220	266 246 227 207	251 233 214 196	235 218 201 184	220 205 189 173							
Area, in.2	41.17	38.81	36.46	34.11	31.76	29.40	27.06	24.70	22.65	20.59	18.53	16.47	14.41
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	623.2 3.89 391.4 3.08	603.5 3.94 369.6 3.09	583.9 4.00 349.0 3.09	564.3 4.07 329.4 3.11	544.8 4.14 310.7 3.13	525.1 4.23 292.8 3.16	423.2 3.96 163.1 2.50	403.6 4.04 152.0 2.48	386.5 4.13 142.9 2.51	369.3 4.24 134.3 2.55	300.4 4.03 85.2 2.14	283.2 4.15 79.5 2.20	266.0 4.30 74.2 2.27
Weight Lbs. per Foot	140	132	124	116	108	100	92	84	77	70	63	56	49

CARNEGIE BEAM SECTIONS—Continued

10 AND 9-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress-City of Chicago Code

1	Nominal Depth and Flange Width—Weight per Foot													
Effective Length	CB 1	02 10	"x8"	CI	3 101	10"x6	"	СВ	93 9"	x9"	CB 92 9"x6½"			
in Feet	42 lbs.	36 lbs.	31 lbs.	30 1bs.	26 lbs.	23 1bs.	21 lbs.	48 lbs.	43 lbs.	38 lbs.	35 lbs.	32 lbs.	29 lbs.	
1 2 3 4 5	173 173 173 173 168	148 148 148 148 145	128 128 128 128 128	123 123 123 121 116	107 107 107 104 100	95 95 95 92 88	86 86 86 84 80	198 198 198 198 198	177 177 177 177 177	156 156 156 156 156	144 144 144 143 138	132 132 132 131 126	119 119 119 118 114	
6 7 8 9 10	162 156 150 144 138	140 135 130 125 120	121 117 113 109 105	110 105 100 95 90	95 91 86 82 77	84 80 76 72 68	76 73 69 65 61	195 190 184 179 174	174 170 165 160 156	154 150 146 141 137	132 127 122 116 111	121 116 111 106 101	109 105 100 96 91	
11 12 13 14 15	132 126 120 114 108	115 110 105 100 95	101 97 93 89 85	85 80 75 70 64	73 68 64 59 55	64 61 57 53 49	58 54 50 47 43	169 164 158 153 148	151 146 142 137 132	133 129 125 121 116	106 100 95 89 84	96 91 86 81 76	87 82 78 73 69	
16 17 18 19 20	102 96 90 84 78	90 85 80 75 71	81 77 73 69 65	59 54 49	50 46	45 41	39 35	143 138 133 127 122	128 123 118 114 109	112 108 104 100 96	79 73 68 63 57	71 67 62 57 52	64 60 55 51	
21 22 23 24 25	72	66 61	61 57 53					117 112 107 102 96	104 100 95 90 86 81	92 87 83 79 75				
27 28								86 81	76 72	67 62				
Area, in.2	12.35	10.58	9.11	8.82	7.64	6.76	6.17	14.11	12.65	11.17	10.29	9.40	8.53	
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	190.4 3.93 36.8 1.73	175.6 4.07 34.4 1.80	163.4 4.23 32.5 1.89	163.2 4.30 18.5 1.45	139.5 4.27 15.7 1.43	122.2 4.25 13.7 1.43	107.6 4.18 12.0 1.39	221.1 3.96 73.8 2.29	195.5 3.93 65.4 2.28	170.4 3.91 57.1 2.26	155.4 3.89 26.6 1.61	140.5 3.87 24.0 1.60	126.0 3.84 21.5 1.59	
Weight Lbs. per Foot	42	36	31	30	26	23	21	48	43	38	35	32	29	

CARNEGIE BEAM SECTIONS—Concluded

8-INCH COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—City of Chicago Code

	Nominal Depth and Flange Width—Weight per Foot													
Effective Length					CB 8	83 8"	x8''					CB 8	2 8"x	61/2"
in Feet	90 lbs.	84 lbs.	78 lbs.	72 lbs.	66 lbs.	60 lbs.	54 lbs.	48 lbs.	42 lbs.	36 lbs.	31 lbs.	30 lbs.	27 lbs.	24 lbs.
1 2 3 4 5	371 371 371 371 371 371	346 346 346 346 346	321 321 321 321 321 321	296 296 296 296 296	272 272 272 272 272 272	247 247 247 247 247 247	222 222 222 222 222 222	197 197 197 197 197	173 173 173 173 172	148 148 148 148 147	127 127 127 127 127 127	123 123 123 123 123	111 111 111 110 106	99 99 99 98 95
6 7 8 9 10	362 352 342 331 321	337 328 318 308 299	313 304 295 286 277	288 280 272 263 255	264 256 249 241 233	240 232 225 218 211	215 209 202 196 190	191 185 180 174 168	167 162 157 152 147	143 138 134 130 125	123 119 115 111 108	114 109 105 100 96	102 98 94 90 86	91 87 83 80 76
11 12 13 14 15	$ \begin{array}{r} 311 \\ 301 \\ 290 \\ 280 \\ 270 \end{array} $	$\begin{array}{c} 289 \\ 280 \\ 270 \\ 260 \\ 251 \end{array}$	268 259 250 241 232	246 238 230 221 213	225 218 210 202 195	204 197 190 183 176	183 177 170 164 157	162 157 151 145 139	142 136 131 126 121	121 116 112 108 103	104 100 96 92 89	91 86 82 77 73	82 78 73 69 65	72 69 65 61 58
16 17 18 19 20	260 249 239 229 219	241 231 222 212 202	223 214 205 196 187	205 196 188 179 171	187 179 171 164 156	169 162 155 147 140	151 144 138 132 125	134 128 122 116 111	116 111 106 101 96	99 94 90 86 81	85 81 77 73 70	68 64 59 55 50	57 53 49 45	54 50 47 43 39
21 22 23 24 25	208 198 188 178 167	193 183 173 164 154	178 169 160 151 142	163 154 146 137 129	148 141 133 125 117	133 126 119 112 105	119 112 106 99 93	105 99 93 88 82	91 86 81 75 70	77 72 68 64 59	66 62 58 54 51			
26 27	157 147	144	133	121	110	98								
Area, in.2	26.47	24.71	22.93	21.17	19.40	17.63	15.87	14.10	12.34	10.58	9.10	8.81	7.93	7.06
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	391.2 3.84 124.4 2.17	358.6 3.81 114.5 2.15	326.5 3.77 104.7 2.14	295.9 3.74 95.3 2.12	265.9 3.70 86.1 2.11	237.1 3.67 77.1 2.09	209.2 3.63 68.3 2.07	182.2 3.59 59.7 2.06	156.2 3.56 51.4 2.04	131.3 3.52 43.4 2.02	110.9 3.49 36.7 2.01	107.8 3.50 23.4 1.63	95.9 3.48 20.8 1.62	84.3 3.46 18.3 1.61
Weight Lbs. per Foot	90	84	78	72	66	60	54	48	42	36	31	30	27	24

STANDARD MILL SECTIONS

MISCELLANEOUS SMALL COLUMNS

ALLOWABLE CONCENTRIC LOADS IN THOUSANDS OF POUNDS

Unit Stress—City of Chicago Code

Nominal Depth and Flange Width—Weight per Foot													
Effective	B	40	B 39		H 4 8"x8"			H 3-A		H 3		H 2	H 1
Length	9"x	5½"	8"x5"					6"x6"		6"x6"		5"x5"	4"x4"
in Feet	25	21	21	18	37.7	34.3	32.6	27.5	25	22.5	20	18.9	13.8
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	1bs.	lbs.	lbs.	lbs.	lbs.
$\frac{1}{2}$	103	86	86	74	154	140	133	113	103	93	82	77	56
	103	86	86	74	154	140	133	113	103	93	82	77	56
3	100	85	84	72	154	$\frac{140}{140}$	133	113	103	93	82	76	53
4	95	81	79	68	154		133	110	100	89	80	72	50
5	89	76	74	64	151		131	105	96	85	76	68	46
6	84	71	69	60	146	133	127	100	91	81	73	65	43
7	78	67	63	56	141	129	123	96	87	77	69	61	39
8	72	62	58	51	136	124	118	91	83	73	65	57	36
9	67	58	53	47	131	120	114	86	79	69	62	53	32
(10	61	53	48	43	126	115	110	81	74	65	58	49	29
11 12 13 14 15	55 50 44	49 44 40 35	43 38	39 35 31	120 115 110 105 100	111 106 102 97 93	106 102 97 93 89	76 72 67 62 57	70 66 61 57	61 57 53 49 45	55 51 48 44 41	45 42 38 34 30	25
16 17 18 19 20					95 90 85 80 75	88 84 79 75 70	85 81 76 72 68	52 47	48 44	40 36	37 34		
21 22 23					70 65	66 61 57	64 60 55						
Area,in.2	7.34	6.17	6.17	5.29	11.00	10.00	9.50	8.08	7.33	6.61	5.86	5.47	3.99
I ₁₋₁ , in. ⁴ r ₁₋₁ , in. I ₂₋₂ , in. ⁴ r ₂₋₂ , in.	95.5	87.6	63.4	58.7	120.8	115.5	112.8	49.3	47.0	41.0	38.8	23.8	10.7
	3.61	3.77	3.21	3.33	3.31	3.40	3.45	2.47	2.53	2.49	2.57	2.08	1.64
	8.8	8.1	6.6	6.1	36.9	35.1	34.2	16.0	14.9	12.2	11.4	7.8	3.6
	1.09	1.14	1.03	1.07	1.83	1.87	1.90	1.41	1.43	1.36	1.39	1.20	0.95
Weight Lbs. per Foot	25	21	21	18	37.7	34.3	32.6	27.5	25	22.5	20	18.9	13.8

OFFICES

GENERAL OFFICES:

Pittsburgh, Carnegie Building, 434 Fifth Avenue.

DISTRICT OFFICES:

Birmingham, Brown-Marx Building, 2000 First Avenue, North, Boston, Statler Office Building, 20 Providence Street, Buffalo, The Marine Trust Co. Building, 233-239 Main Street,

Chicago, 208 South La Salle Street,

Cincinnati, Union Trust Building, Fourth and Walnut Streets, Cleveland, Rockefeller Building, 614 Superior Avenue, N. W.,

Denver, First National Bank Building, 17th and Stout Streets,

Detroit, 2130 Buhl Building, 535 Griswold Street,

New Orleans, Maison Blanche, 921 Canal Street,

New York, Empire Building, 71 Broadway,

Philadelphia, Widener Building, Chestnut and Juniper Streets,

Pittsburgh, Carnegie Building, 434 Fifth Avenue,

St. Louis, 506 Olive Street,

St. Paul, 1308 Merchants National Bank Building, 4th & Robert Sts.

EXPORT REPRESENTATIVES:

UNITED STATES STEEL PRODUCTS CO.,

New York, Hudson Terminal, 30 Church Street.

PACIFIC COAST REPRESENTATIVES:

UNITED STATES STEEL PRODUCTS CO., PACIFIC COAST DEPT.

Los Angeles, 2087 East Slauson Avenue,

Portland, 777 Nicolai Street,

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